

**Addendum to  
Hydrologic and Hydraulic Study  
for  
Leucadia  
Drainage Improvement  
Alternatives**

**Encinitas, California**  
January 28, 2005

Prepared for



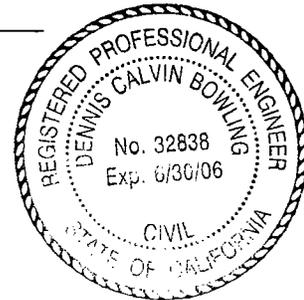
Prepared by

**RICK**  
ENGINEERING COMPANY

**ADDENDUM TO  
HYDROLOGIC AND HYDRAULIC STUDY  
FOR  
LEUCADIA DRAINAGE IMPROVEMENT ALTERNATIVES**

**Job Number 14413**

  
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Attachment 1: Alternative 4 100-Year HEC-1 Analysis

Attachment 2: Alternative 4 100-Year HEC-RAS Analysis

Attachment 3: Alternative 5 10-Year and 100-Year HEC-1 Analyses

Attachment 4: Alternative 5 10-Year and 100-Year HEC-RAS Analyses

Attachment 5: Rick Engineering Company Cost Estimates for Alternative 3 –  
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## INTRODUCTION

Rick Engineering Company conducted a detailed hydrologic and hydraulic study under the direction of the City of Encinitas (City) to analyze inundation of City streets and private properties in Leucadia during varying return frequency storm events. The June 14, 2004 report titled, "Hydrologic and Hydraulic Study for Leucadia Drainage Improvement Alternatives," presents several solutions to improve drainage within the Leucadia area. The findings of this report were presented to Encinitas City Council on June 16, 2004. Subsequently, Rick Engineering Company was contracted to analyze additional drainage improvement alternatives as well as provide supplemental information for the previously analyzed alternatives at the request of City Council. This report presents the additional analyses and information described below, and is an addendum to the June 2004 report. The contents of this report were presented at the City Council meeting on November 16, 2004.

### **Additional Alternatives**

- Alternative 4: Construct a 10-year storm drain facility along Highway 101
- Alternative 5: Construct a storm drain outfall from Leucadia Park to Beacons Beach in combination with grading a portion of Highway 101 (Construct both Alternatives 1 and 2c from the June 2004 report)

### **Supplemental Information**

- Floodplain and photo-simulation exhibits for Alternative 1
- Cost estimate for Alternative 3 assuming 3-phase construction
- Impact of Alternatives 2 and 5 to existing trees along Highway 101
- Cistern Analysis
- Infiltration System
- Quantify parcels removed from 10-year and 100-year floodplains for each alternative
- Summary table of benefits and costs for each alternative

## ADDITIONAL ALTERNATIVES

### **Alternative 4: Construct 10-year Storm Drain Facility**

Construct an underground storm drain system along Highway 101 with the capacity to convey the peak flow rate from the 10-year frequency storm event. This option includes the utilization of the existing 24" storm drain as a low flow system discharging to the detention basins located north of La Costa Avenue to preserve water quality benefits. This storm drain system would remove the 10-year floodplain from the study area because storm runoff would be conveyed in the storm drain system, however runoff exceeding the 10-year storm would be conveyed overland along Hwy 101 and outlet to the NCTD right-of-way as it does today.

Environmental permitting of the outlet has not been investigated but is expected to present a significant challenge in the feasibility of this project.

Hydrologic analyses for Alternative 4 included preparation of the following HEC-1 models:

- 10-year undetained HEC-1 model to determine peak discharge rates within each drainage basin and preliminary pipe sizes. A copy of the HEC-1 is provided in Appendix B of the June 2004 report.
- 100-year detained HEC-1 model diverting the 10-year flow rate into the storm drain system. The peak flow rates calculated in this model were used in the HEC-RAS model to determine floodplain elevations. A copy of the Alternative 4 100-year HEC-1 is provided in Attachment 1 of this addendum.

Normal depth calculations were performed to determine preliminary required pipe sizes for both the main storm drain line and the tributary lateral lines using Manning's equation. A hydraulic model of the main storm drain line was created in WSPGW to confirm the capacity requirements for the storm drain system. The WSPGW model verified that the proposed pipe sizes have the capacity to convey the peak runoff from the 10-year storm event. However, further analyses and design is required if this alternative is selected.

Flooding patterns including floodplain elevations were determined using HEC-RAS. A copy of the Alternative 4 100-year HEC-RAS is provided in Attachment 2 of this addendum. Refer to the HEC-RAS Workmap in Map Pocket 1 in the June 2004 report for the locations of the cross-sections.

Preliminary results show a 3.5-foot diameter pipe at the upstream end of the watershed near Basil Street, transitioning to a 5-foot diameter pipe at the outlet into the lagoon is required to convey the 10-year storm event peak discharge within the storm drain system. Preliminary storm drain pipe sizes are presented in Table 1 shown below.

**Table 1. 10-Year Capacity Storm Drain System Pipe Sizes**

<b>BASIN<sup>*</sup></b>	<b>PEAK Q (cfs<sup>**</sup>)</b>	<b>DIAMETER (FT)</b>
<b>3</b>	11	3.5
<b>4</b>	48	4
<b>5</b>	57	4
<b>7</b>	79	4
<b>8</b>	83	4
<b>9A</b>	91	4.5
<b>9</b>	105	4.5
<b>9B</b>	115	5
<b>10</b>	117	5
<b>11</b>	136	5

\* Only basins along Highway 101 were included in analysis.

\*\* cubic feet per second

Alternative 4 removes approximately 10 parcels from the 100-year floodplain and 116 parcels from the 10-year floodplain. The implementation of Alternative 4 reduces existing 100-year floodplain water surface elevations a maximum of 0.4 feet. Table 2 presents a summary of the 100-year floodplain elevations. Exhibit 1 shows the existing and proposed 100-year floodplains.





### **Alternative 5: Leucadia Park Overflow and Re-grade a Portion of Hwy 101**

Construct an overflow storm drain system to collect runoff from the upper watershed (Basins 1, 2, 3, 4, 5, and 7) at Leucadia Park and re-grade the northbound lanes of Highway 101 from approximately Jupiter Street to Moorgate Road (approximately 3,170 linear feet). This alternative is essentially a combination of Alternative 1 and Alternative 2, Option C, both of which are outlined in the June 2004 report.

In the upper portion of the watershed, storm runoff would be diverted from the main storm drain system at Leucadia Park to an overflow system that would extend from the park through the bluffs at Beacons Beach. Runoff would be conveyed to Leucadia Park through the existing storm drain system and via overland flow. Since the existing storm drain system does not have capacity to convey runoff from storms greater than an estimated 5-year frequency, this alternative would only function efficiently if the storm drain system upstream of the diversion were upsized. If the storm drain system is not upsized, flooding patterns similar to the existing condition would continue because runoff would have to pond until it reached elevations high enough to allow it to pass from sump to sump until reaching the park.

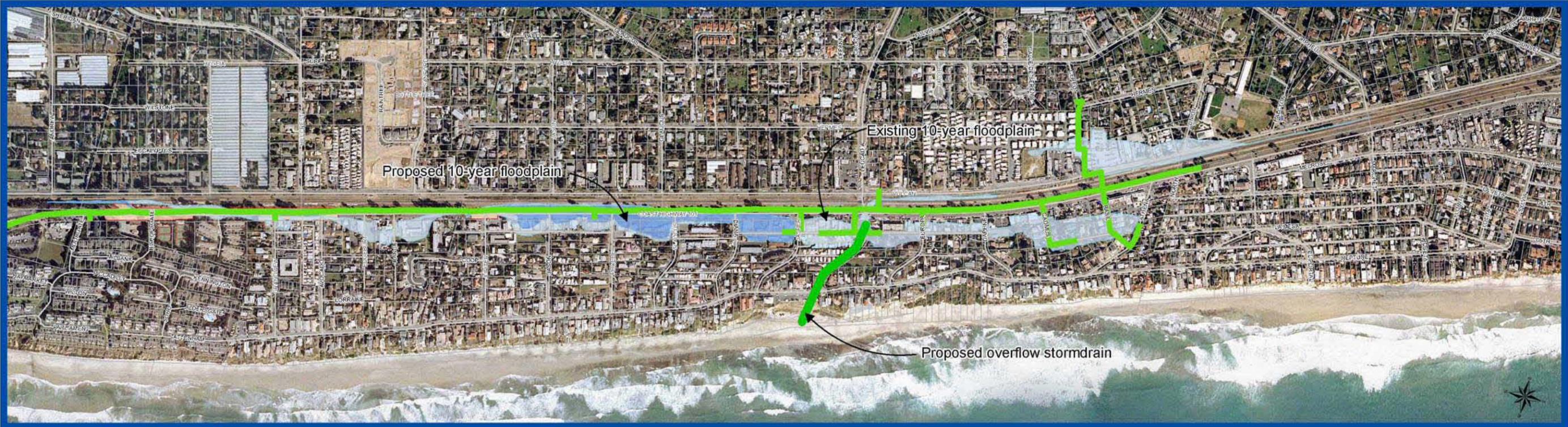
Hydrologic analyses for Alternative 5 included preparation of two HEC-1 models: a 10-year HEC-1 and a 100-year HEC-1 that modeled Basins 9B, 10, and 11 undetained (due to proposed grading of Hwy 101) and modeled all basins upstream as detained, to determine peak discharge rates within each drainage basin for use in the HEC-RAS. Copies of the HEC-1 analyses are provided in Attachment 3 of this addendum.

Flooding patterns including floodplain elevations were determined using HEC-RAS. Copies of the Alternative 5, 10-year and 100-year HEC-RAS analyses are provided in Attachment 4 of this addendum. Refer to the HEC-RAS Workmap in Map Pocket 1 in the June 2004 report for the locations of the cross-sections.

Alternative 5 removes approximately 87 parcels from the 10-year floodplain and 47 parcels from the 100-year floodplain. Alternative 5 reduces existing 10- and 100-year floodplain water surface elevations by a maximum of 3.7 feet and 2.2 feet, respectively. Tables 3 and 4 present a







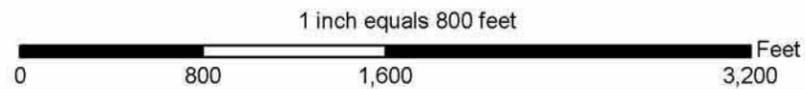
10-Year Floodplain



100-Year Floodplain



Srv\_sd1\DATA\14413\leucadia\_floodplain\_coast\_hwy101\_14413\Proposed\_alt5\_10yr\_100yr.mxd



**Legend**

- █ Proposed Stormdrains
- █ Existing Stormdrains
- Parcels
- Proposed 10-Year Floodplain
- Existing 10-Year Floodplain
- Limits of Grading



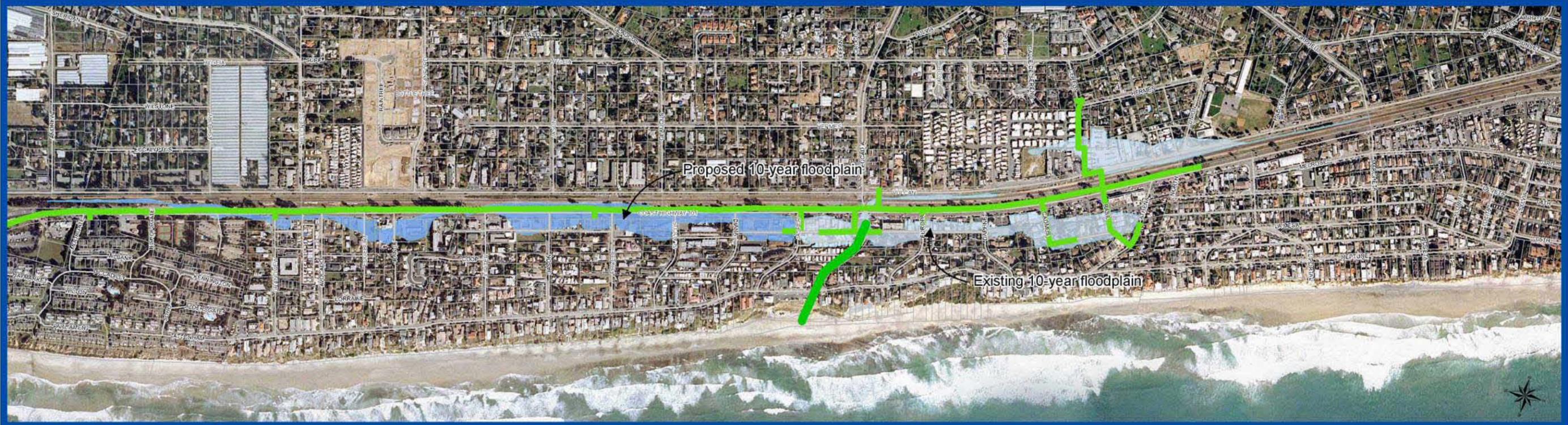
**Exhibit 2:  
ALTERNATIVE 5  
10-YEAR AND 100-YEAR  
FLOODPLAINS**

## SUPPLEMENTAL INFORMATION

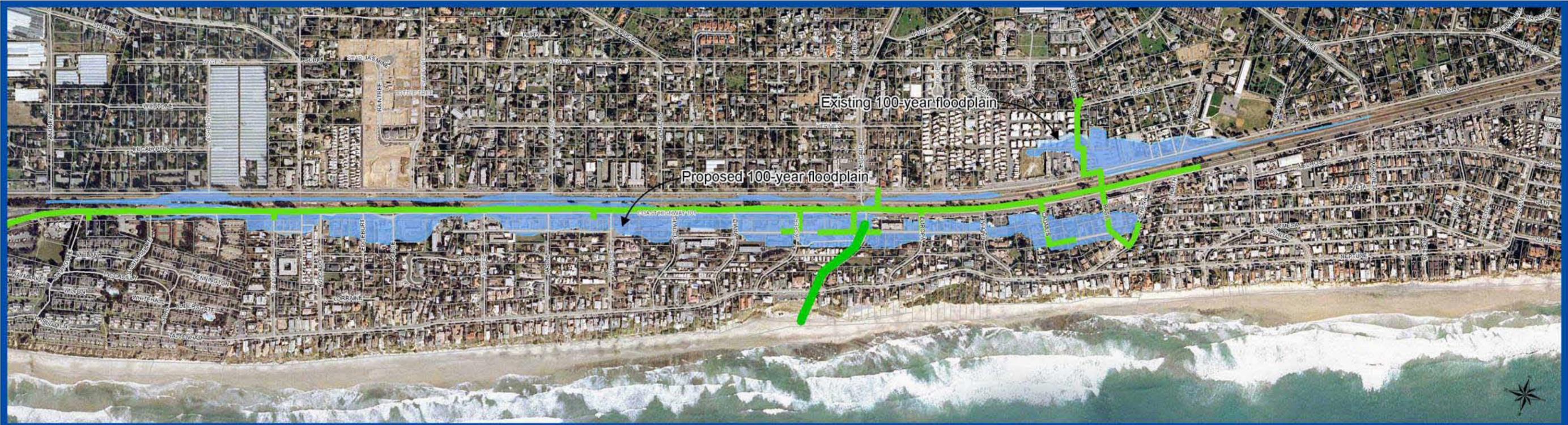
### **Floodplain Exhibit for Alternative 1**

Alternative 1 proposes the construction of an overflow storm drain system to collect runoff from the upper watershed at Leucadia Park, where the runoff would be diverted from the main storm drain line to an overflow system that would discharge over the bluffs at Beacons Beach. The overflow could potentially divert up to 90% of the 10-year runoff and relieve the downstream main storm drain system during smaller storms. It would also eliminate the necessity for pumping at Leucadia Park during storm events smaller than 10-year frequency, which includes the types of storms frequently experienced in Encinitas. This alternative would improve flooding conditions in the upper basins and do little to nothing for the downstream basins. The overflow system is not expected to significantly reduce 100-year floodplain elevations, or affect the size of pipes or cost of installing the ultimate 100-year storm drain system. Exhibit 3 shows the 10-year and 100-year floodplains for Alternative 1.

An example of the proposed outlet structure was created and superimposed on a photograph of Beacons Beach to show generally what aesthetic impact the structure would have to the beachfront. The photo-simulation of the Beacons Beach outlet structure is shown on Exhibit 4.



10-Year Floodplain



100-Year Floodplain

**Legend**

- Proposed Stormdrains
- Existing Stormdrains
- Parcels
- Proposed 10-Year Floodplain
- Existing 10-Year Floodplain

**Location Map**

City of Encinitas

**Exhibit 3:  
ALTERNATIVE 1  
10-YEAR AND 100-YEAR  
FLOODPLAINS**



Existing View



Proposed View

Exhibit 4:  
ALTERNATIVES 1 AND 5  
PHOTO SIMULATION OF  
OVERFLOW OUTLET  
AT BEACONS BEACH

### Cost Estimate for Alternative 3 Assuming 3-Phase Construction

A cost estimate was prepared for constructing the 100-year ultimate storm drain system along Highway 101 in three separate construction periods to spread the cost out over several years. Cost estimates to construct the ultimate storm drain system in one phase, as well as estimated construction costs for three separate phases are summarized below in Table 5. Because the ultimate phased construction schedule is unknown at this time, no consideration for time related escalation was taken.

**Table 5. 100-Year Cost Estimates for Phased Trenchless Construction Methods**

<b>Proposed Trenchless Method 100-Year Storm Event</b>	<b>Estimated Cost<sup>1</sup> for Construction Performed During One Mobilization</b>	<b>Estimated Cost<sup>1</sup> for Phased Construction (August 13, 2004)</b>
<b>TBM only<sup>2</sup></b>	\$30 to 34 million	\$34 to 39 million
<b>TBM and Shield Tunnel<sup>2</sup></b>	\$31 to 35 million	\$35 to 41 million
<b>Conventional Methods<sup>3</sup></b>	\$40 million	\$42 million

1. Estimated costs include equipment mobilization, excavation and spoils disposal, casing or initial tunnel support, shaft construction, grouting, final product pipe, gaskets and fittings, 11 cleanout structures, and 35% for design costs.
2. Cost estimate prepared by Haley & Aldrich (Attachment 6)
3. Cost estimate prepared by Rick Engineering Company (Attachment 5)

As the above table indicates, the cost associated with phased construction is significantly more expensive than the cost associated with construction performed during one mobilization. However, factors such as inflation, depreciation of equipment, and financing costs may make phased construction more cost effective or feasible over time.

### Impact of Alternatives 2 and 5 to Existing Trees Along Highway 101

Grading activities associated with Alternatives 2 and 5 require the removal or relocation (if possible) of several established trees, some of which are large and highly unstable eucalyptus trees. Construction of these alternatives involves grading within the median and Highway 101 right-of-way east of the traffic lanes. An arborist report titled “Assessment of Trees in the Highway 101 Right-Of-Way,” dated October 7, 2002, was prepared by Michael T. Mahoney. This report was referenced to determine the impact to trees within the right-of-way of Highway 101 for each of the grading alternatives (Alternatives 2 and 5).

The arborist report summarizes recommendations to mitigate concern for the stability of 278 trees of various species. The trees are located in the public right-of-way along Highway 101 between La Costa Avenue and A Street. Many are large and mature eucalyptus trees that have suffered injury due to encroachments onto adjacent roadways. Trees are recommended for removal based on their instability. Factors that determine a tree’s stability include anchoring capacity, load bearing and leverage, canopy density, and other conditions and combination of conditions. The report recommends the removal of 32 large trees and 9 smaller trees that are either dead, damaged, or defective. Table 6 presents a summary of the number of trees to be removed or relocated for each grading alternative. The table also summarizes the percentage of those trees to be removed or relocated that were previously recommended for removal by the arborist report.

**Table 6. Trees to be Removed/Relocated by Various Grading Alternatives**

	<b>Number of Trees to be Removed/Relocated by Grading Alternative</b>	<b>Number of Trees Recommended for Removal by Arborist Report</b>	<b>Percent of Number of Trees to be Removed/Relocated that are Recommended for Removal by Arborist Report</b>
<b>Alternative 2</b>			
<b>Option A</b>	20	5	25%
<b>Option B</b>	44	6	14%
<b>Option C</b>	134	24	18%
<b>Alternative 5</b> <i>(Grading Option 2c)</i>	134	24	18%

### **Cistern Analysis**

Some Leucadia residents have expressed interest in the use of cisterns to contain the 100-year flood instead of constructing a 100-year capacity storm drain system. Cisterns are typically used to collect runoff from rooftops into one or more barrels, where it is stored and used as needed to irrigate landscape.

Since cisterns are most widely used as runoff collection systems for individual parcels, it is not surprising that the size of one cistern to store runoff from a 100-year flood for a watershed of this size would be prohibitively large. The dimensions of one cistern that would contain the total

volume of runoff for a 100-year storm were calculated. This calculation is based on the 100-year, 24-hour precipitation data in the San Diego County Hydrology Manual and uses the following assumptions:

- Precipitation = 4",
- Area of the watershed = 0.86 mi<sup>2</sup>,
- Runoff coefficient = 0.65 (65% of rainfall becomes runoff, 35% of rainfall infiltrates),
- Assumes capture and containment of all runoff – if all of the runoff is not captured there would still be flooding in Leucadia.

Volume = Precipitation \* Runoff Coefficient \* Area  
Volume = (4")(0.65)(0.86 mi<sup>2</sup>)  
Volume = 5,194,675 ft<sup>3</sup> or approximately 39 million gallons

Dimensions of one cistern = height \* width \* length  
Dimensions of one cistern = Volume  
Assume height = 8', width = 80', Volume = 5,194,675 ft<sup>3</sup>  
Find length

Volume = (8')(80')(length)  
Length = 5,194,675/[(8')(80')]  
Length = 8117 ft, or 1.5 mi.

Dimensions = 8-ft. deep x 8-ft. wide x 1.5-mi. long

The use of one cistern (or many cisterns) to contain the runoff from the 100-year, 24-hour storm is not a feasible flood control structure. Rick Engineering Company has not analyzed in detail the feasibility of using cisterns to contain smaller, more frequent events (less than 2-year). However, based on preliminary investigation there are several obstacles concerning the logistics of using cisterns including:

- Mobilization of large tanks – the tanks are normally scheduled for delivery in advance, not in emergency (flooding) situations
- Difficult negotiations with NCTD to place the tanks within their right-of-way

- Mobilization of vector trucks to pump runoff from flooded areas and dispose into tanks
- Mobilization of vector trucks to empty tanks after the storm. The tanks must be emptied after each storm to be available for the next storm. With the rains experienced in Leucadia this season there would be a constant effort to empty the tanks.
- Disposal of water in filled tanks after the storm – once the water is contained it either has to be pumped into the sanitary sewer or environmental permits must be obtained to pump it into the lagoon
- Removal of tanks after each storm
- Each mobilization requires availability of personnel
- Significant costs would be incurred with each storm that includes tank rental, personnel, pumping costs, disposal costs, etc.

The City of Encinitas has implemented an emergency response program to address the small, frequent storm events. This program, combined with upgrades to the existing storm drain system, has proven to protect the residents in Leucadia from structural damage due to flooding in the 2004-2005 rainy season to date. The use of cisterns as a short-term solution would be more costly and inefficient than the current program.

### **Infiltration System**

Implementation of an infiltration system to address flooding issues in Leucadia was considered but not analyzed. Infiltration is the downward entry of water into the surface of the soil, commonly used in hydrology to denote the flow of water into soil material. The system would consist of large underground containment structures that would allow runoff to infiltrate into the soil. There has previously been concern expressed by residents living along the coastal bluffs about infiltration causing bluff failures. While studies have indicated that this is not the case with natural infiltration, it may be difficult to make a definitive assessment about this concern relative to large scale induced infiltration. Due to these concerns, implementation of an infiltration system was eliminated from further analysis.

### Quantify Parcels Removed from 10-year and 100-year Floodplains for Each Alternative

Various drainage improvement alternatives are proposed in Leucadia in the City of Encinitas to relieve flooding in the area. Only Alternative 3 removes all parcels from the 100-year floodplain, however, floodplain depths are reduced in the other alternatives. The number of parcels removed from the 10- and 100-year floodplains for each of the proposed alternatives is summarized below in Tables 7 and 8.

**Table 7. Number of Parcels Removed from the 10-year Floodplain**

Alternative	10-Year Study				
	Existing Parcels in Floodplain	Parcels Removed	Parcels Remaining	% Parcels Removed	Approximate Reduction in Flood Depth (ft)
Alt 1	116	69	47	60%	1.5
Alt 2 – Option A	116	0	116	0%	1.1
Alt 2 – Option B	116	2	114	2%	2.3
Alt 2 – Option C	116	18	98	16%	2.7
Alt 3	116	116	0	100%	N/A
Alt 4	116	116	0	100%	N/A
Alt 5	116	87	29	75%	3.7

**Table 8. Number of Parcels Removed from the 100-year Floodplain**

Alternative	100-Year Study				
	Existing Parcels in Floodplain	Parcels Removed	Parcels Remaining	% Parcels Removed	Approximate Reduction in Flood Depth (ft)
Alt 1	152	5	147	3%	0.1
Alt 2 – Option A	152	25	127	16%	1.1
Alt 2 – Option B	152	28	124	18%	2.1
Alt 2 – Option C	152	43	109	28%	2.2
Alt 3	152	152	0	100%	N/A
Alt 4	152	10	142	7%	0.4
Alt 5	152	47	105	31%	2.2

**Summary Table of Benefits and Costs for Each Alternative**

Table 9 shows the number of parcels removed from the 10-year and 100-year floodplains, the percent of parcels removed from the 10-year and 100-year floodplains, the floodplain depth reduction, and the cost estimate for each alternative.

**Table 9. Summary of Benefits and Costs for Each Alternative**

<b>Alternative</b>	<b>Existing Parcels in 10-year Floodplain</b>	<b>% Parcels Removed 10-year Storm</b>	<b>Existing Parcels in 100-year Floodplain</b>	<b>% Parcels Removed 100-year Storm</b>	<b>Approximate Reduction in Flood Depth 100-year (ft)</b>	<b>Cost Estimate</b>
<b>Alt 1</b> Leucadia Overflow	116	60%	152	3%	0.1	\$1.5 – \$2.5 M
<b>Alt 2 – Option A</b> NCTD Grading	116	0%	152	16%	1.1	\$1 M
<b>Alt 2 – Option B</b> Hwy 101 Grading	116	2%	152	18%	2.1	\$3.5 M
<b>Alt 2 – Option C</b> Hwy 101 Grading	116	16%	152	28%	2.2	\$4.5 M
<b>Alt 3</b> 100-yr Storm Drain System	116	100%	152	100%	N/A	\$30-34 M (tunneling methods) \$34-39 M (3-phase tunneling) \$40 M (conventional methods) \$42 M (3-phase conventional)
<b>Alt 4</b> 10-yr Storm Drain System	116	100%	152	7%	0.4	\$18-22M (tunneling methods) \$36 M (conventional methods)
<b>Alt 5</b> Alt 1 + Alt 2 Option C	116	75%	152	31%	2.2	\$6 – \$7 M

## RECOMMENDATIONS

Based on the analyses of the hydrologic and hydraulic characteristics of the Leucadia area, Rick Engineering Company recommends proceeding with the design of Alternative 3, construction of a 100-year capacity storm drain system, which was described in the June 2004 report. Although other alternatives would provide flooding relief for some residents during small, frequent storm events, they do not provide equal protection to the entire area affected by flooding. In addition, new development and redevelopment projects within the City of Encinitas are required to design the finished floor elevations of insurable structures above the 100-year floodplain elevation (where applicable), in accordance with Federal Management Flood Agency's (FEMA) requirement. Not only is construction of any other alternative costly, it would not adequately protect Leucadia from flooding during the 100-year flood and would be considered a "short-term" solution.

**ATTACHMENT 1**

**ALTERNATIVE 4  
100-YEAR HEC-1 ANALYSIS**

**ATTACHMENT 2**

**ALTERNATIVE 4**

**100-YEAR HEC-RAS ANALYSIS**

**ATTACHMENT 3**

**ALTERNATIVE 5  
10-YEAR AND 100-YEAR  
HEC-1 ANALYSES**

**ALTERNATIVE 5**  
**10-YEAR HEC-1 ANALYSIS**

**ALTERNATIVE 5**  
**100-YEAR HEC-1 ANALYSIS**

**ATTACHMENT 4**

**ALTERNATIVE 5  
10-YEAR AND 100-YEAR  
HEC-RAS ANALYSES**

**ALTERNATIVE 5**  
**10-YEAR HEC-RAS ANALYSIS**

**ALTERNATIVE 5**  
**100-YEAR HEC-RAS ANALYSIS**

**ATTACHMENT 5**

**RICK ENGINEERING COMPANY  
COST ESTIMATES FOR  
ALTERNATIVE 3 – PHASED CONSTRUCTION  
AND ALTERNATIVE 4**

**ATTACHMENT 6**

**HALEY & ALDRICH COST ESTIMATES:**

**JUNE 8, 2004**

**AUGUST 13, 2004**

**HALEY & ALDRICH COST ESTIMATE – JUNE 8, 2004**  
**“GEOTECHNICAL FEASIBILITY STUDY”**

**HALEY & ALDRICH COST ESTIMATE – AUGUST 13, 2004**  
**“SUPPLEMENTAL GEOTECHNICAL FEASIBILITY STUDY”**

**ATTACHMENT 1**

**ALTERNATIVE 4**

**100-YEAR HEC-1 ANALYSIS**

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*      JUN 1998                    *
*      VERSION 4.1                  *
*
* RUN DATE 17AUG04 TIME 14:40:45 *
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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

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X   X  XXXXXXXX  XXXXX      X
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X   X X      X           X
XXXXXXX  XXXX   X       XXXXX  X
X   X X      X           X
X   X X      X   X      X
X   X  XXXXXXXX  XXXXX      XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

ENCINITAS 14413  
 100-yr AH. 4  
 100A4.ncl

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

          *DIAGRAM
1         ID *****
2         ID ENCINITAS COAST HWY 101          J-14413          7-13-04
3         ID SAME AS BELOW EXCPET 100-YEAR DETAINED
4         ID DIVERTED 10-YEAR STORM TO STORM DRAIN
5         ID CHANGED FILE NAME
6         ID FN: 100A4.HC1
7         ID *****
8         ID ENCINITAS COAST HWY 101          J-14413          7-13-04
9         ID 100-YEAR UNDETAINED W/PIPE ROUTING BETWEEN BASINS
10        ID SAME AS BELOW BUT DIVERTED 10-YEAR STORM TO STORM DRAIN
11        ID CHANGED FILE NAME
12        ID FN: 100UDTDV.HC1
13        ID *****
14        ID ENCINITAS COAST HWY 101          J-14413          5-27-04
15        ID 100-YEAR UNDETAINED W/PIPE ROUTING BETWEEN BASINS
16        ID FN: 100UD.HC1
17        ID *****
18        ID ENCINITAS COAST HWY 101          J-14413          3-24-04
19        ID REMOVED STORAGE IN BASINS 1 &2
20        ID FN: 100UD.HC1
21        ID *****
22        ID ENCINITAS COAST HWY 101          J-14413          1-08-04
23        ID SAME AS BELOW BUT CHANGED ROUTING TO MATCH DETAINED 100-YR
24        ID RUN (100DET3.HC1) BUT WITHOUT DETENTION
25        ID FN: 100UD.HC1
26        ID *****
27        ID ENCINITAS COAST HWY 101          J-14413          1-07-04
28        ID SAME AS BELOW BUT CHANGED PI CARDS (INCREASED BASIN AREA)
29        ID FN: 100R.HC1
30        ID *****
31        ID ENCINITAS COAST HWY 101          J-14413          12/29/03
32        ID 100-YEAR RUN WITH BASIN AREAS EXTENDED TO THE RIDGE EAST OF
33        ID THE RR TRACKS. PI CARDS CHANGED FOR 100-YR BASED ON FN: E100.HC1
34        ID LAG AND CURVE NUMBERS CHANGED FOR 100-YEAR.
35        ID BASIN AREAS ALSO CHANGED FOR 7 THROUGH 11.
36        ID *****
37        ID ENCINITAS COAST HWY 101
38        ID J-14413
39        ID SEPT 25, 2003
40        ID MODIFIED EXISTING RUN TO MODEL PROPOSED DETENTION OF BASINS
41        ID 1A, 1B, 1, 2, 3, 4, 5, 6, AND 8
42        ID DETENTION CARDS SA/SV, SQ, SE OBTAINED FROM FN: DSI_5R.HC1
43        ID *****
44        ID ENCINITAS- COAST HIGHWAY 101
45        ID JOB # 14413
46        ID 09-12-03
47        ID MODIFIED PUMP Q TO 1.7 CFS, AND ROUTING OF BASINS 9A, 9B, AND 9
48        ID FROM PUMP STATION THROUGH 10" LATERAL, CONFLUENCING
49        ID WITH MAIN LINE AT AT CONNECTION 3 INSTEAD OF CONNECTION 2
50        ID ALSO CHANGED ROUTING THROUGH MAIN LINE FROM LINE G TO CONNECTION
51        ID 2, TO LINE G TO CONNECTION 3
52        ID *****
53        ID ENCINITAS- COAST HIGHWAY 101
54        ID JOB # 14413
    
```

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
55      ID    09-04-03
56      ID    MODIFIED CURVE NUMBER AND REMOVED % IMPERVIOUS
57      ID    *****
58      ID    ENCINITAS- COAST HIGHWAY 101
59      ID    JOB # 14413
60      ID    06-03-03
61      ID    POST-IMPROVEMENT (EXISTING) CONDITION          FN: 101EX_5.HC1
62      ID    5-YEAR, 24-HR STORM EVENT
63      ID    LAG CALCULATION ARE BASED OFF OF NRCS METHOD
64      ID    AND ARE A FUNCTION OF RUNOFF COEF. AND VELOCITY
65      ID    NESTED STORM PER COUNTY OF SAN DIEGO HYDROLOGY MANUAL
66      ID    COPYRIGHT 2003 RICK ENGINEERING COMPANY
67      ID    6HR RAINFALL IS  1.6  INCHES
68      ID    24HR RAINFALL IS  2.5  INCHES
69      ID    TOTAL BASIN AREA IS  .5  SQUARE MILES

*** FREE ***

70      IT      5 01JAN90    1200    300
71      IO      5

72      KK      1A
73      KO      0      0      0      0      21
74      KM      NESTED STORM PER COUNTY OF SAN DIEGO HYDROLOGY MANUAL
75      KM      COPYRIGHT 2003 RICK ENGINEERING COMPANY
76      KM      THE FOLLOWING IT CARD MUST BE USED IN YOUR DATA SET
77      KM      IT 5 01JAN90 1200 300
78      KM      6HR RAINFALL IS  2.5  INCHES
79      KM      24HR RAINFALL IS  4  INCHES
80      KM      DAR30 = .989908
81      KM      DAR60 = .99478
82      KM      DAR180 = .99652
83      KM      DAR360 = .99739
84      KM      DAR1440 = .99826
85      KM      BASIN AREA IS  .87  SQUARE MILES
86      IN      5 01JAN90    1200    300
87      PI      .0047 .00473 .00474 .00476 .00477 .00479 .00481 .00483 .00484 .00486
88      PI      .00488 .0049 .00491 .00494 .00495 .00497 .00499 .00501 .00502 .00505
89      PI      .00506 .00509 .0051 .00513 .00514 .00517 .00518 .00521 .00522 .00525
90      PI      .00527 .0053 .00531 .00534 .00536 .00539 .0054 .00543 .00545 .00548
91      PI      .0055 .00553 .00554 .00558 .00559 .00563 .00565 .00568 .0057 .00573
92      PI      .00575 .00579 .00581 .00584 .00586 .0059 .00592 .00596 .00598 .00602
93      PI      .00604 .00608 .0061 .00614 .00616 .00621 .00623 .00627 .0063 .00634
94      PI      .00636 .00641 .00643 .00648 .00651 .00656 .00658 .00663 .00666 .0067
95      PI      .00674 .00679 .00682 .00688 .0069 .00696 .00699 .00705 .00708 .00714
96      PI      .00717 .00724 .00727 .00733 .00737 .00743 .00747 .00754 .00758 .0076
97      PI      .00768 .00776 .0078 .00788 .00792 .008 .00804 .00812 .00817 .00826
98      PI      .0083 .00839 .00844 .00853 .00858 .00868 .00873 .00884 .00889 .009
99      PI      .00906 .00917 .00923 .00935 .00941 .00954 .0096 .00973 .0098 .00994
100     PI      .01001 .01016 .01024 .01039 .01047 .01064 .01072 .0109 .01099 .01118
101     PI      .01127 .01147 .01158 .01244 .01255 .01278 .0129 .01315 .01328 .01355
102     PI      .01369 .01398 .01414 .01446 .01462 .01497 .01515 .01553 .01573 .0161
103     PI      .01638 .01684 .01709 .01761 .01789 .01848 .0188 .01956 .01992 .02069
104     PI      .02111 .02201 .0225 .02357 .02415 .02544 .02616 .02777 .02867 .03072
105     PI      .0319 .03466 .03629 .04117 .04353 .04959 .05361 .06433 .07327 .10759
106     PI      .15159 .54336 .08629 .05863 .0463 .03812 .03321 .02965 .02693 .02478
107     PI      .02302 .02155 .0203 .01913 .01818 .01735 .01661 .01594 .01534 .01479
    
```

LINE	ID	1	2	3	4	5	6	7	8	9	10
108	PI	.01429	.01384	.01342	.01303	.01266	.01168	.01137	.01108	.01081	.0105
109	PI	.01031	.01009	.00987	.00967	.00947	.00929	.00911	.00895	.00879	.0086
110	PI	.00849	.00835	.00821	.00808	.00796	.00784	.00772	.00761	.0075	.0074
111	PI	.0073	.0072	.00711	.00702	.00693	.00685	.00676	.00669	.00661	.00653
112	PI	.00646	.00639	.00632	.00625	.00619	.00612	.00606	.006	.00594	.00588
113	PI	.00582	.00577	.00572	.00566	.00561	.00556	.00551	.00546	.00542	.0053
114	PI	.00533	.00528	.00524	.0052	.00516	.00512	.00507	.00504	.005	.00496
115	PI	.00492	.00489	.00485	.00482	.00478	.00475	.00472	0	0	0
116	PI	0	0	0	0	0	0	0	0	0	0
117	PI	0	0								
118	BA	0.01									
119	LS	0	69								
120	UD	0.139									
121	KK	RT1A									
122	KM	ROUTE RUNOFF FROM BASIN 1A THROUGH BASIN 1 (ALONG HW 101)									
123	RS	3	STOR	-1							
124	RC	0.02	0.02	0.02	3225	0.0068					
125	RX	0	5	10	15	20	25	30	35		
126	RY	2	2	1.5	1	1	1.5	2	2		
127	KK	1B									
128	BA	0.03									
129	LS	0	74								
130	UD	0.163									
131	KK	RT1B									
132	KM	ROUTE RUNOFF FROM BASIN 1B THROUGH BASIN 1 (ALONG ORPHEUS ST.)									
133	RS	1	STOR	-1							
134	RC	0.02	0.02	0.02	1125						
135	RX	0	5	10	15	20	25	30	35		
136	RY	2	2	1.5	1	1	1.5	2	2		
137	KK	RT1B									
138	KM	ROUTE RUNOFF FROM BASIN 1B THROUGH BASIN 1 (ALONG HW 101)									
139	RS	1	STOR	-1							
140	RC	0.02	0.02	0.02	1250						
141	RX	0	5	10	15	20	25	30	35		
142	RY	2	2	1.5	1	1	1.5	2	2		
143	KK	1									
144	BA	0.09									
145	LS	0	71								
146	UD	0.282									
147	KK	Q&1									
148	KM	COMBINE BASINS 1A, 1B AND BASIN 1									
149	HC	3									
150	KKQ1_in101										
151	KM	100-YEAR FLOW IN HYW 101 WITH 10-YR FLOWS DIVERTED TO STORM DRAIN									
152	DT	10YR_SD									
153	DI	0	15	70							
154	DQ	0	15	15							

LINE	ID	1	2	3	4	5	6	7	8	9	10
155	KK	DET_11A,1B									
156	KM	DETAIN RUNOFF FROM BASIN 1, 1B AND 1A									
157	RS	1	STOR	-1							
158	SV	2.01	3.34	4.01	5.84	9.54	11.85				
159	SQ	1	50	100	250	500	750				
160	SE	68.47	69.39	69.85	70.76	71.75	72.27				
161	KK	2									
162	BA	0.06									
163	LS	0	76								
164	UD	0.145									
165	KK	Q&2									
166	KM	COMBINE BASIN 1A AND BASIN 1 WITH BASIN 2									
167	HC	2									
168	KKQ2_in101										
169	KM	100-YEAR FLOW IN HYW 101 WITH 10-YR FLOWS DIVERTED TO STORM DRAIN									
170	DT	10YR_SD									
171	DI	0	19	130							
172	DQ	0	19	19							
173	KK	DET_2									
174	KM	DETAIN BASINS 1A, 1 AND 2									
175	RS	1	STOR	-1							
176	SV	2.17	4.58	5.69	7.93	10.6	13.16				
177	SQ	1	50	100	250	500	750				
178	SE	66.73	67.37	67.63	68.09	68.54	68.92				
179	KK	6									
180	BA	0.06									
181	LS	0	81								
182	UD	0.323									
183	KK	Q@6									
184	KM	COMBINE BASIN 1A,1B, 1 & 2 WITH BASIN 6									
185	HC	2									
186	KKQ6_in101										
187	KM	100-YEAR FLOW IN HYW 101 WITH 10-YR FLOWS DIVERTED TO STORM DRAIN									
188	DT	10YR_SD									
189	DI	0	16	250							
190	DQ	0	16	16							
191	KK	DET_6									
192	KO	0	0	0	0	21					
193	KM	DETAIN 6									
194	RS	1	STOR	-1							
195	SV	.02	.27	.43	.8	1.4	1.99				
196	SQ	1	50	100	250	500	750				
197	SE	64.16	65.03	65.31	65.81	66.38	66.85				



LINE	ID	1	2	3	4	5	6	7	8	9	10
241	KKQ5_in101										
242	KM	100-YEAR FLOW IN HYW 101 WITH 10-YR FLOWS DIVERTED TO STORM DRAIN									
243	DT	10YR_SD									
244	DI	0	9	190							
245	DQ	0	9	9							
246	KK	DET5									
247	KM	DETAIN BASIN 5									
248	KO	0	0	0	0	21					
249	RS	1	STOR	-1							
250	SV	1.35	2.32	2.8	3.92	5.58	7.1				
251	SQ	1	50	100	250	500	750				
252	SE	57.76	58.39	58.64	59.17	59.81	60.31				
253	KK	B7									
254	KM	BASIN 7									
255	BA	0.04									
256	LS	0	75								
257	UD	0.300									
258	KK	5+7									
259	KM	COMBINE BASIN 5 WITH BASIN 7									
260	HC	2									
261	KKQ7_in101										
262	KM	100-YEAR FLOW IN HYW 101 WITH 10-YR FLOWS DIVERTED TO STORM DRAIN									
263	DT	10YR_SD									
264	DI	0	6	250							
265	DQ	0	6	6							
266	KK	Q@7									
267	KM	COMBINE 3,4,5,7 AND 1,2,6 (EAST OF TRACKS)									
268	HC	2									
269	KK	DET7									
270	KM	DETAIN AT BASIN 7									
271	KO	0	0	0	0	21					
272	RS	1	STOR	-1							
273	SV	1.37	2.26	2.71	3.74	5.47	6.99				
274	SQ	1	50	100	250	500	750				
275	SE	55.22	55.79	56.03	56.49	57.15	57.66				
276	KK	B8									
277	KM	BASIN 8									
278	BA	0.06									
279	LS	0	71								
280	UD	0.090									
281	KK	Q@8									
282	KM	COMBINE ALL BASINS UP TO AND INCLUDING 8									
283	HC	2									

LINE	ID	1	2	3	4	5	6	7	8	9	10
284	KKQ8_in101										
285	KM	100-YEAR FLOW IN HYW 101 WITH 10-YR FLOWS DIVERTED TO STORM DRAIN									
286	DT	10YR_SD									
287	DI	0	4	300							
288	DQ	0	4	4							
289	KK	DET8									
290	KM	DETAIN BASIN 8									
291	KO	0	0	0	0	21					
292	RS	1	STOR	-1							
293	SV	0.72	1.44	1.79	2.6	3.97	5.1				
294	SQ	1	50	100	250	500	750				
295	SE	55.22	55.78	55.99	56.40	57.03	57.52				
296	KK	9A									
297	KM	BASIN 9A									
298	BA	0.10									
299	LS	0	71								
300	UD	0.110									
301	KK	Q@9A									
302	KM	COMBINE ALL BASINS UP TO AND INCLUDING 9A									
303	HC	2									
304	KKQ9A_in101										
305	KM	100-YEAR FLOW IN HYW 101 WITH 10-YR FLOWS DIVERTED TO STORM DRAIN									
306	DT	10YR_SD									
307	DI	0	8	405							
308	DQ	0	8	8							
309	KK	DET9A									
310	KM	DETAIN AT BASIN 9A									
311	KO	0	0	0	0	21					
312	RS	1	STOR	-1							
313	SV	1.31	3.19	4.13	6.62	10.46	13.34				
314	SQ	1	50	100	250	500	750				
315	SE	54.63	55.26	55.51	56.09	56.81	57.33				
316	KK	B9									
317	KM	BASIN 9									
318	BA	0.10									
319	LS	0	73								
320	UD	0.11									
321	KK	Q@9									
322	KM	COMBINE ALL BASINS UP TO AND INCLUDING 9									
323	HC	2									
324	KKQ9_in101										
325	KM	100-YEAR FLOW IN HYW 101 WITH 10-YR FLOWS DIVERTED TO STORM DRAIN									
326	DT	10YR_SD									
327	DI	0	14	500							
328	DQ	0	14	14							

LINE	ID	1	2	3	4	5	6	7	8	9	10
329	KK	DET9									
330	KM	DETAIN AT BASIN 9									
331	KO	0	0	0	0	21					
332	RS	1	STOR	-1							
333	SV	2.1	4.34	5.45	8.83	13.19	16.35				
334	SQ	1	50	100	250	500	750				
335	SE	54.36	55.07	55.36	56.01	56.76	57.26				
336	KK	9B									
337	KM	BASIN 9B									
338	BA	0.09									
339	LS	0	74								
340	UD	0.12									
341	KK	Q@9B									
342	KM	COMBINE ALL BASINS UP TO AND INCLUDING 9B									
343	HC	2									
344	KKQ9B_in101										
345	KM	100-YEAR FLOW IN HYW 101 WITH 10-YR FLOWS DIVERTED TO STORM DRAIN									
346	DT	10YR_SD									
347	DI	0	10	595							
348	DQ	0	10	10							
349	KK	DET9B									
350	KM	DETAIN AT BASIN 9B									
351	KO	0	0	0	0	21					
352	RS	1	STOR	-1							
353	SV	0.18	2.06	3.55	7.78	12.26	15.3				
354	SQ	1	50	100	250	500	750				
355	SE	54.03	54.63	54.98	55.85	56.63	57.12				
356	KK	B10									
357	KM	BASIN 10									
358	BA	0.05									
359	LS	0	73								
360	UD	0.09									
361	KK	Q@10									
362	KM	COMBINE ALL BASINS UP TO AND INCLUDING 10									
363	HC	2									
364	KKQ10_in101										
365	KM	100-YEAR FLOW IN HYW 101 WITH 10-YR FLOWS DIVERTED TO STORM DRAIN									
366	DT	10YR_SD									
367	DI	0	2	625							
368	DQ	0	2	2							
369	KK	DET10									
370	KM	DETAIN AT BASIN 10									
371	KO	0	0	0	0	21					
372	RS	1	STOR	-1							
373	SV	0.22	1.16	1.86	3.83	5.97	7.37				
374	SQ	1	50	100	250	500	750				



SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT

LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
72	1A	
	V	
	V	
121	RT1A	
	.	
	.	
127	.	1B
	.	V
	.	V
131	.	RT1B
	.	V
	.	V
137	.	RT1B
	.	.
	.	.
143	.	.
	.	1
	.	.
	.	.
147	Q&1.....	
	.	
	.	
152	.	-----> 10YR_SD
150	Q1_in101	
	V	
	V	
155	DET_1	
	.	
	.	
161	.	2
	.	.
	.	.
165	Q&2.....	
	.	
	.	
170	.	-----> 10YR_SD
168	Q2_in101	
	V	
	V	
173	DET_2	
	.	
	.	
179	.	6
	.	.
	.	.
183	Q@6.....	
	.	
	.	
188	.	-----> 10YR_SD
186	Q6_in101	
	V	
	V	
191	DET_6	
	.	

```
198 .          B3
.          .
.          .
204 .          .-----> 10YR_SD
202 .    Q3_in101
.          V
.          V
207 .          DET3
.          .
.          .
214 .          .          B4
.          .          .
.          .          .
218 .          3+4.....
.          .
.          .
223 .          .-----> 10YR_SD
221 .    Q4_in101
.          V
.          V
226 .          DET4
.          .
.          .
233 .          .          B5
.          .          .
.          .          .
238 .          Q@5.....
.          .
.          .
243 .          .-----> 10YR_SD
241 .    Q5_in101
.          V
.          V
246 .          DET5
.          .
.          .
253 .          .          B7
.          .          .
.          .          .
258 .          5+7.....
.          .
.          .
263 .          .-----> 10YR_SD
261 .    Q7_in101
.          .
.          .
266 .    Q@7.....
.          V
.          V
269 .    DET7
.          .
.          .
276 .          .          B8
.          .          .
.          .          .
281 .    Q@8.....
.          .
.          .
286 .          .-----> 10YR_SD
```

284 Q8\_in101  
V  
V  
289 DET8  
. .  
296 . 9A  
. .  
301 Q@9A.....  
. .  
306 .-----> 10YR\_SD  
304 Q9A\_in10  
V  
V  
309 DET9A  
. .  
316 . B9  
. .  
321 Q@9.....  
. .  
326 .-----> 10YR\_SD  
324 Q9\_in101  
V  
V  
329 DET9  
. .  
336 . 9B  
. .  
341 Q@9B.....  
. .  
346 .-----> 10YR\_SD  
344 Q9B\_in10  
V  
V  
349 DET9B  
. .  
356 . B10  
. .  
361 Q@10.....  
. .  
366 .-----> 10YR\_SD  
364 Q10\_in10  
V  
V  
369 DET10  
. .  
376 . B11  
. .

```
381      Q@11.....  
      .  
      .  
386      .-----> 10YR_SD  
384      Q11_in10  
      V  
      V  
389      DET11
```

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

\*\*\*\*\*  
\*  
\* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
\* JUN 1998 \*  
\* VERSION 4.1 \*  
\*  
\* RUN DATE 17AUG04 TIME 14:40:45 \*  
\*  
\*\*\*\*\*

\*\*\*\*\*  
\*  
\* U.S. ARMY CORPS OF ENGINEERS  
\* HYDROLOGIC ENGINEERING CENTER  
\* 609 SECOND STREET  
\* DAVIS, CALIFORNIA 95616  
\* (916) 756-1104  
\*  
\*\*\*\*\*

\*\*\*\*\*  
ENCINITAS COAST HWY 101 J-14413 7-13-04  
SAME AS BELOW EXCPET 100-YEAR DETAINED  
DIVERTED 10-YEAR STORM TO STORM DRAIN  
CHANGED FILE NAME  
FN: 100A4.HC1  
\*\*\*\*\*  
ENCINITAS COAST HWY 101 J-14413 7-13-04  
100-YEAR UNDETAINED W/PIPE ROUTING BETWEEN BASINS  
SAME AS BELOW BUT DIVERTED 10-YEAR STORM TO STORM DRAIN  
CHANGED FILE NAME  
FN: 100UDTDV.HC1  
\*\*\*\*\*  
ENCINITAS COAST HWY 101 J-14413 5-27-04  
100-YEAR UNDETAINED W/PIPE ROUTING BETWEEN BASINS  
FN: 100UD.HC1  
\*\*\*\*\*  
ENCINITAS COAST HWY 101 J-14413 3-24-04  
REMOVED STORAGE IN BASINS 1 &2  
FN: 100UD.HC1  
\*\*\*\*\*  
ENCINITAS COAST HWY 101 J-14413 1-08-04  
SAME AS BELOW BUT CHANGED ROUTING TO MATCH DETAINED 100-YR  
RUN (100DET3.HC1) BUT WITHOUT DETENTION  
FN: 100UD.HC1  
\*\*\*\*\*  
ENCINITAS COAST HWY 101 J-14413 1-07-04  
SAME AS BELOW BUT CHANGED PI CARDS (INCREASED BASIN AREA)  
FN: 100R.HC1  
\*\*\*\*\*  
ENCINITAS COAST HWY 101 J-14413 12/29/03  
100-YEAR RUN WITH BASIN AREAS EXTENDED TO THE RIDGE EAST OF  
THE RR TRACKS. PI CARDS CHANGED FOR 100-YR BASED ON FN: E100.HC1  
LAG AND CURVE NUMBERS CHANGED FOR 100-YEAR.  
BASIN AREAS ALSO CHANGED FOR 7 THROUGH 11.  
\*\*\*\*\*  
ENCINITAS COAST HWY 101  
J-14413  
SEPT 25, 2003  
MODIFIED EXISTING RUN TO MODEL PROPOSED DETENTION OF BASINS  
1A, 1B, 1, 2, 3, 4, 5, 6, AND 8  
DETENTION CARDS SA/SV, SQ, SE OBTAINED FROM FN: DSI\_5R.HC1  
\*\*\*\*\*  
ENCINITAS- COAST HIGHWAY 101  
JOB # 14413  
09-12-03

MODIFIED PUMP Q TO 1.7 CFS, AND ROUTING OF BASINS 9A, 9B, AND 9  
FROM PUMP STATION THROUGH 10" LATERAL, CONFLUENCING  
WITH MAIN LINE AT AT CONNECTION 3 INSTEAD OF CONNECTION 2  
ALSO CHANGED ROUTING THROUGH MAIN LINE FROM LINE G TO CONNECTION  
2, TO LINE G TO CONNECTION 3

\*\*\*\*\*

ENCINITAS- COAST HIGHWAY 101

JOB # 14413

09-04-03

MODIFIED CURVE NUMBER AND REMOVED % IMPERVIOUS

\*\*\*\*\*

ENCINITAS- COAST HIGHWAY 101

JOB # 14413

06-03-03

POST-IMPROVEMENT (EXISTING) CONDITION FN: 101EX\_5.HC1

5-YEAR, 24-HR STORM EVENT

LAG CALCULATION ARE BASED OFF OF NRCS METHOD

AND ARE A FUNCTION OF RUNOFF COEF. AND VELOCITY

NESTED STORM PER COUNTY OF SAN DIEGO HYDROLOGY MANUAL

COPYRIGHT 2003 RICK ENGINEERING COMPANY

6HR RAINFALL IS 1.6 INCHES

24HR RAINFALL IS 2.5 INCHES

TOTAL BASIN AREA IS .5 SQUARE MILES

71 IO OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA

NMIN 5 MINUTES IN COMPUTATION INTERVAL  
IDATE 1JAN90 STARTING DATE  
ITIME 1200 STARTING TIME  
NQ 300 NUMBER OF HYDROGRAPH ORDINATES  
NDDATE 2JAN90 ENDING DATE  
NDTIME 1255 ENDING TIME  
ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS

TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES  
PRECIPITATION DEPTH INCHES  
LENGTH, ELEVATION FEET  
FLOW CUBIC FEET PER SECOND  
STORAGE VOLUME ACRE-FEET  
SURFACE AREA ACRES  
TEMPERATURE DEGREES FAHRENHEIT

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72 KK \* 1A \*

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73 KO

OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	300	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

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 \* DET\_6 \*  
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191 KK

192 KO

OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	300	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

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 \* DET3 \*  
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207 KK

209 KO

OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	300	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

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\* DET4 \*  
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226 KK

228 KO

OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE  
IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
ISAV2 300 LAST ORDINATE PUNCHED OR SAVED  
TIMINT .083 TIME INTERVAL IN HOURS

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\* DET5 \*  
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246 KK

248 KO

OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE  
IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
ISAV2 300 LAST ORDINATE PUNCHED OR SAVED  
TIMINT .083 TIME INTERVAL IN HOURS

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\* DET7 \*  
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269 KK

271 KO

OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE  
IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
ISAV2 300 LAST ORDINATE PUNCHED OR SAVED  
TIMINT .083 TIME INTERVAL IN HOURS

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289 KK \* DET8 \*  
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291 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE  
IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
ISAV2 300 LAST ORDINATE PUNCHED OR SAVED  
TIMINT .083 TIME INTERVAL IN HOURS

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309 KK \* DET9A \*  
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311 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE  
IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
ISAV2 300 LAST ORDINATE PUNCHED OR SAVED  
TIMINT .083 TIME INTERVAL IN HOURS

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329 KK \* DET9 \*  
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331 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL

QSCAL 0. HYDROGRAPH PLOT SCALE  
IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
ISAV2 300 LAST ORDINATE PUNCHED OR SAVED  
TIMINT .083 TIME INTERVAL IN HOURS

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349 KK \* DET9B \*  
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351 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE  
IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
ISAV2 300 LAST ORDINATE PUNCHED OR SAVED  
TIMINT .083 TIME INTERVAL IN HOURS

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369 KK \* DET10 \*  
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371 KO OUTPUT CONTROL VARIABLES  
IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE  
IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
ISAV2 300 LAST ORDINATE PUNCHED OR SAVED  
TIMINT .083 TIME INTERVAL IN HOURS

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389 KK \* DET11 \*  
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391 KO

OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	300	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	1A	9.	16.08	1.	0.	0.	.01		
ROUTED TO	RT1A	6.	16.42	1.	0.	0.	.01	1.31	16.42
HYDROGRAPH AT	1B	31.	16.08	4.	1.	1.	.03		
ROUTED TO	RT1B	0.	.00	0.	0.	0.	.03	5.63	24.92
ROUTED TO	RT1B	0.	.00	0.	0.	0.	.03	2.00	.00
HYDROGRAPH AT	1	62.	16.25	11.	3.	3.	.09		
3 COMBINED AT	Q&1	67.	16.25	12.	4.	4.	.13		
DIVERSION TO	10YR_SD	15.	16.25	8.	3.	3.	.13		
HYDROGRAPH AT	Q1_in101	52.	16.25	4.	1.	1.	.13		
ROUTED TO	DET_1	13.	16.67	2.	1.	1.	.13	68.70	16.67
HYDROGRAPH AT	2	72.	16.08	9.	3.	3.	.06		
2 COMBINED AT	Q&2	73.	16.08	11.	4.	4.	.19		
DIVERSION TO	10YR_SD	19.	16.08	9.	3.	3.	.19		
HYDROGRAPH AT	Q2_in101	54.	16.08	3.	1.	1.	.19		
ROUTED TO	DET_2	1.	.08	1.	1.	1.	.19	66.73	.00
HYDROGRAPH AT	6	55.	16.25	11.	3.	3.	.06		
2 COMBINED AT	Q@6	56.	16.25	12.	4.	4.	.25		
DIVERSION TO	10YR_SD	16.	16.25	8.	4.	4.	.25		
HYDROGRAPH AT	Q6_in101	40.	16.25	3.	1.	1.	.25		
ROUTED TO	DET_6	38.	16.33	4.	2.	2.	.25	64.82	16.33
HYDROGRAPH AT	B3	30.	16.08	3.	1.	1.	.02		
DIVERSION TO	10YR_SD	11.	16.08	3.	1.	1.	.02		
HYDROGRAPH AT	Q3_in101	19.	16.08	1.	0.	0.	.02		
ROUTED TO	DET3	1.	.08	1.	1.	1.	.02	59.68	.00
HYDROGRAPH AT	B4	27.	16.00	3.	1.	1.	.02		
2 COMBINED AT	3+4	28.	16.00	4.	2.	2.	.04		

DIVERSION TO	10YR_SD	7.	16.00	3.	2.	2.	.04		
HYDROGRAPH AT	Q4_in101	21.	16.00	1.	0.	0.	.04		
ROUTED TO	DET4	1.	.08	1.	1.	1.	.04	59.54	.00
HYDROGRAPH AT	B5	28.	16.08	3.	1.	1.	.02		
2 COMBINED AT	Q@5	29.	16.08	4.	2.	2.	.06		
DIVERSION TO	10YR_SD	9.	16.08	3.	2.	2.	.06		
HYDROGRAPH AT	Q5_in101	20.	16.08	1.	0.	0.	.06		
ROUTED TO	DET5	1.	.08	1.	1.	1.	.06	57.76	.00
HYDROGRAPH AT	B7	31.	16.25	6.	2.	2.	.04		
2 COMBINED AT	5+7	32.	16.25	7.	3.	3.	.10		
DIVERSION TO	10YR_SD	6.	16.25	4.	2.	2.	.10		
HYDROGRAPH AT	Q7_in101	26.	16.25	2.	1.	1.	.10		
2 COMBINED AT	Q@7	62.	16.33	6.	2.	2.	.35		
ROUTED TO	DET7	47.	16.50	6.	2.	2.	.35	55.75	16.50
HYDROGRAPH AT	B8	69.	16.08	7.	2.	2.	.06		
2 COMBINED AT	Q@8	78.	16.08	14.	5.	4.	.41		
DIVERSION TO	10YR_SD	4.	16.08	4.	2.	2.	.41		
HYDROGRAPH AT	Q8_in101	74.	16.08	10.	2.	2.	.41		
ROUTED TO	DET8	50.	16.58	9.	3.	3.	.41	55.78	16.58
HYDROGRAPH AT	9A	114.	16.08	12.	4.	4.	.10		
2 COMBINED AT	Q@9A	136.	16.08	21.	7.	6.	.51		
DIVERSION TO	10YR_SD	8.	16.08	7.	3.	3.	.51		
HYDROGRAPH AT	Q9A_in10	128.	16.08	14.	4.	3.	.51		
ROUTED TO	DET9A	51.	16.67	12.	4.	4.	.51	55.27	16.67
HYDROGRAPH AT	B9	123.	16.08	13.	4.	4.	.10		
2 COMBINED AT	Q@9	130.	16.08	25.	8.	8.	.61		
DIVERSION TO	10YR_SD	14.	16.08	10.	4.	4.	.61		
HYDROGRAPH AT	Q9_in101	116.	16.08	15.	4.	4.	.61		
ROUTED TO	DET9	44.	16.92	13.	4.	4.	.61	54.98	16.92
HYDROGRAPH AT	9B	111.	16.08	12.	4.	4.	.09		

2 COMBINED AT	Q@9B	112.	16.08	25.	8.	8.	.70		
DIVERSION TO	10YR_SD	10.	16.08	9.	4.	4.	.70		
HYDROGRAPH AT	Q9B_in10	102.	16.08	17.	4.	4.	.70		
ROUTED TO	DET9B	46.	16.50	17.	5.	5.	.70	54.58	16.50
HYDROGRAPH AT	B10	62.	16.08	7.	2.	2.	.05		
2 COMBINED AT	Q@10	86.	16.08	23.	7.	7.	.75		
DIVERSION TO	10YR_SD	2.	16.08	2.	2.	1.	.75		
HYDROGRAPH AT	Q10_in10	84.	16.08	21.	5.	5.	.75		
ROUTED TO	DET10	56.	16.33	21.	6.	6.	.75	54.51	16.33
HYDROGRAPH AT	B11	141.	16.08	18.	6.	5.	.12		
2 COMBINED AT	Q@11	179.	16.08	39.	12.	11.	.87		
DIVERSION TO	10YR_SD	19.	16.08	15.	6.	6.	.87		
HYDROGRAPH AT	Q11_in10	160.	16.08	23.	6.	6.	.87		
ROUTED TO	DET11	138.	16.25	23.	7.	6.	.87	51.72	16.25

\*\*\* NORMAL END OF HEC-1 \*\*\*

**ATTACHMENT 2**

**ALTERNATIVE 4**

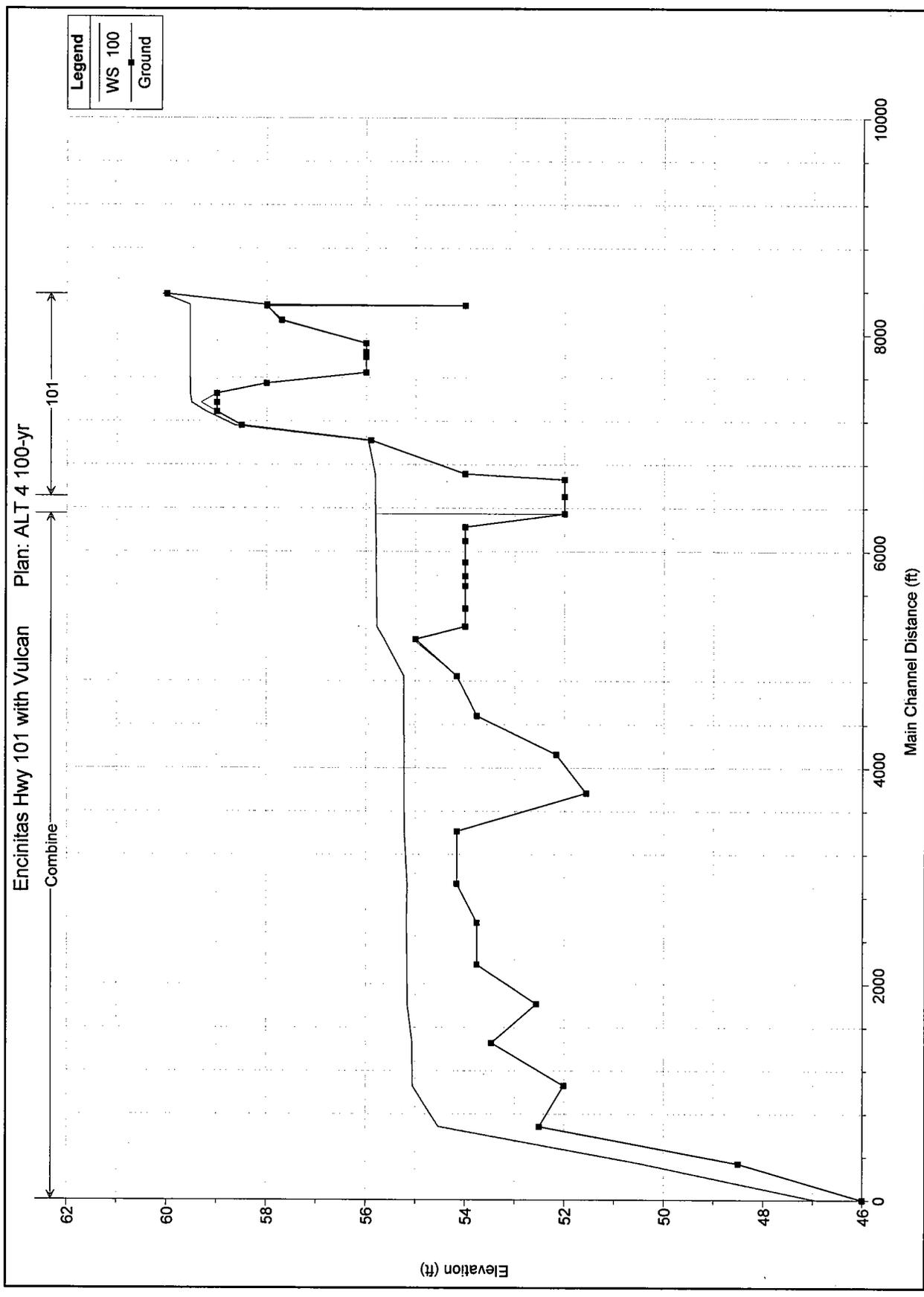
**100-YEAR HEC-RAS ANALYSIS**

HEC-RAS Plan: 100A4 Profile: 100

Reach	River Sta	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Vulcan	3300.14	13.00	72.16	72.59	72.59	72.79	0.023812	3.71	3.58	8.85	1.00
Vulcan	3200.15	13.00	71.16	71.88	71.58	71.95	0.003891	2.14	6.30	9.40	0.44
Vulcan	3100.16	13.00	70.76	71.44	71.19	71.51	0.004919	2.29	5.86	9.35	0.49
Vulcan	3000.17	13.00	70.26	70.93	70.69	71.01	0.005168	2.33	5.77	9.33	0.50
Vulcan	2900.18	13.00	69.76	70.47	70.19	70.54	0.004234	2.19	6.14	9.41	0.46
Vulcan	2800.19	13.00	69.26	69.83	69.69	69.94	0.008797	2.74	4.88	9.14	0.64
Vulcan	2700.20	13.00	67.96	68.39	68.39	68.59	0.022845	3.66	3.63	8.86	0.98
Vulcan	2600.21	13.00	65.96	66.85	66.39	66.90	0.001875	1.71	7.95	9.79	0.32
Vulcan	2500.22	13.00	64.46	66.86	64.89	66.87	0.000057	0.58	25.01	12.81	0.07
Vulcan	2400.23	13.00	63.96	66.86	64.39	66.87	0.000029	0.46	31.66	13.81	0.05
Vulcan	2300.24	13.00	63.46	66.86	63.89	66.87	0.000016	0.38	38.81	14.81	0.04
Vulcan	2200.25	13.00	62.96	66.86	63.39	66.87	0.000012	0.36	46.96	32.44	0.03
Vulcan	2100.26	13.00	62.46	66.86	62.89	66.86	0.000002	0.16	129.37	82.28	0.01
Vulcan	245	13.00	64.00	66.86		66.86	0.000003	0.15	118.42	81.57	0.02
Vulcan	240	1.00	64.00	66.86		66.86	0.000000	0.01	160.35	114.77	0.00
Vulcan	235	1.00	66.00	66.86		66.86	0.000000	0.01	121.00	155.23	0.00
Vulcan	230	1.00	66.00	66.86		66.86	0.000000	0.01	132.43	171.70	0.00
Vulcan	225	1.00	66.00	66.86		66.86	0.000000	0.01	93.65	119.89	0.00
Vulcan	220	1.00	66.00	66.86		66.86	0.000000	0.00	271.66	333.13	0.00
Vulcan	215	1.00	67.90	66.83	66.83	66.86	0.014435		0.68	9.90	0.00
Vulcan	195	38.00	68.00	66.71	66.27	66.72	0.000260		47.12	84.98	0.00
Vulcan	175	38.00	65.50	66.37	66.37	66.48	0.004576	3.64	18.56	85.07	0.81
Vulcan	165	38.00	63.00	64.57	64.02	64.62	0.000608	1.90	21.04	24.51	0.33
Vulcan	150	38.00	63.00	63.86	63.86	64.07	0.007780	3.71	10.24	23.94	1.00
101	230	1.00	60.00	60.08	60.08	60.10	0.017075	1.12	0.89	22.55	1.00
101	225.3	1.00	58.00	59.54	58.03	59.54	0.000000	0.01	79.95	70.52	0.00
101	225.2	1.00	54.64	59.54		59.54	0.000000	0.01	158.06	70.52	0.00
101	225.1	1.00	58.00	59.54		59.54	0.000000	0.01	79.94	70.52	0.00
101	220	1.00	57.75	59.54		59.54	0.000000	0.01	141.80	110.60	0.00
101	215	1.00	56.00	59.54		59.54	0.000000	0.00	402.07	160.61	0.00
101	210	1.00	56.00	59.54		59.54	0.000000	0.00	286.25	92.35	0.00
101	205	1.00	56.00	59.54		59.54	0.000000	0.00	354.55	114.90	0.00
101	195	1.00	56.00	59.54		59.54	0.000000	0.01	188.18	102.50	0.00
101	190	1.00	58.00	59.54		59.54	0.000000	0.01	122.09	90.00	0.00
101	185	1.00	59.00	59.54		59.54	0.000002	0.05	18.44	50.00	0.02
101	180	1.00	59.32	59.51	59.49	59.54	0.008400	1.38	0.73	7.81	0.80

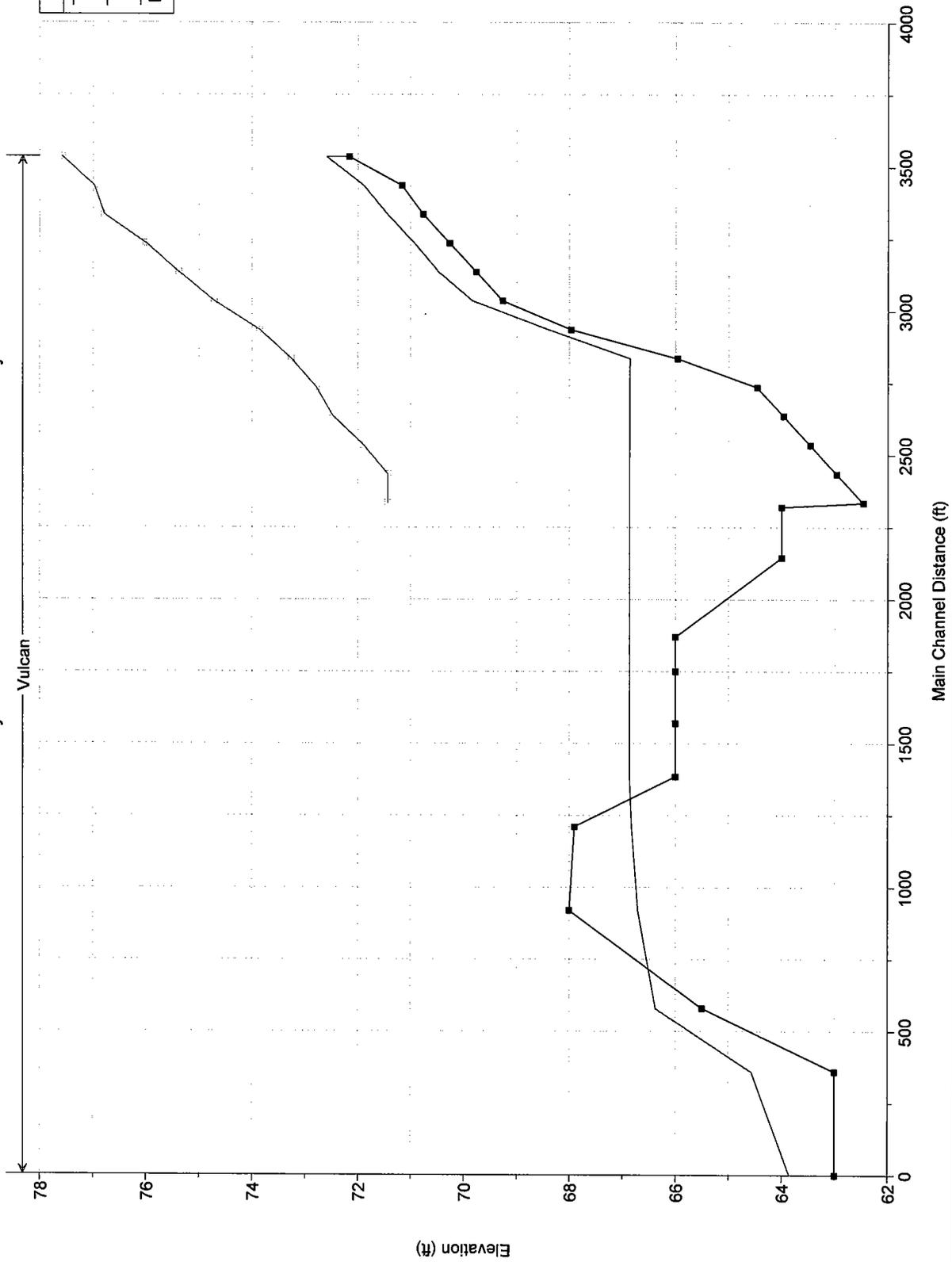
HEC-RAS Plan: 100A4 Profile: 100 (Continued)

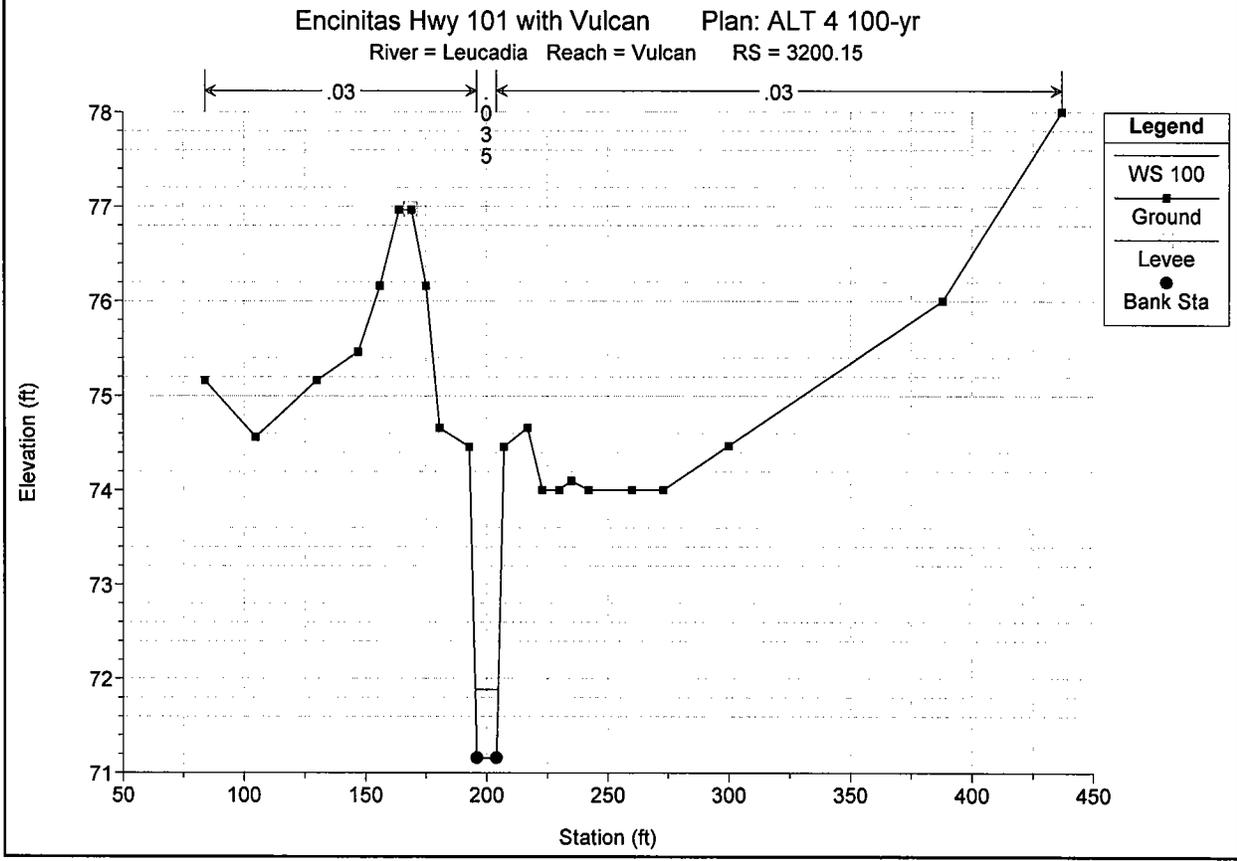
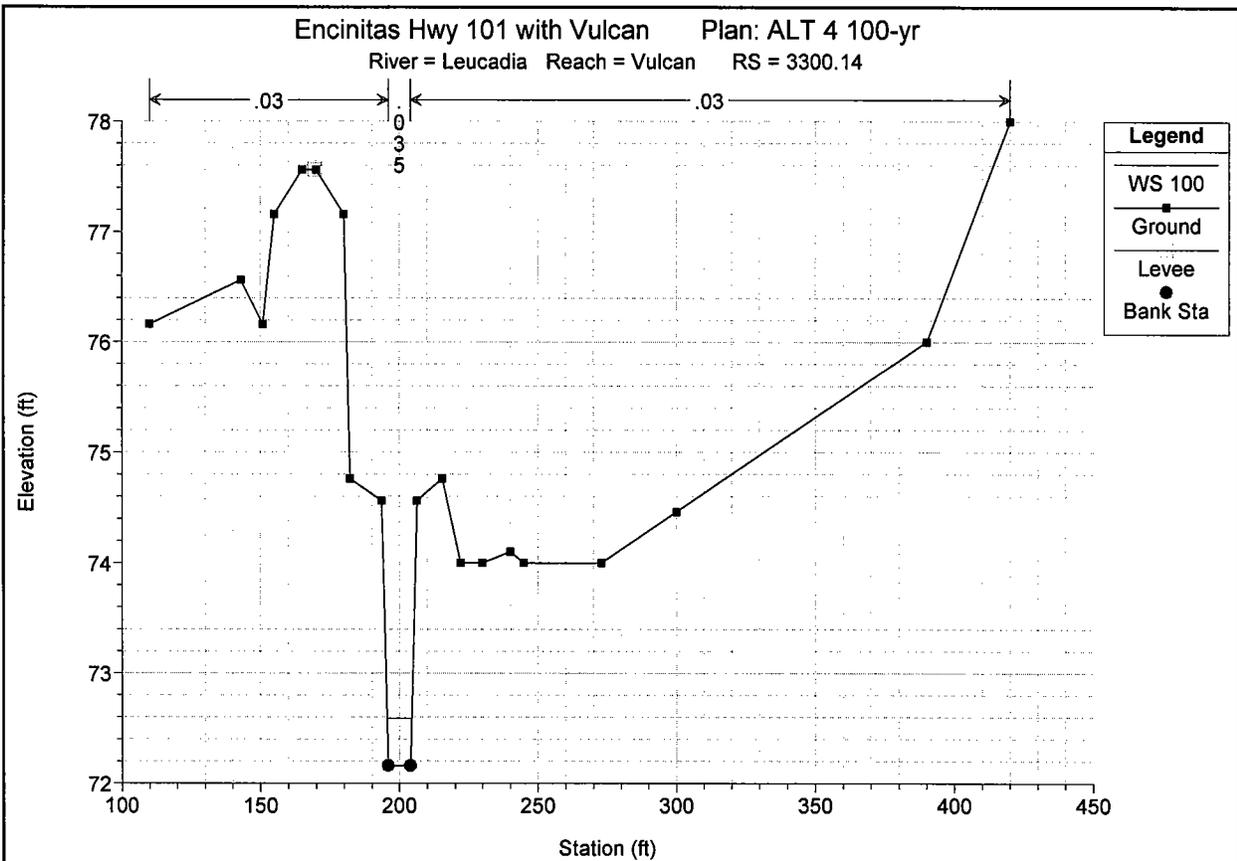
Reach	River Sta	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude #	Chl
101	175	1.00	59.00	59.21	59.14	59.22	0.002048	0.80	1.25	10.64	0.41	0.41
101	170	1.00	58.50	58.64	58.64	58.68	0.014397	1.53	0.65	9.21	1.01	1.01
101	165	1.00	55.90	55.96	55.96	55.98	0.028200	1.16	0.86	30.15	1.22	1.22
101	160	1.00	54.00	55.82	54.15	55.82	0.000000	0.01	93.12	92.91	0.00	0.00
101	150	1.00	52.00	55.82		55.82	0.000000	0.00	258.07	123.56	0.00	0.00
101	145	1.00	52.00	55.81		55.81	0.000000	0.01	140.95	60.00	0.00	0.00
Combine	140	47.00	52.00	55.81	52.75	55.81	0.000006	0.37	129.31	51.80	0.04	0.04
Combine	135	47.00	54.00	55.81		55.81	0.000004	0.22	253.27	197.37	0.03	0.03
Combine	130	47.00	54.00	55.80		55.81	0.000055	0.81	68.16	62.33	0.11	0.11
Combine	125	47.00	54.00	55.80		55.80	0.000005	0.26	213.84	151.85	0.03	0.03
Combine	120	50.00	54.00	55.79		55.80	0.000047	0.70	83.49	87.54	0.09	0.09
Combine	115	50.00	54.00	55.79		55.80	0.000045	0.69	84.01	93.24	0.09	0.09
Combine	110	50.00	54.00	55.79		55.79	0.000011	0.34	179.19	154.71	0.04	0.04
Combine	105	51.00	54.00	55.78		55.78	0.000047	0.71	106.18	139.97	0.09	0.09
Combine	100	51.00	55.06	55.63	55.63	55.75	0.009946	2.80	18.22	77.65	1.02	1.02
Combine	95	51.00	54.16	55.23	54.63	55.24	0.000162	0.80	68.85	103.07	0.16	0.16
Combine	90	44.00	53.76	55.23		55.23	0.000006	0.24	210.10	174.50	0.03	0.03
Combine	85	44.00	52.16	55.23		55.23	0.000001	0.17	314.20	158.78	0.02	0.02
Combine	80	44.00	51.56	55.23		55.23	0.000002	0.20	297.66	185.32	0.02	0.02
Combine	75	46.00	54.16	55.22		55.23	0.000036	0.41	115.34	143.68	0.08	0.08
Combine	70	46.00	54.16	55.17		55.18	0.000390	1.04	50.38	148.08	0.24	0.24
Combine	65	46.00	53.76	55.17		55.17	0.000003	0.16	303.16	274.84	0.03	0.03
Combine	60	56.00	53.76	55.16		55.17	0.000091	0.77	78.12	89.81	0.13	0.13
Combine	55	56.00	52.56	55.16		55.16	0.000011	0.41	197.50	187.99	0.05	0.05
Combine	50	138.00	53.46	55.06		55.13	0.000569	2.09	68.67	61.11	0.33	0.33
Combine	45	138.00	52.01	55.06		55.06	0.000048	1.08	195.69	142.19	0.11	0.11
Combine	40	138.00	52.50	54.53	54.53	54.96	0.006610	5.27	26.18	30.75	1.01	1.01
Combine	35	138.00	48.50	50.45	50.72	51.34	0.018364	7.57	18.22	27.28	1.63	1.63
Combine	30	138.00	46.00	46.94	47.02	47.51	0.007407	6.15	23.06	25.94	1.12	1.12

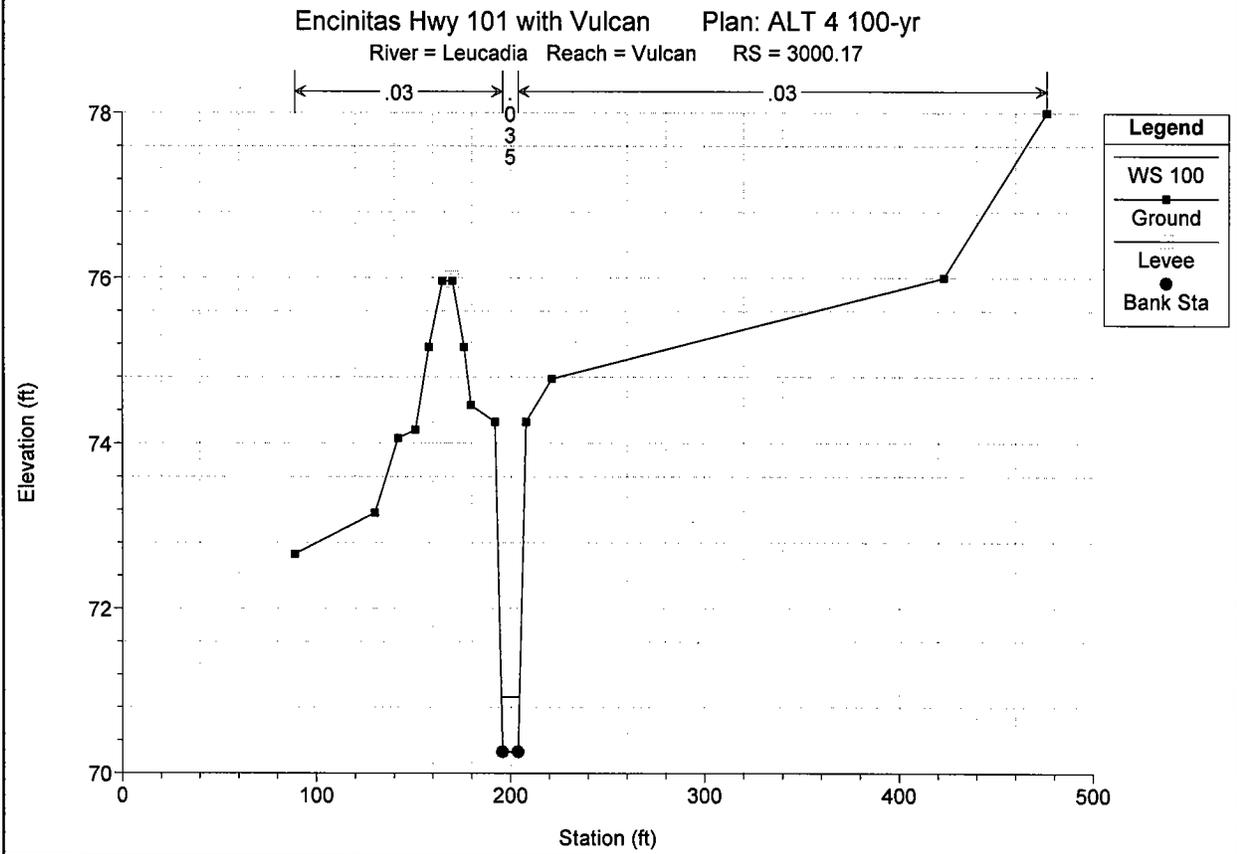
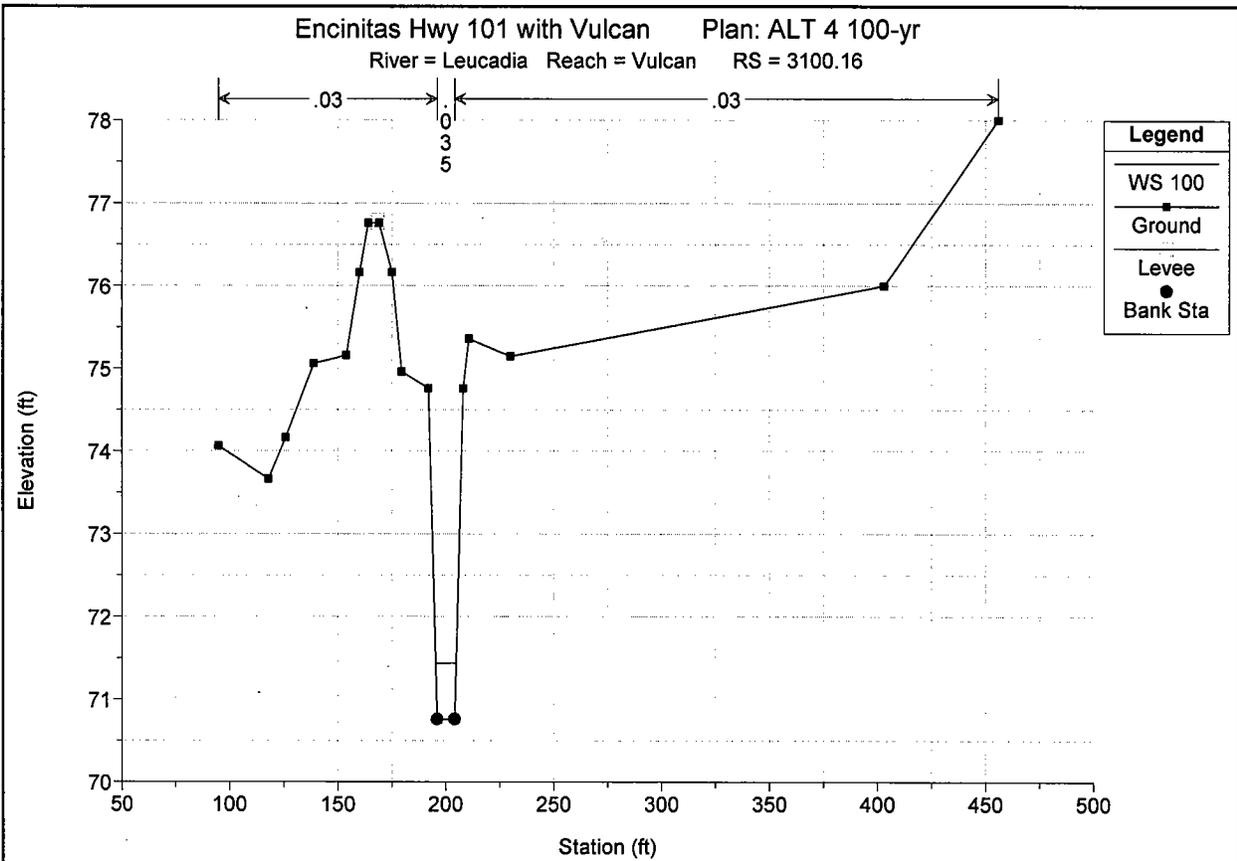


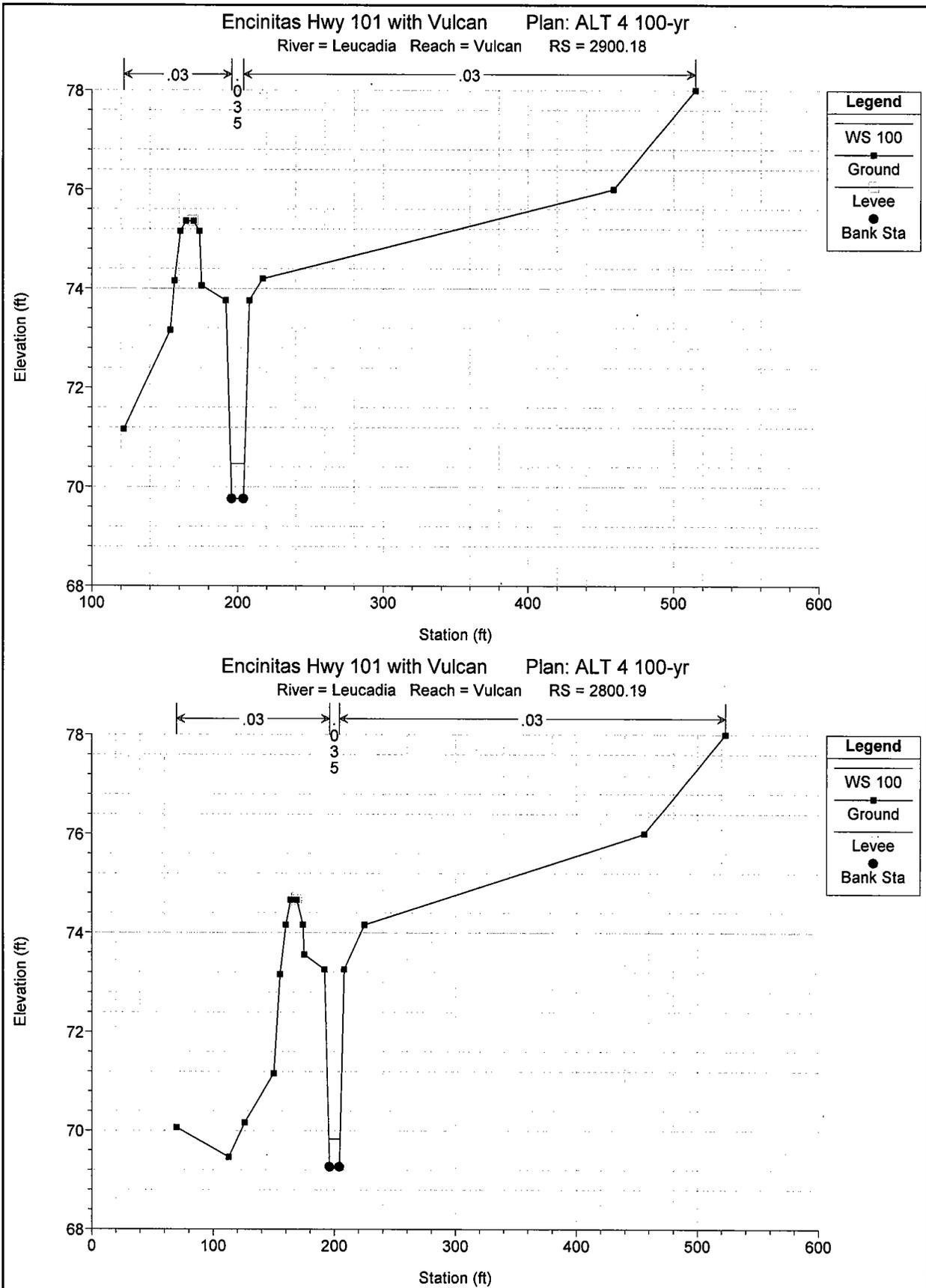
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr

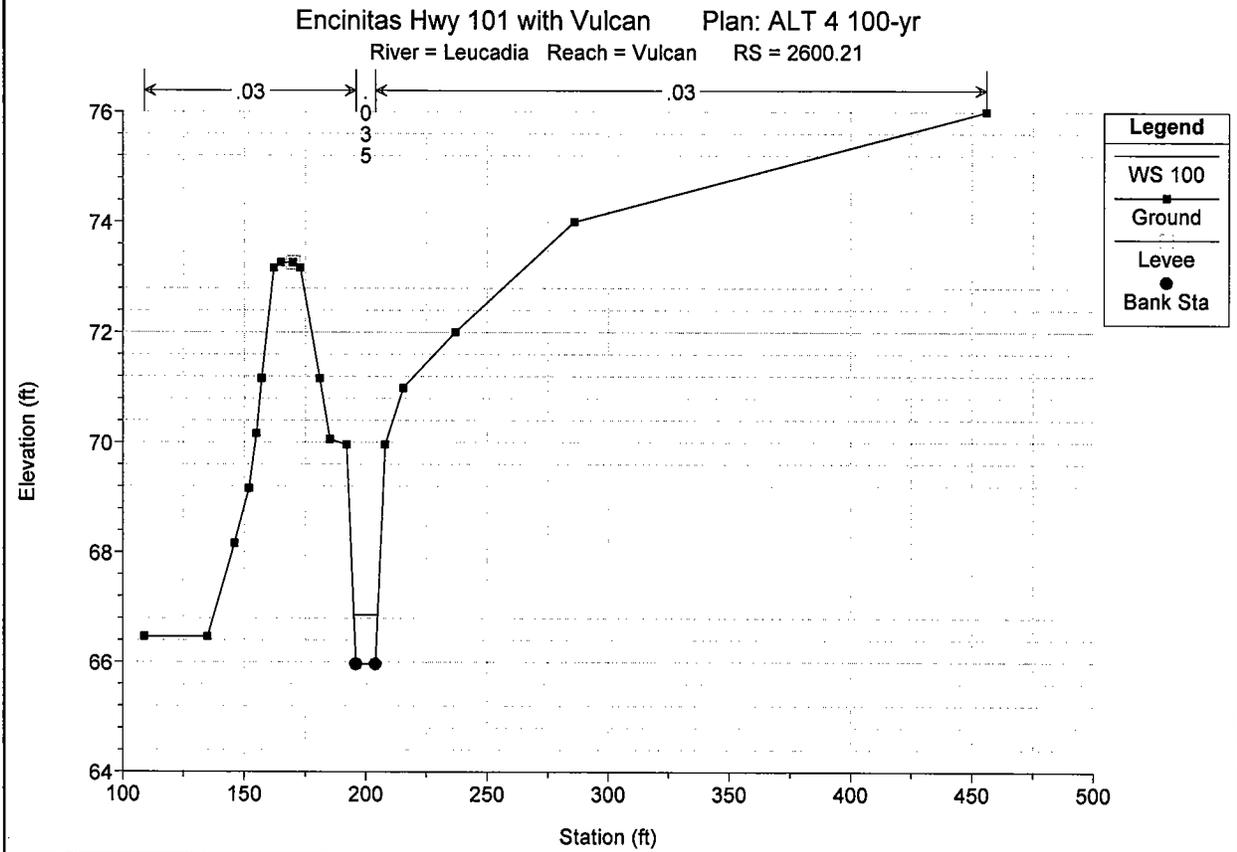
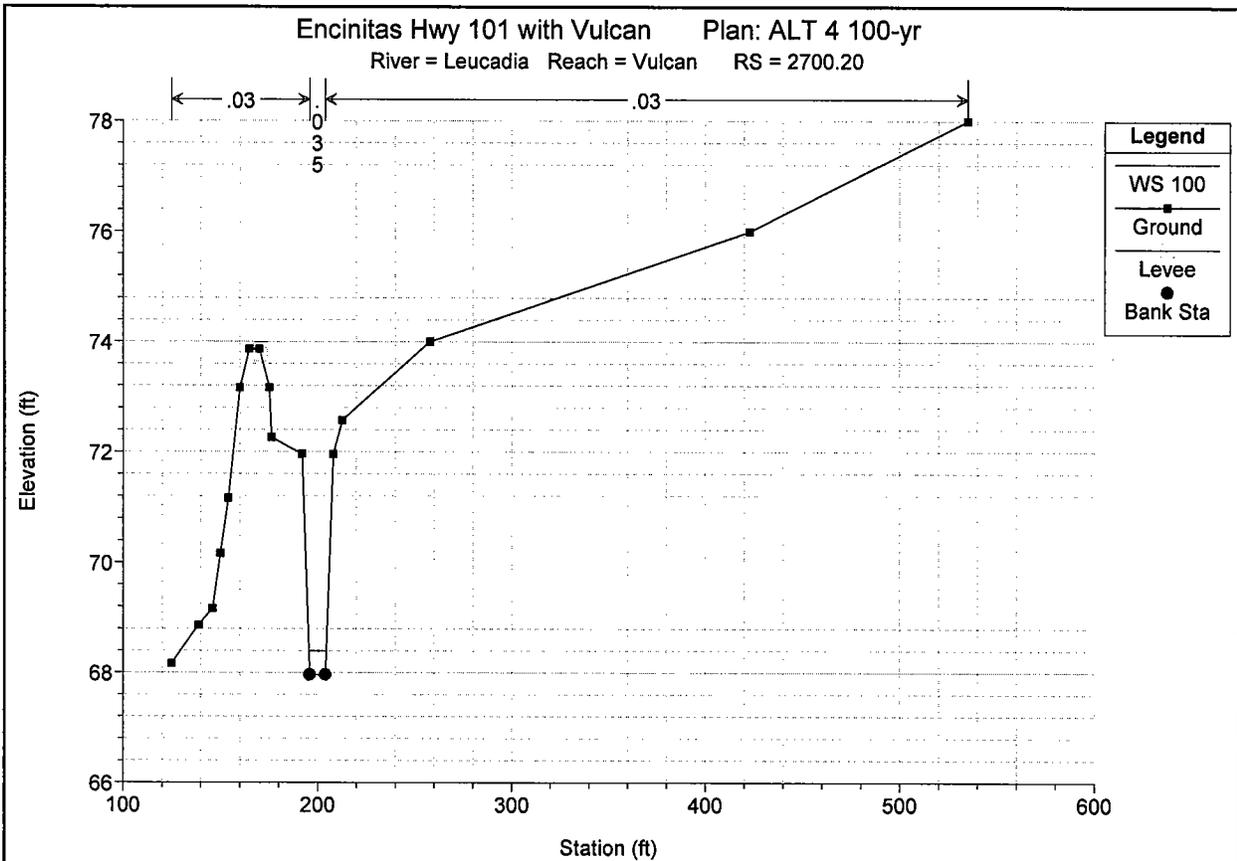
Legend	
—	WS 100
—■—	Ground
—	Left Levee

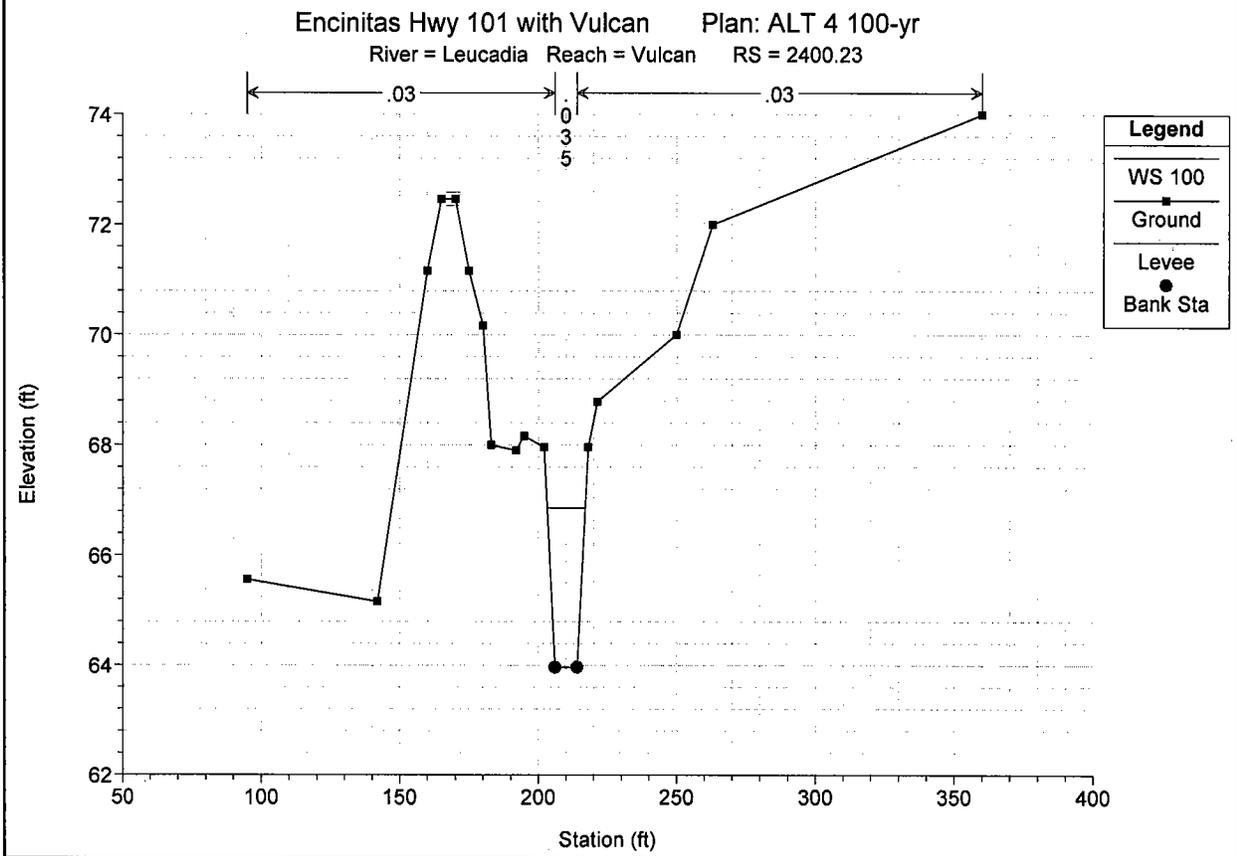
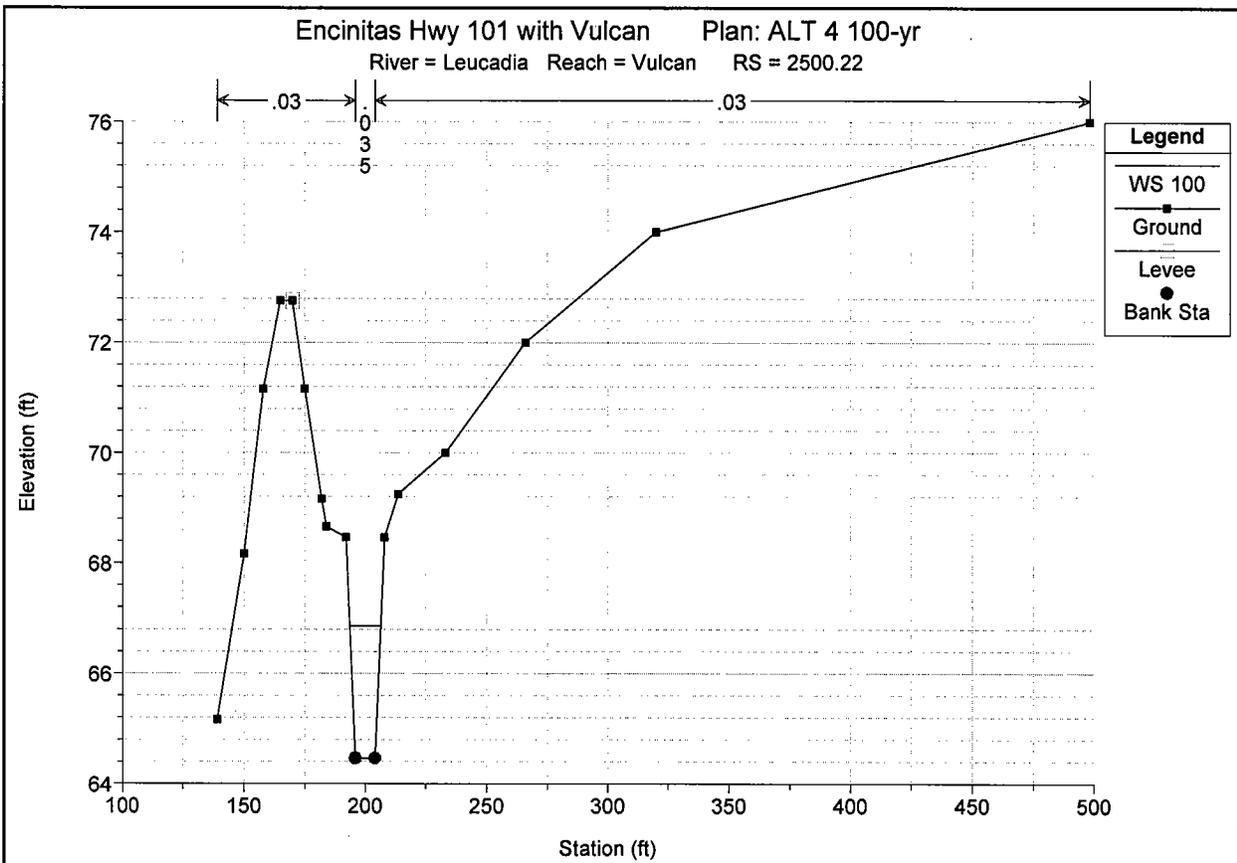


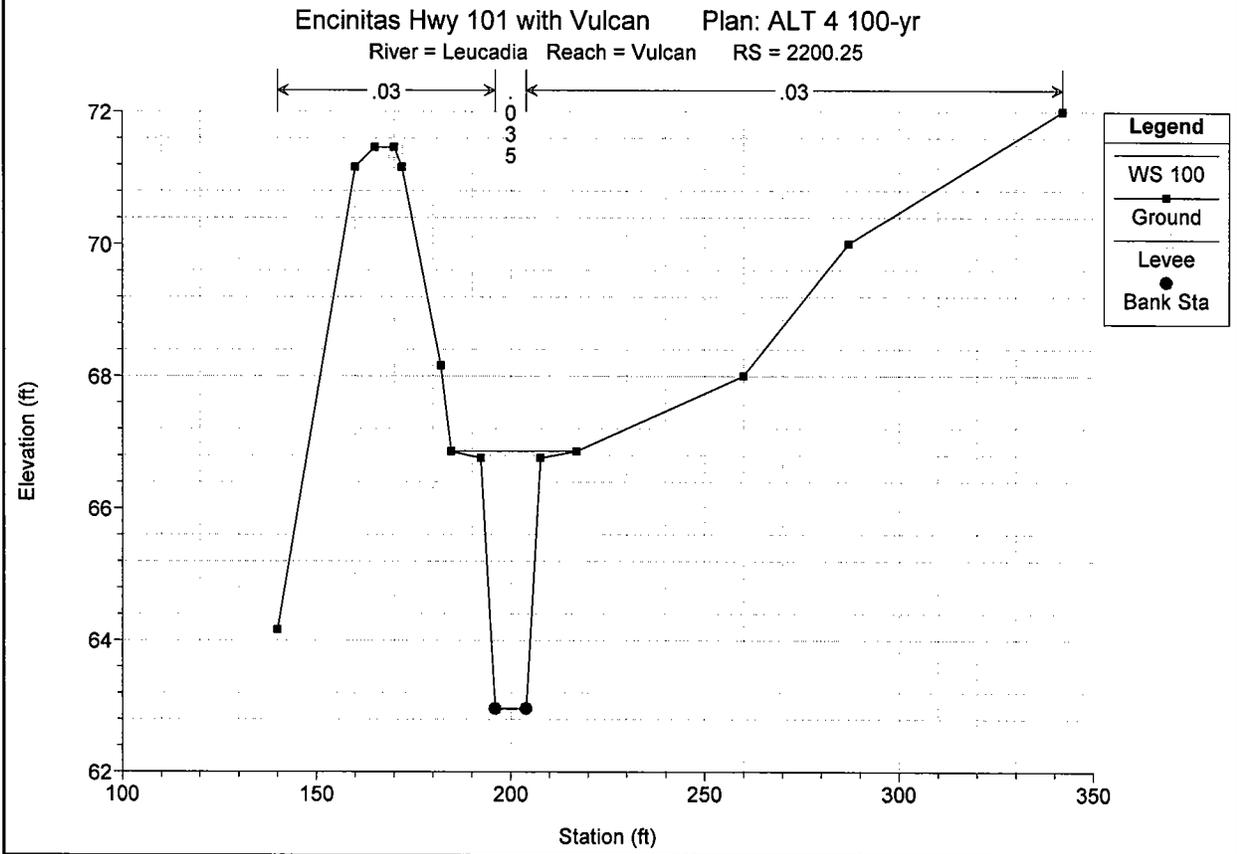
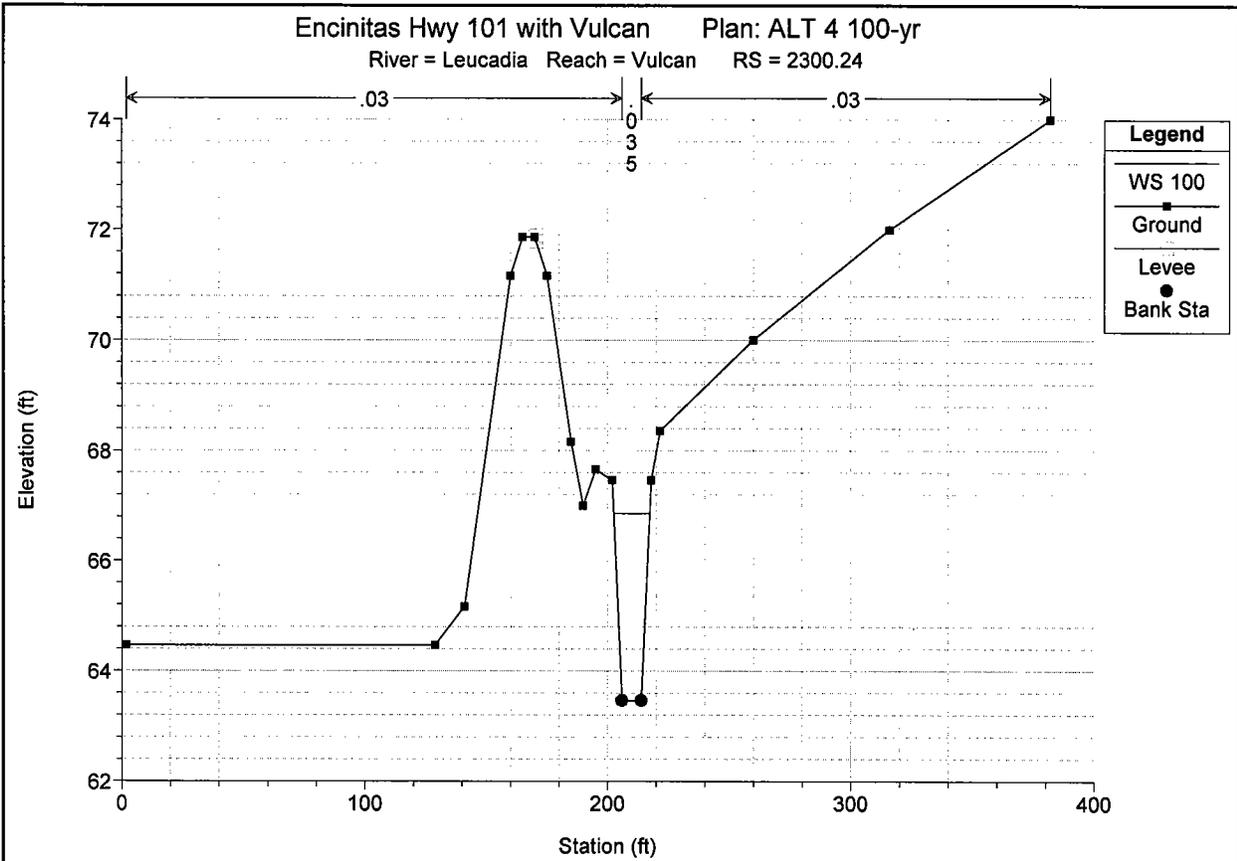


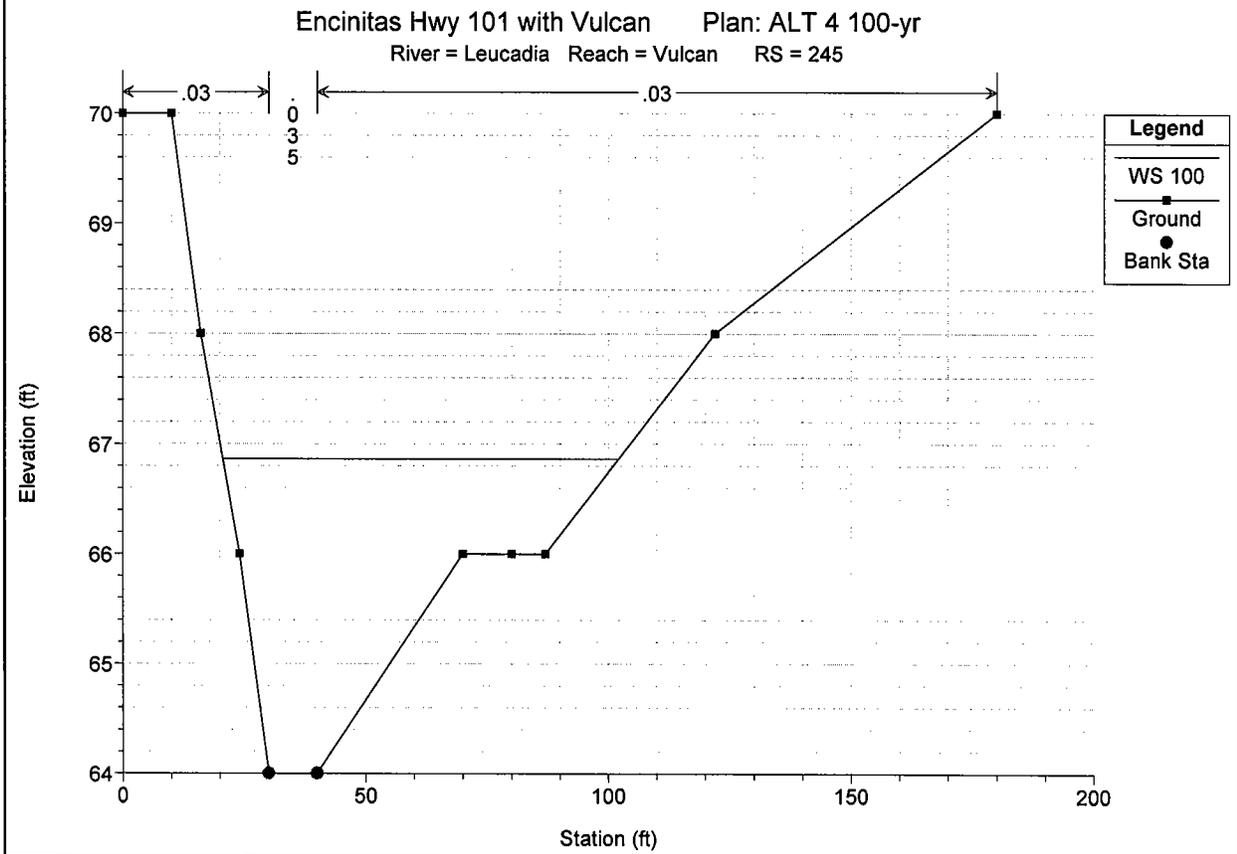
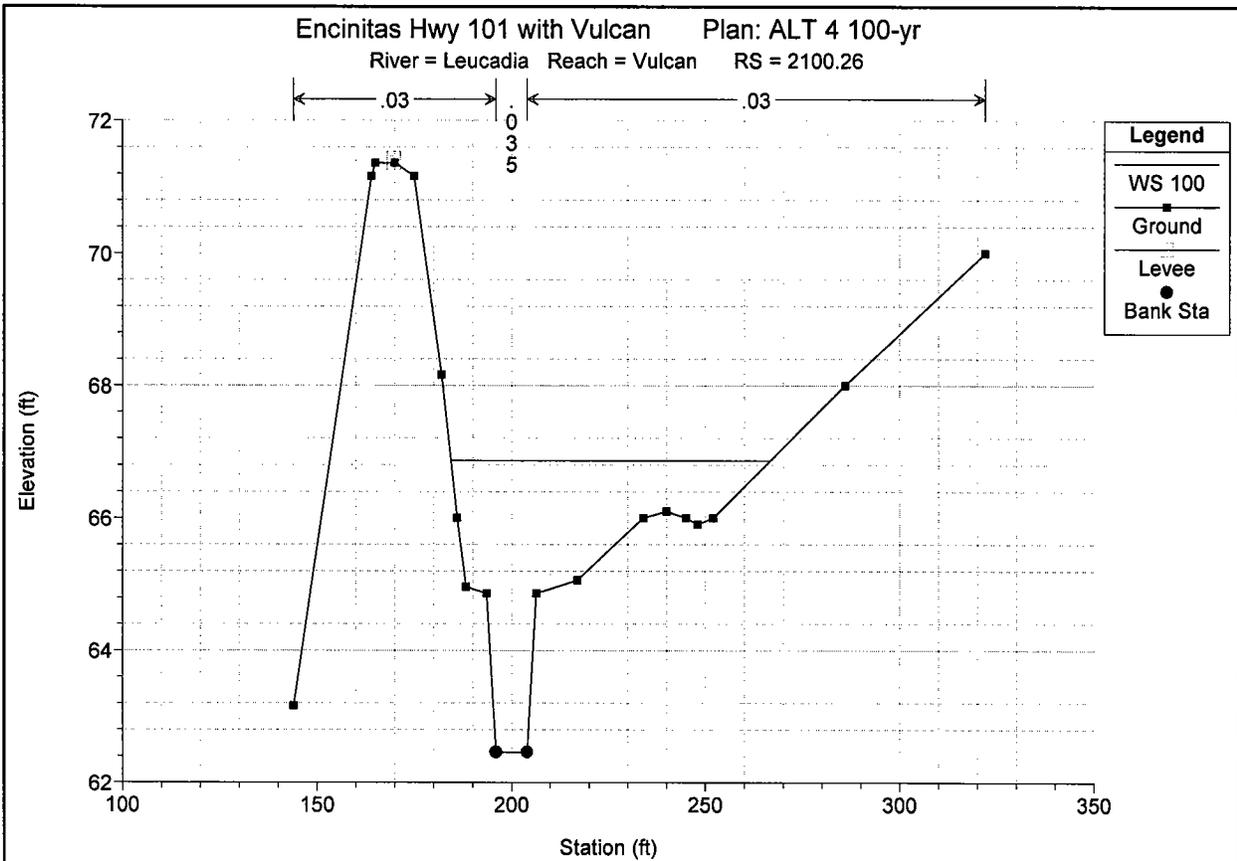




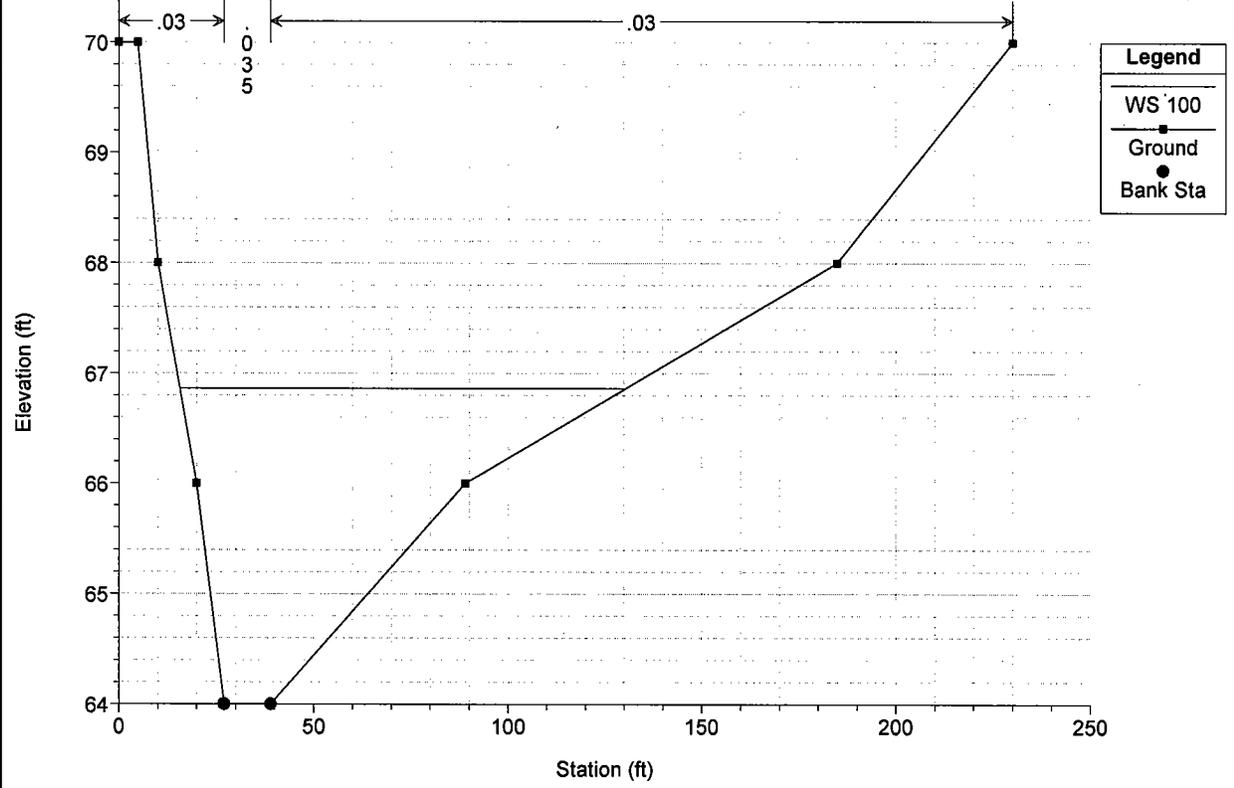




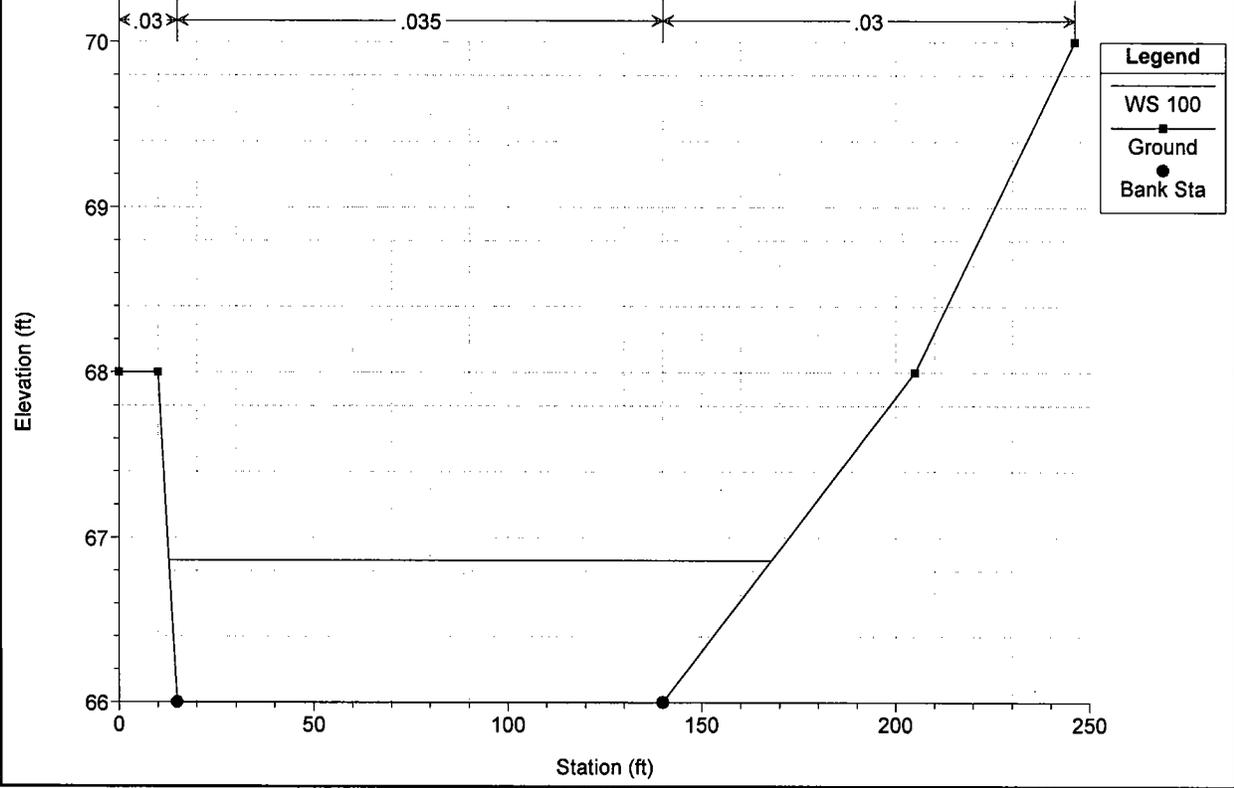


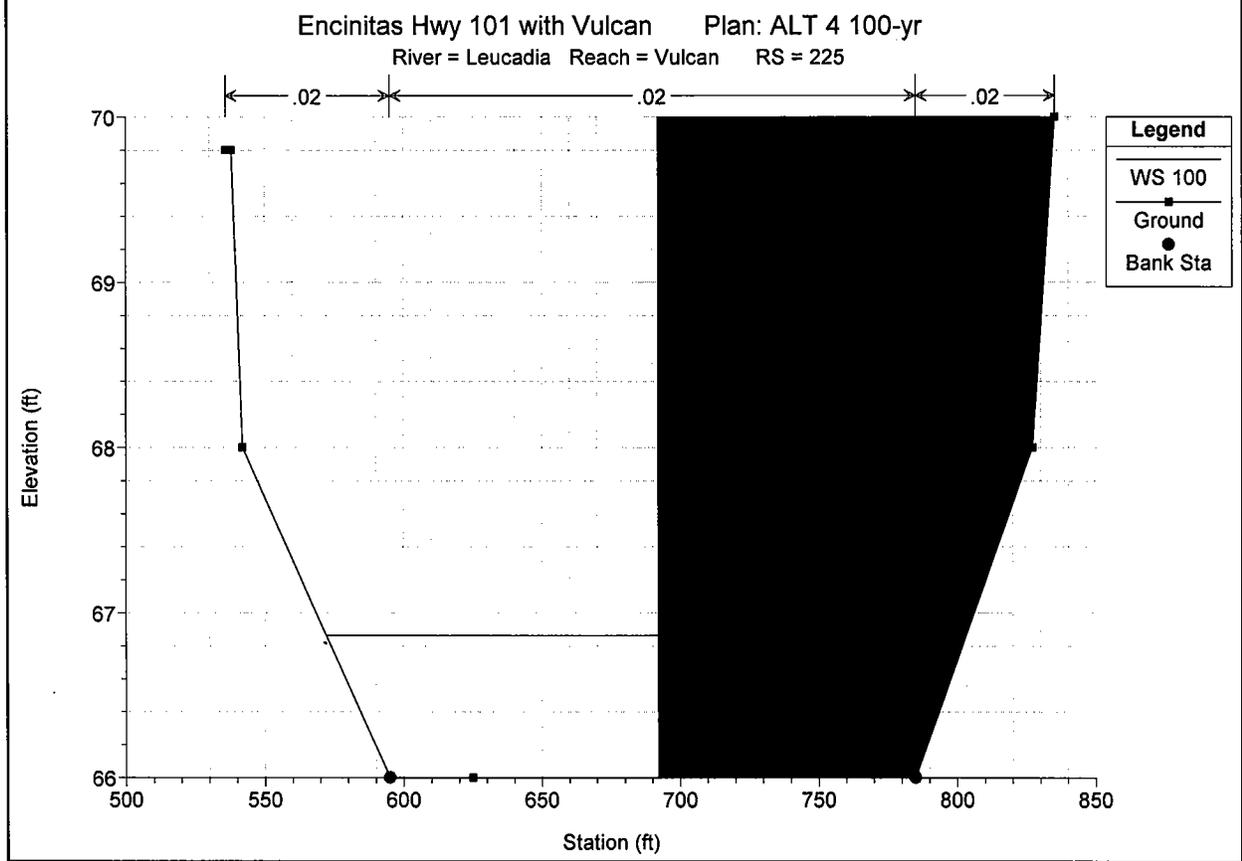
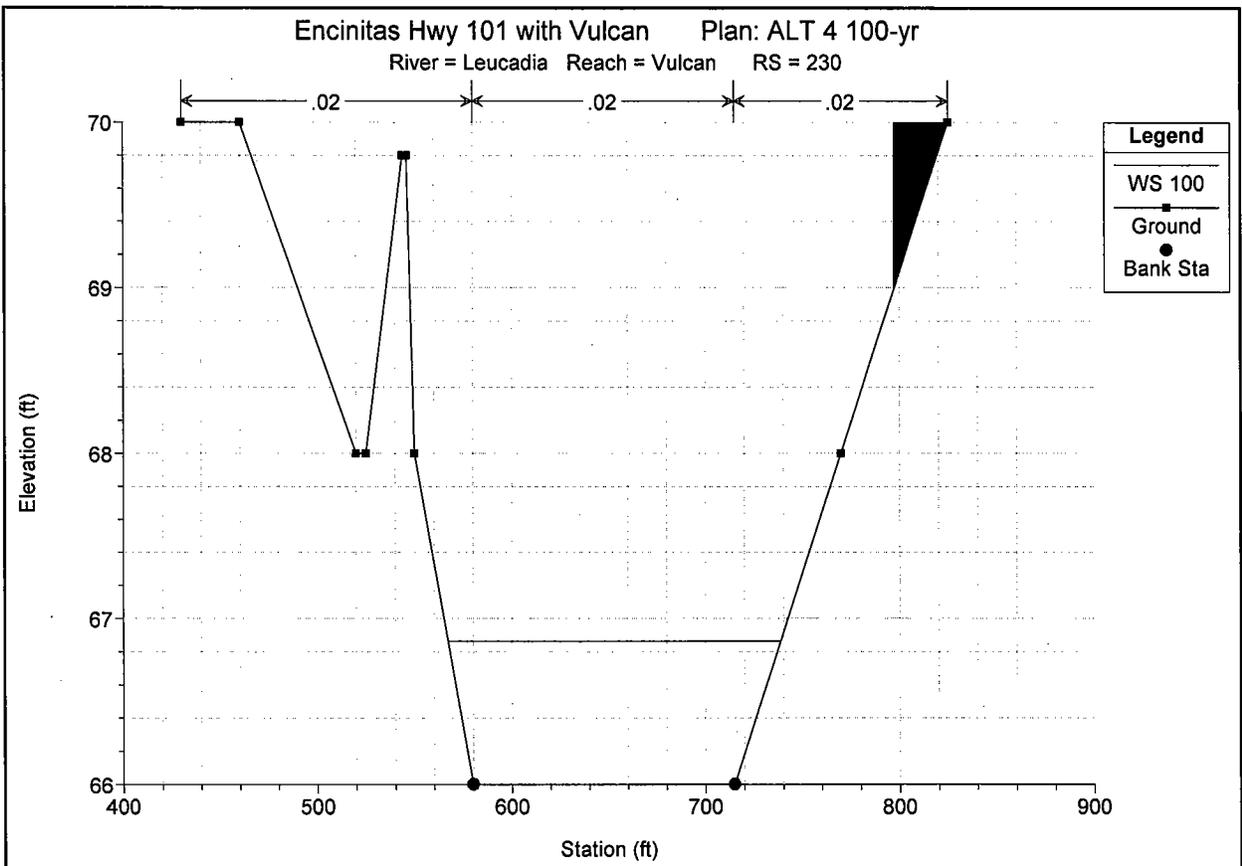


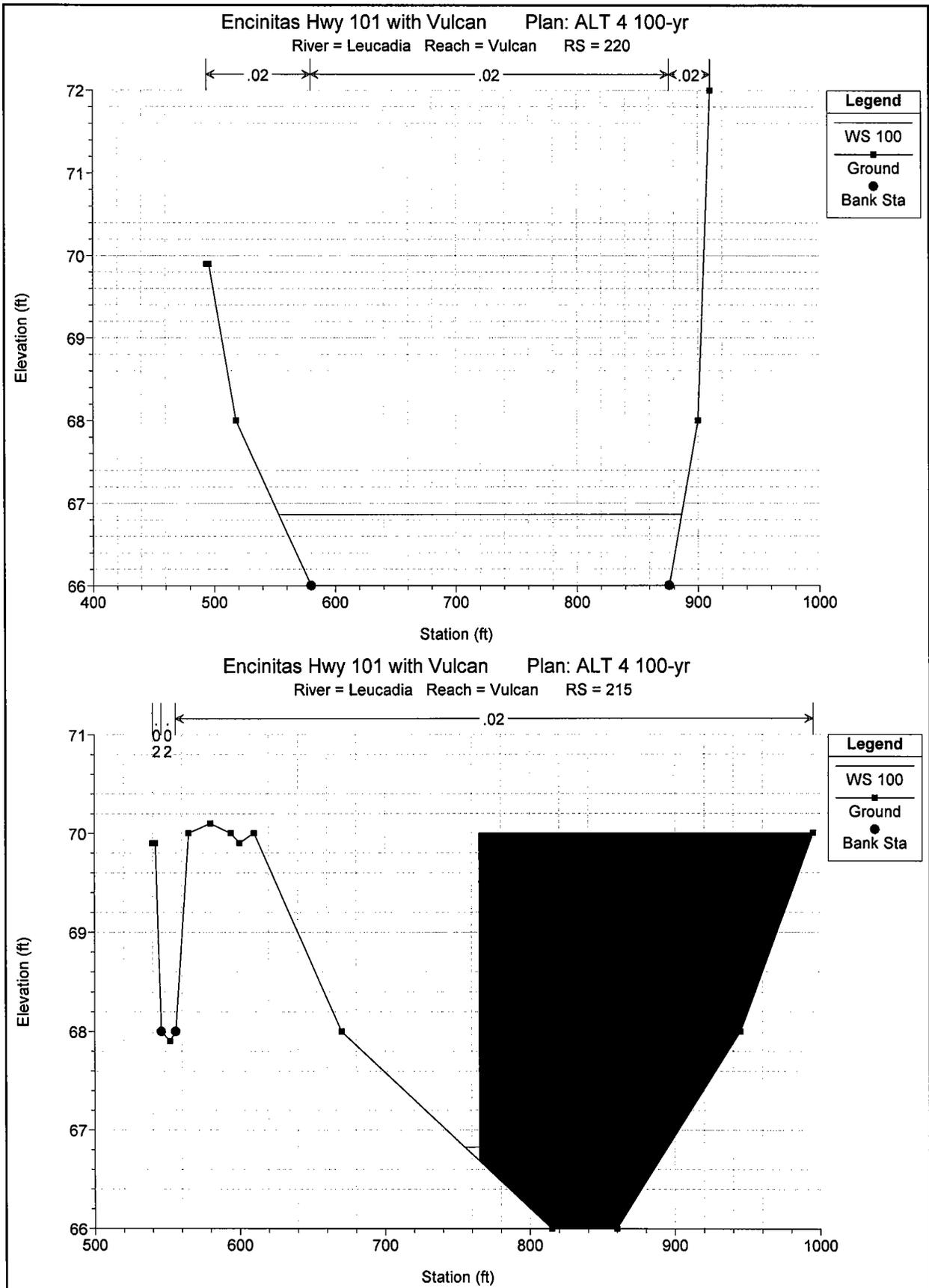
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = Vulcan RS = 240



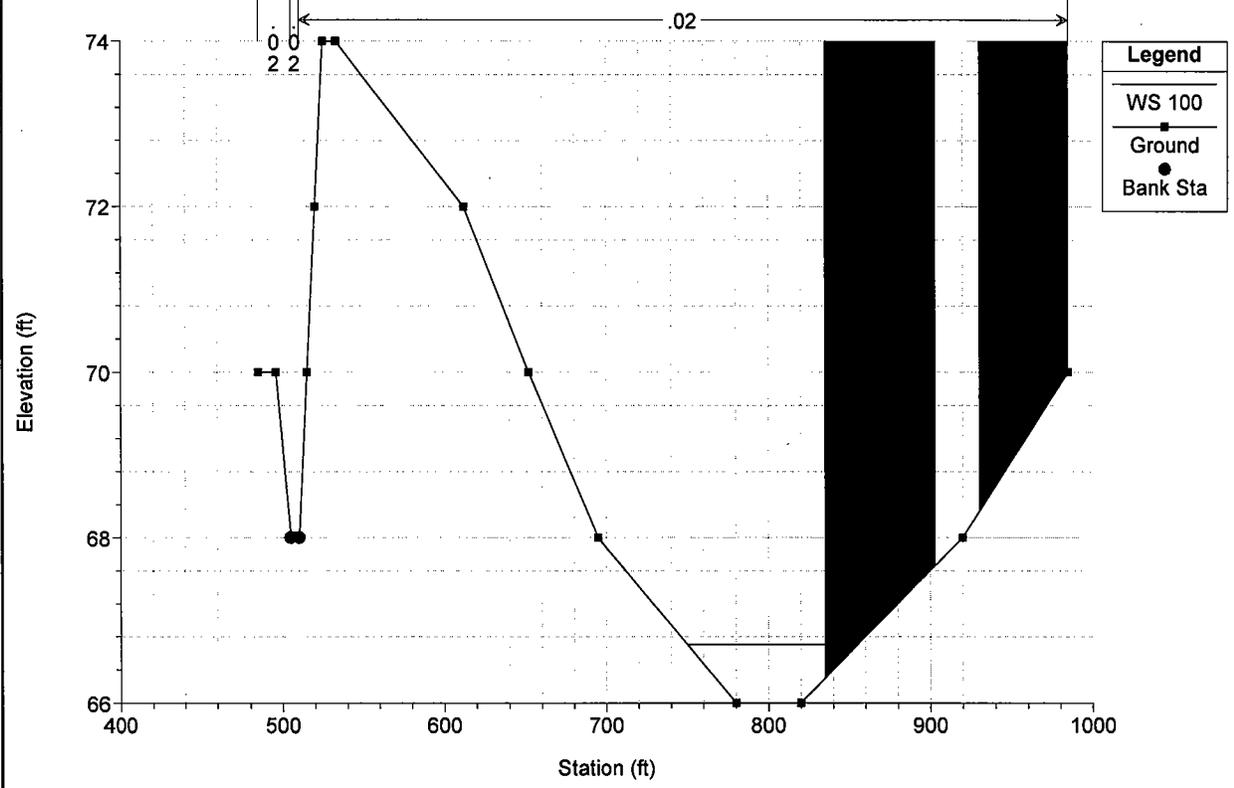
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = Vulcan RS = 235



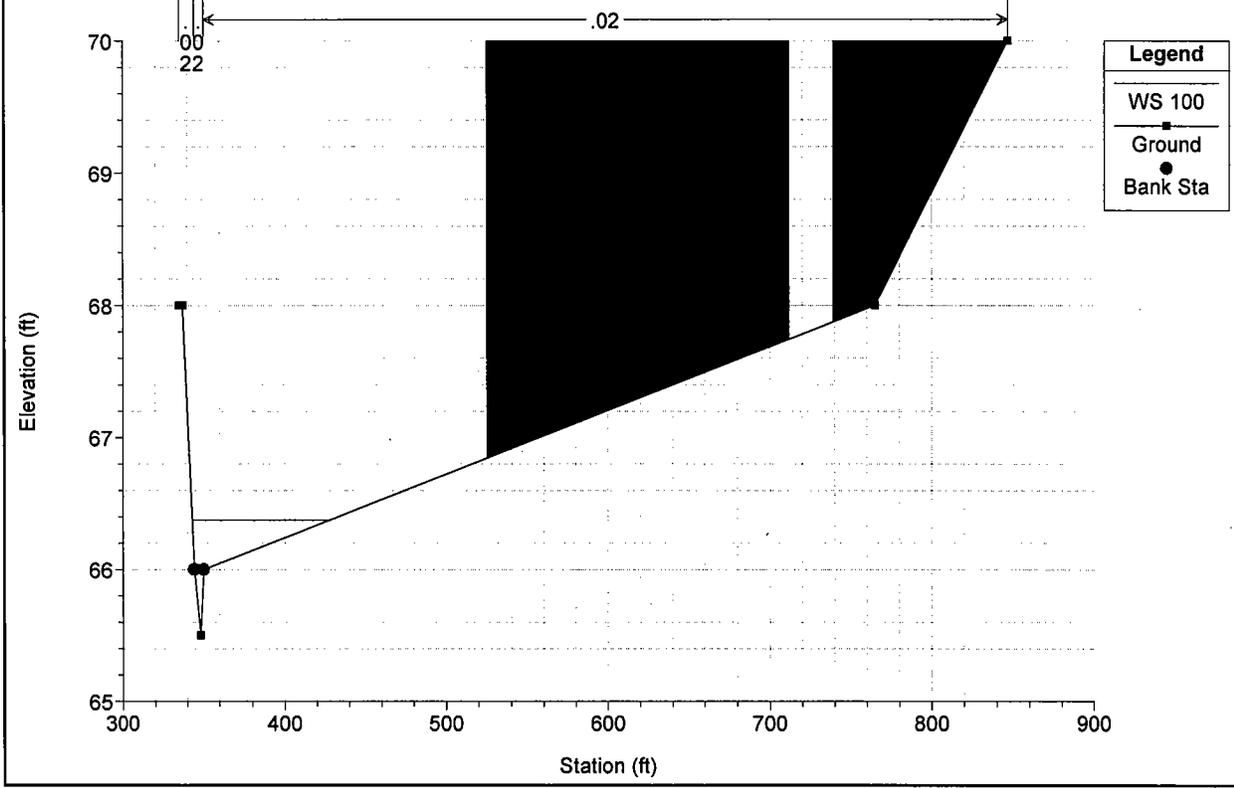


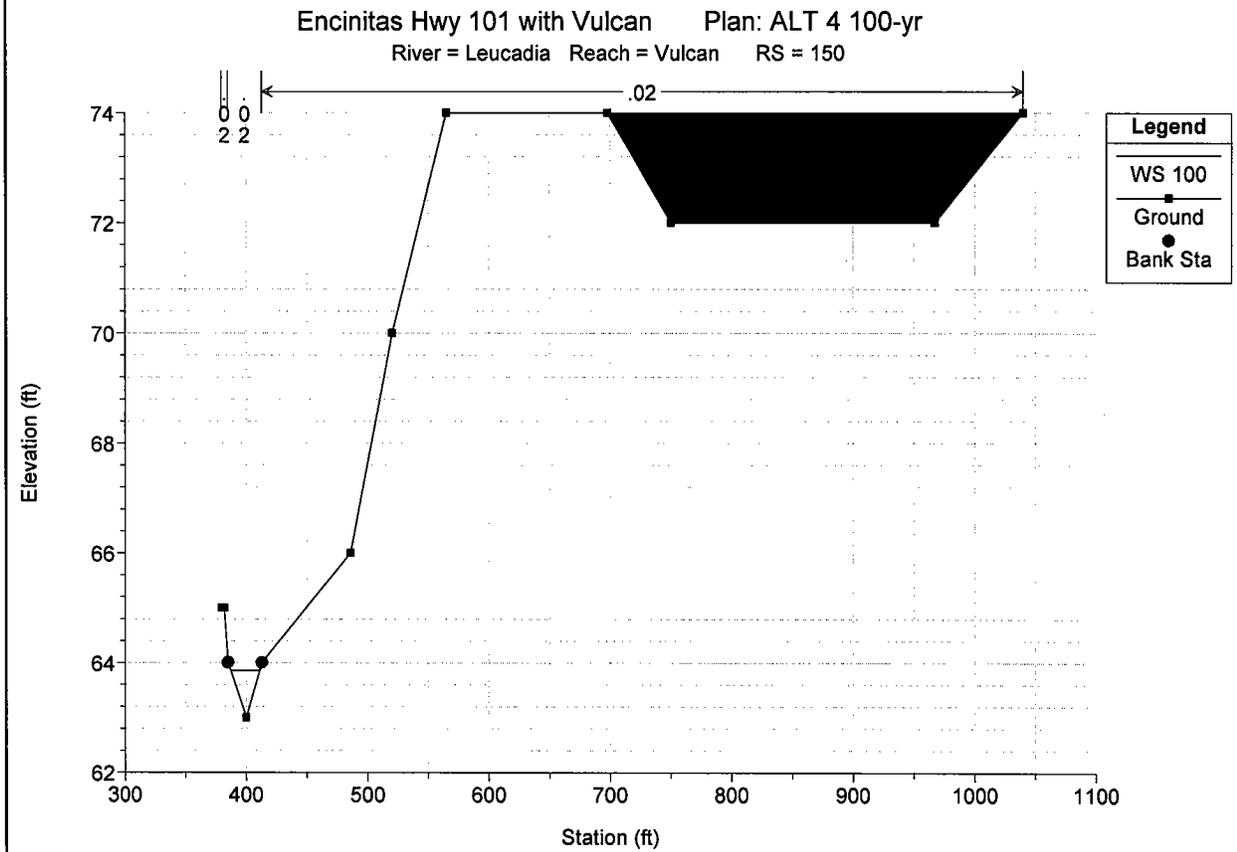
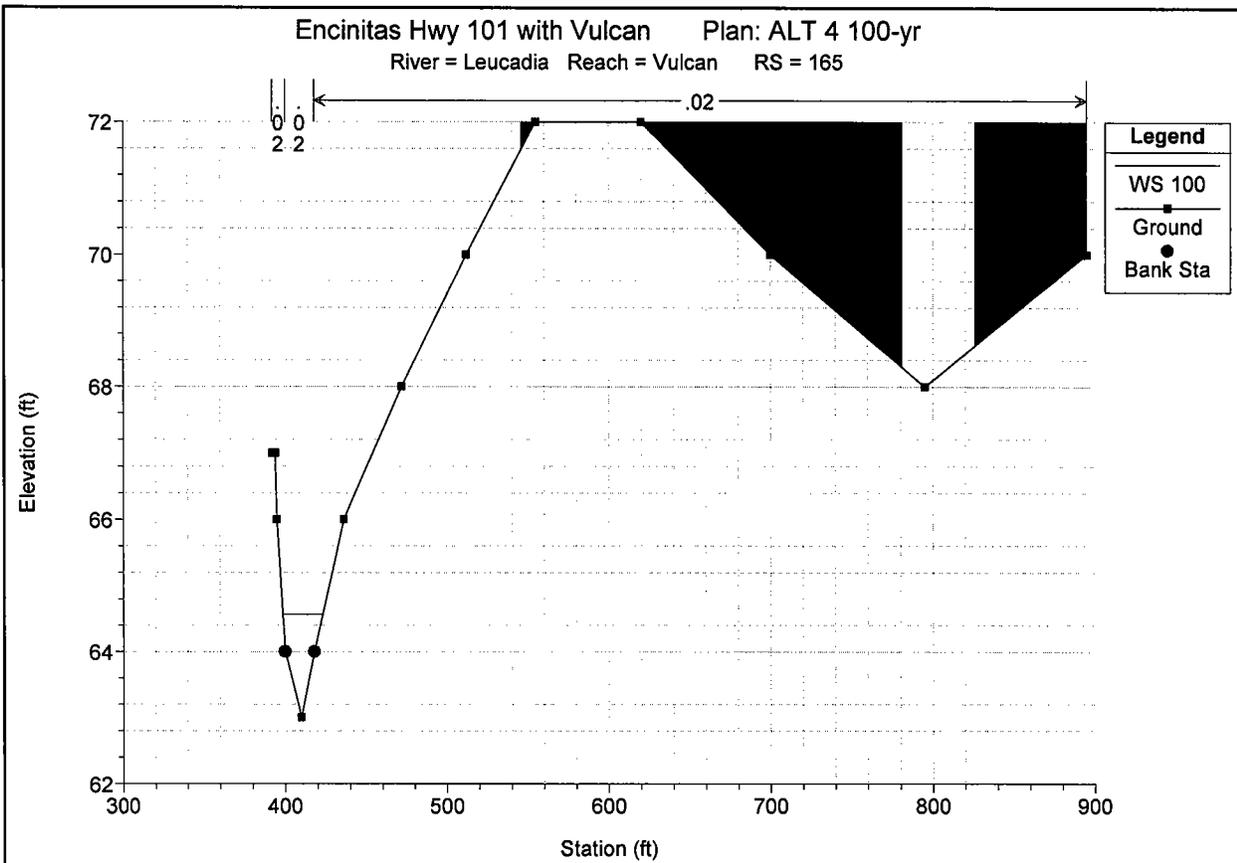


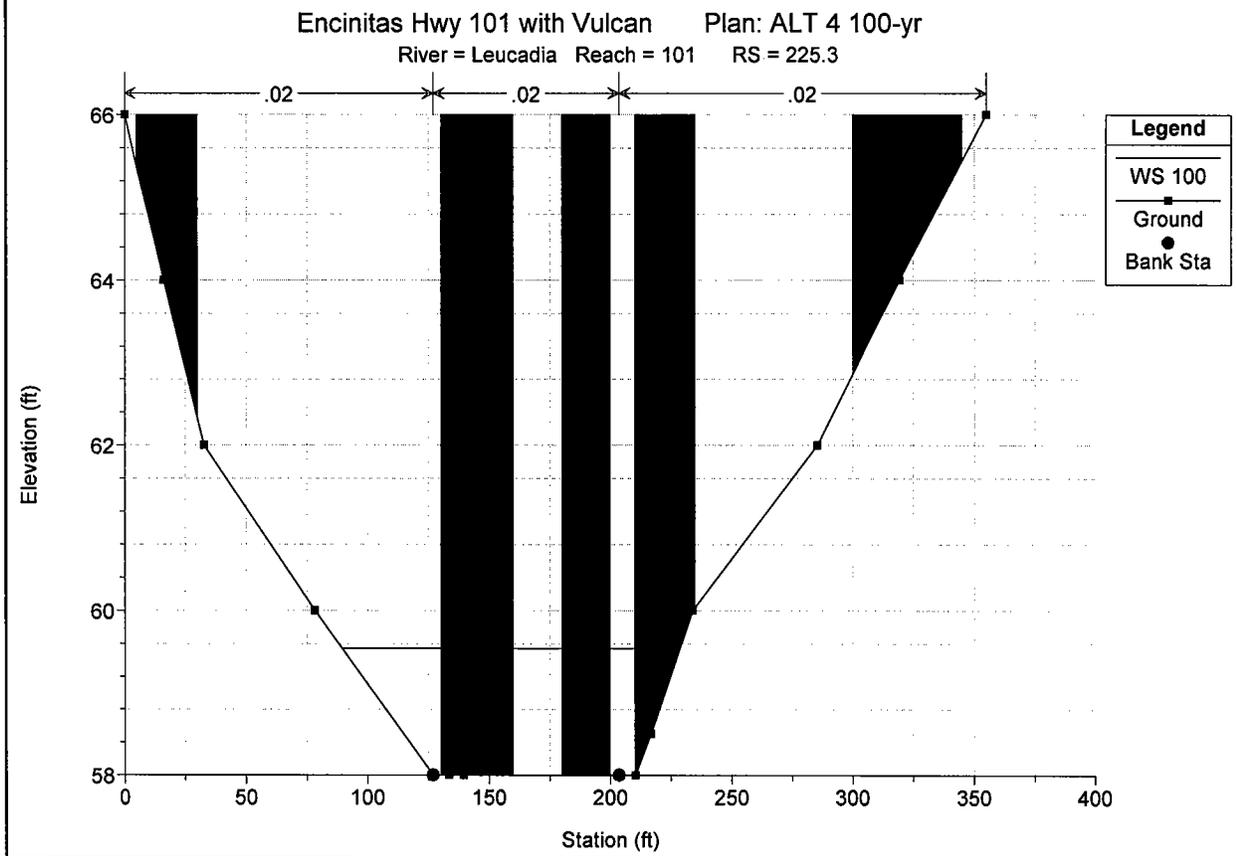
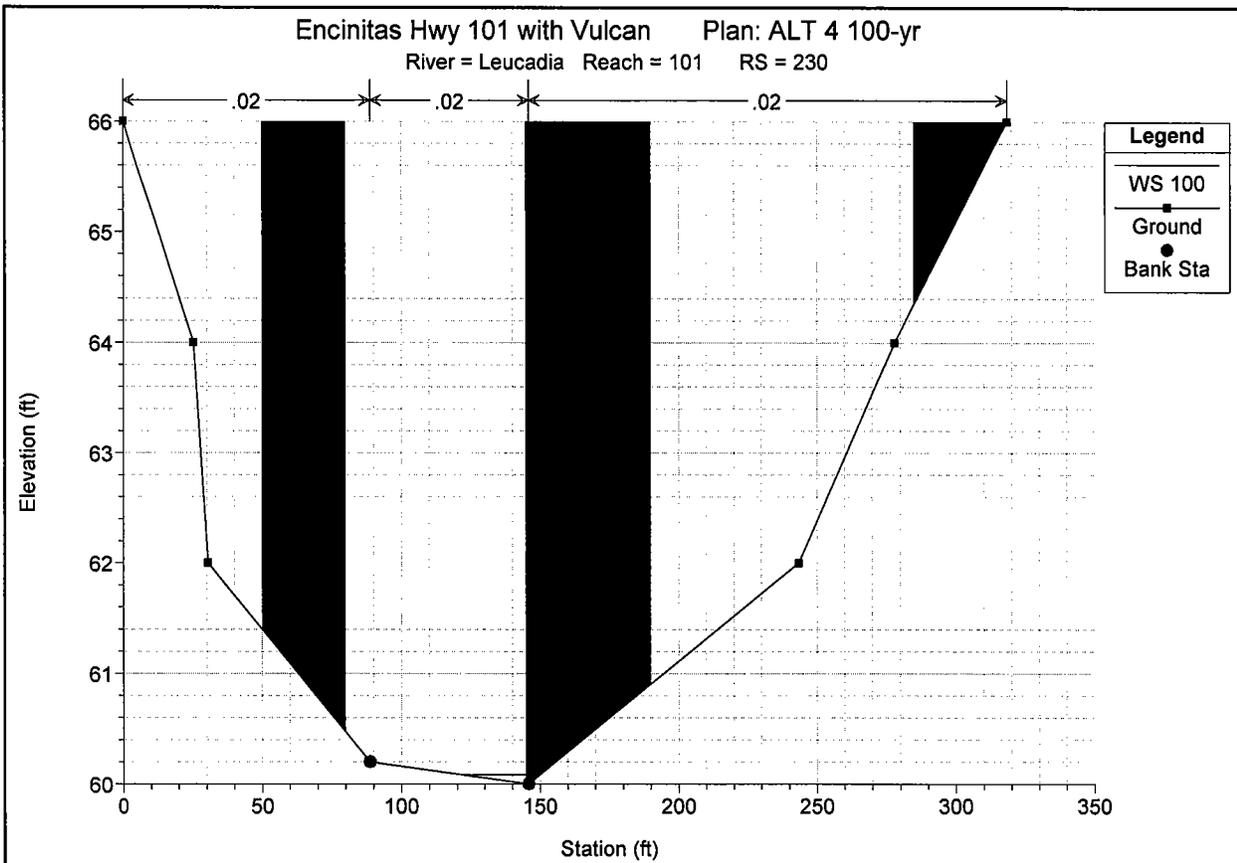
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = Vulcan RS = 195

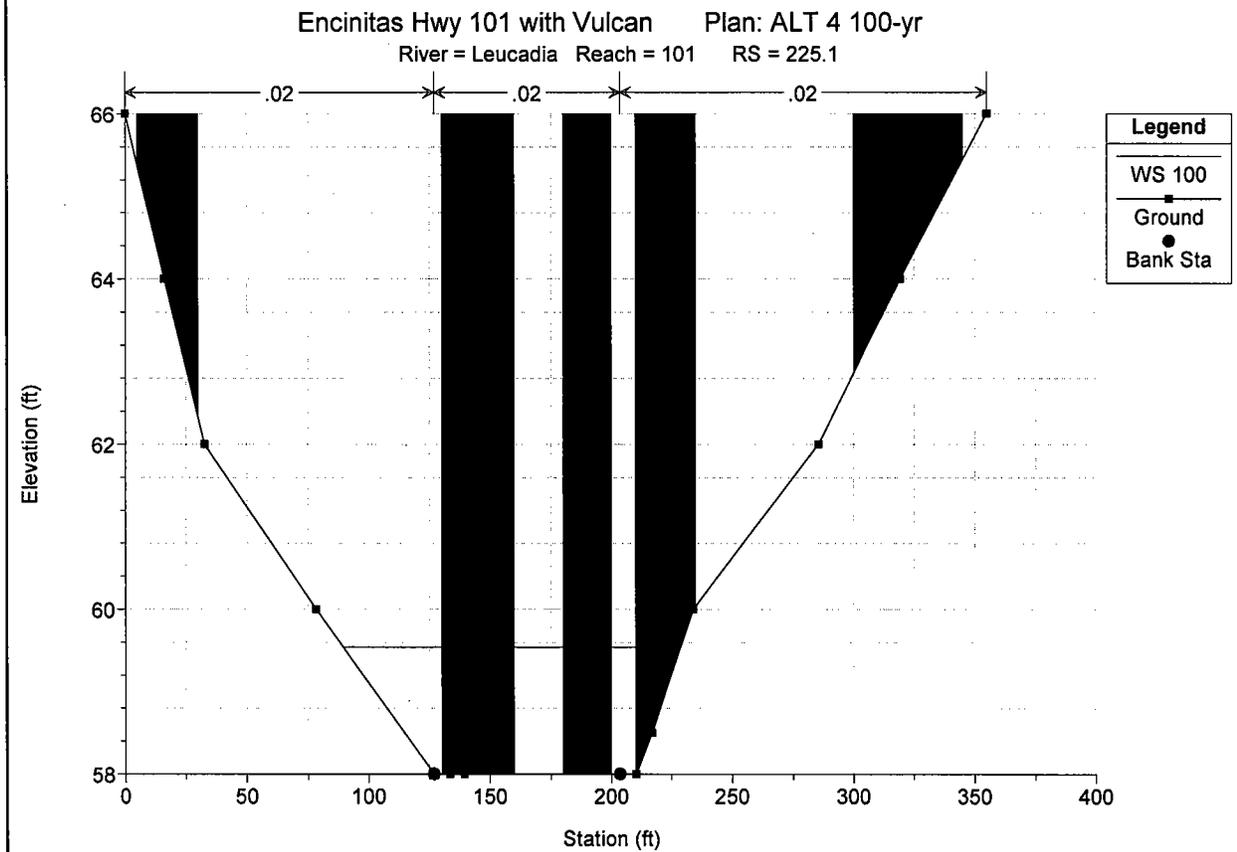
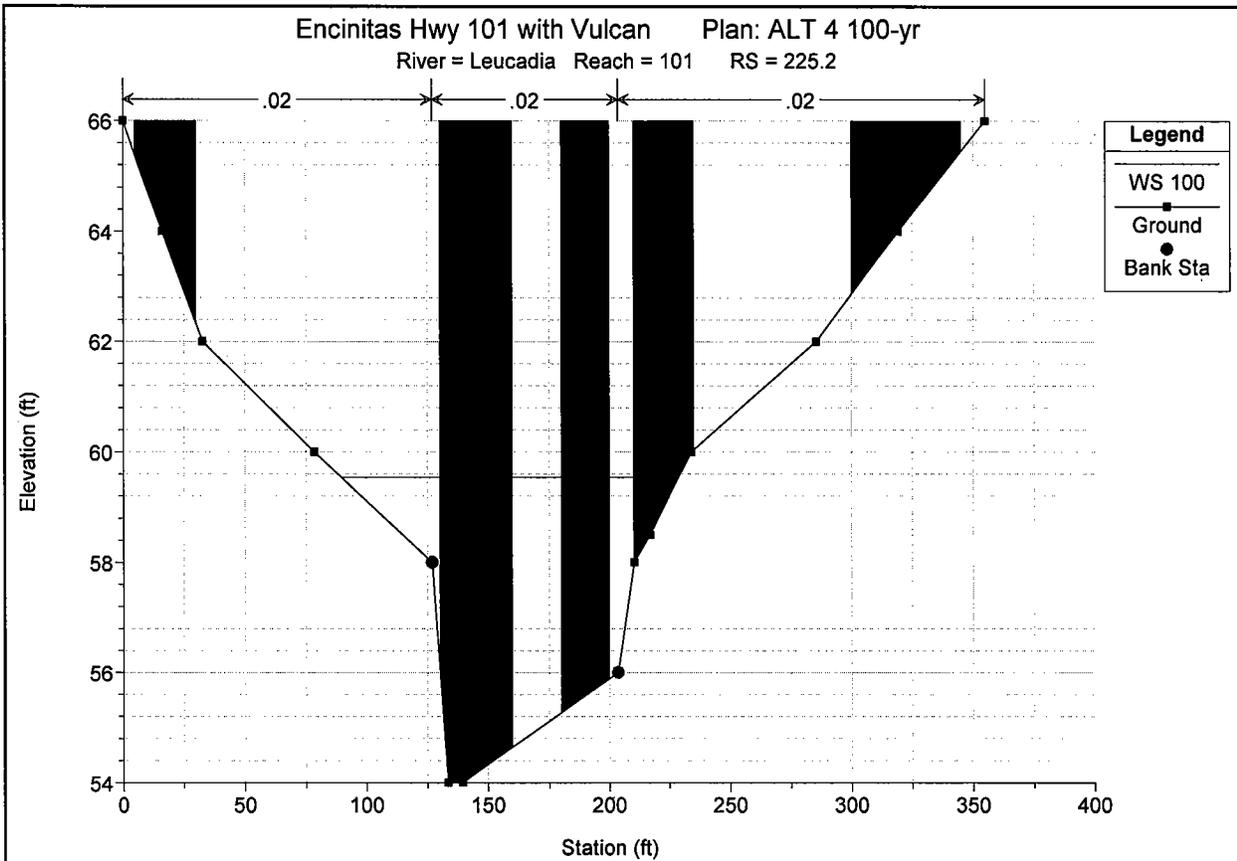


Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = Vulcan RS = 175



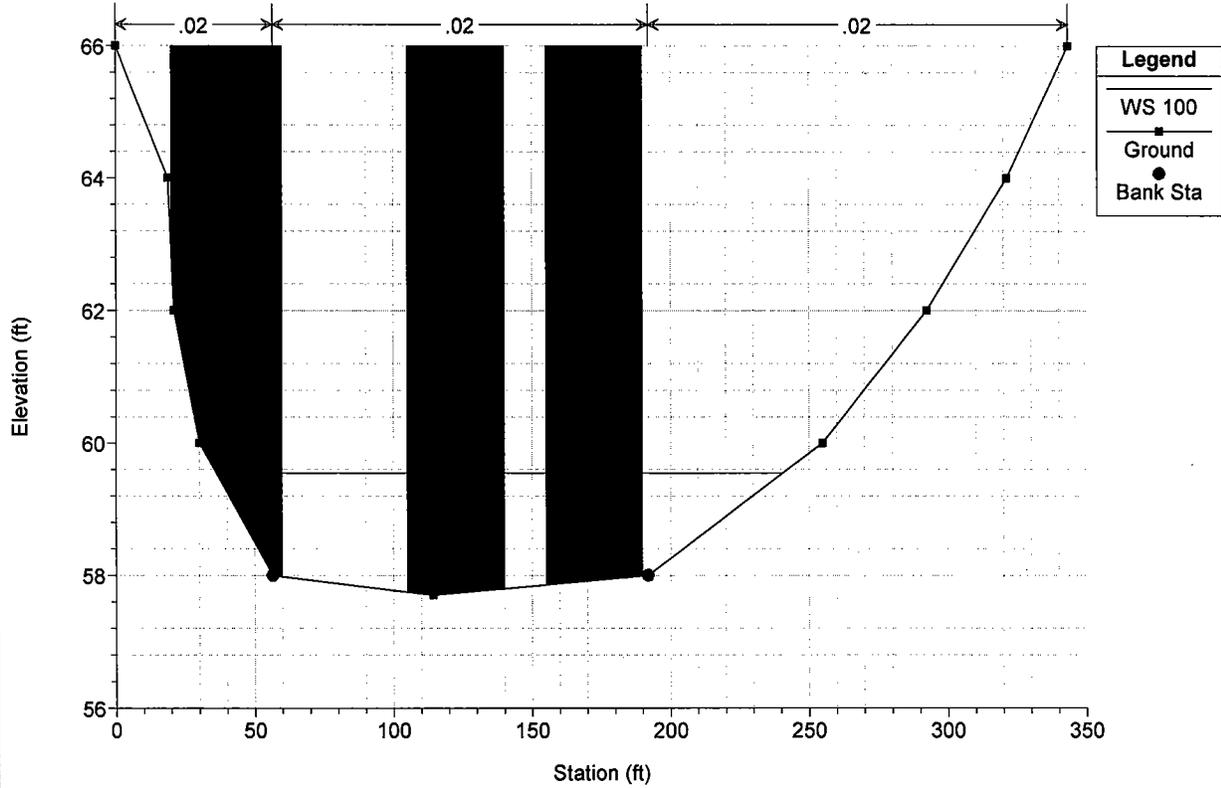






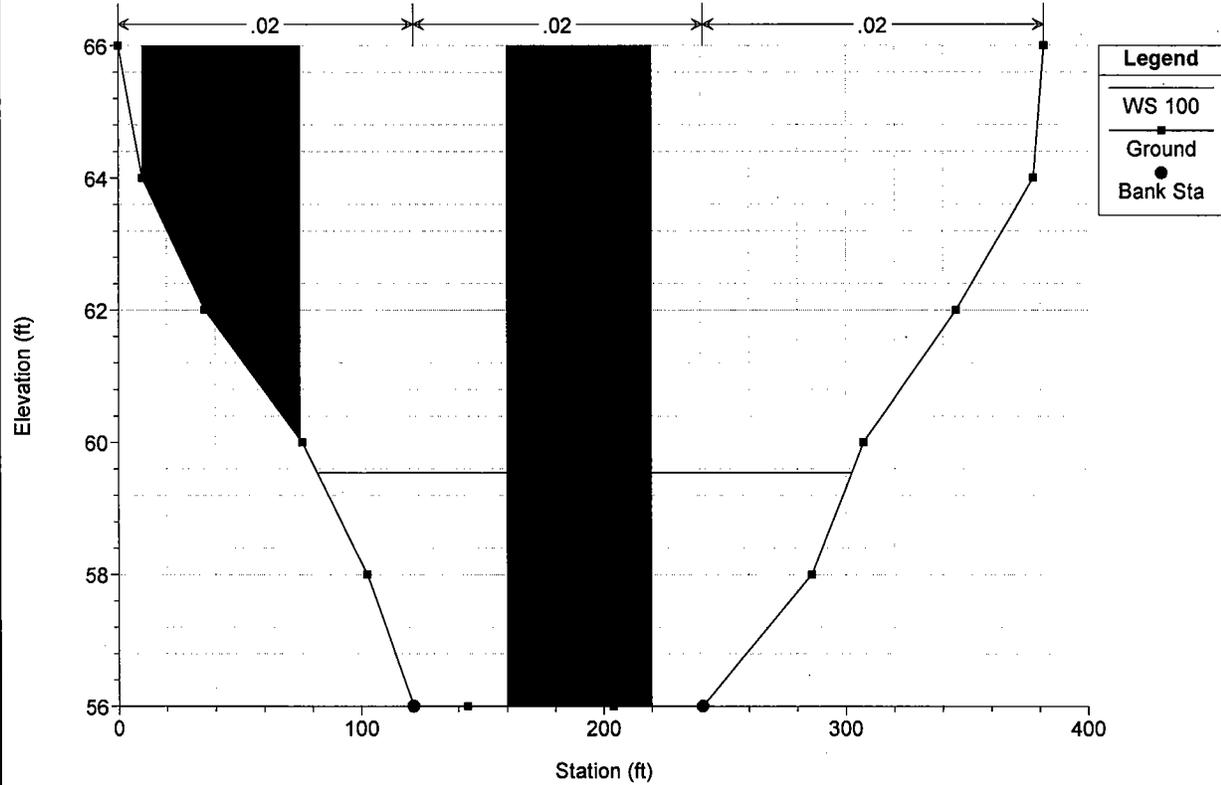
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr

River = Leucadia Reach = 101 RS = 220

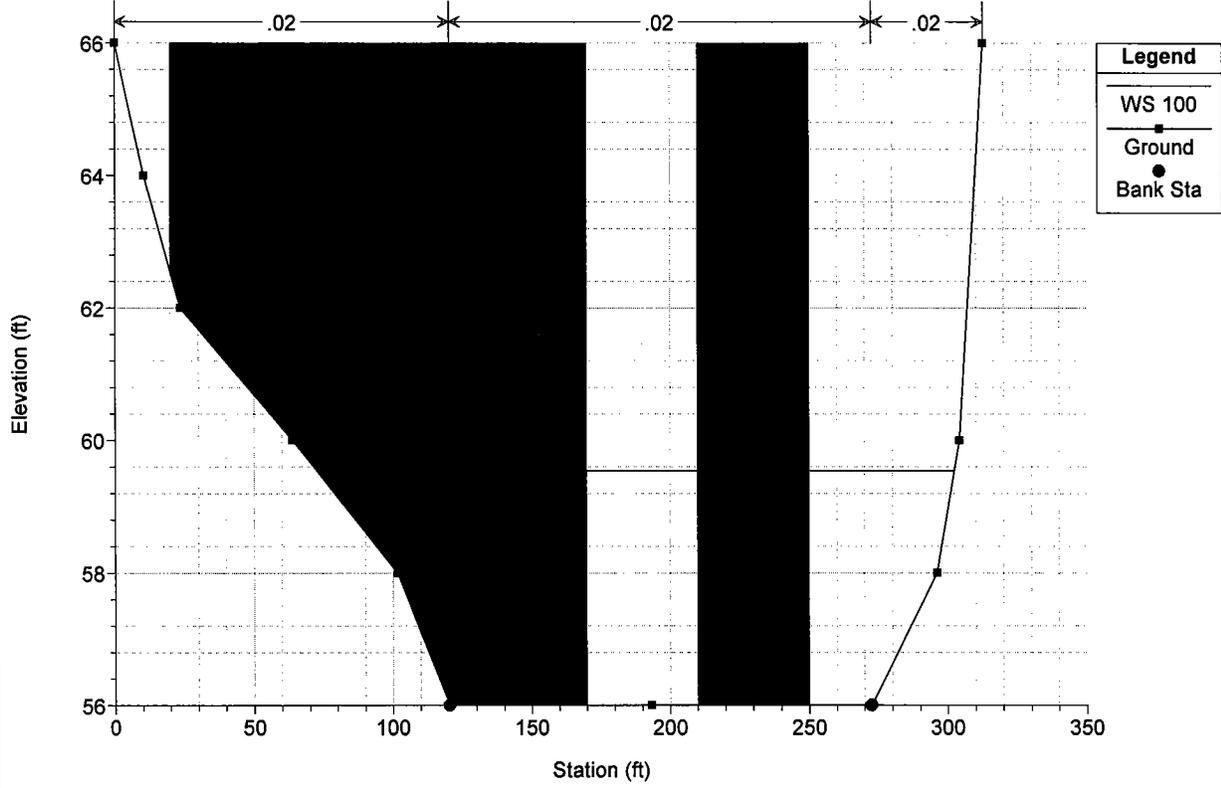


Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr

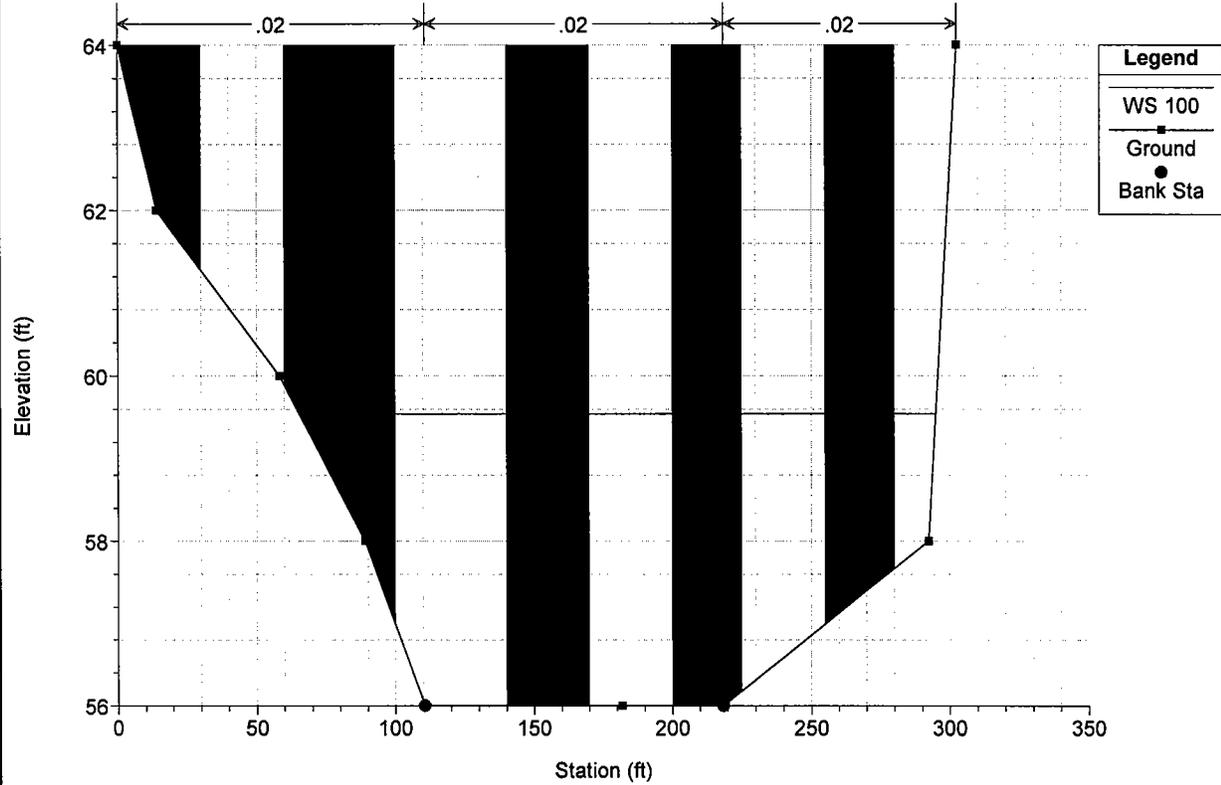
River = Leucadia Reach = 101 RS = 215



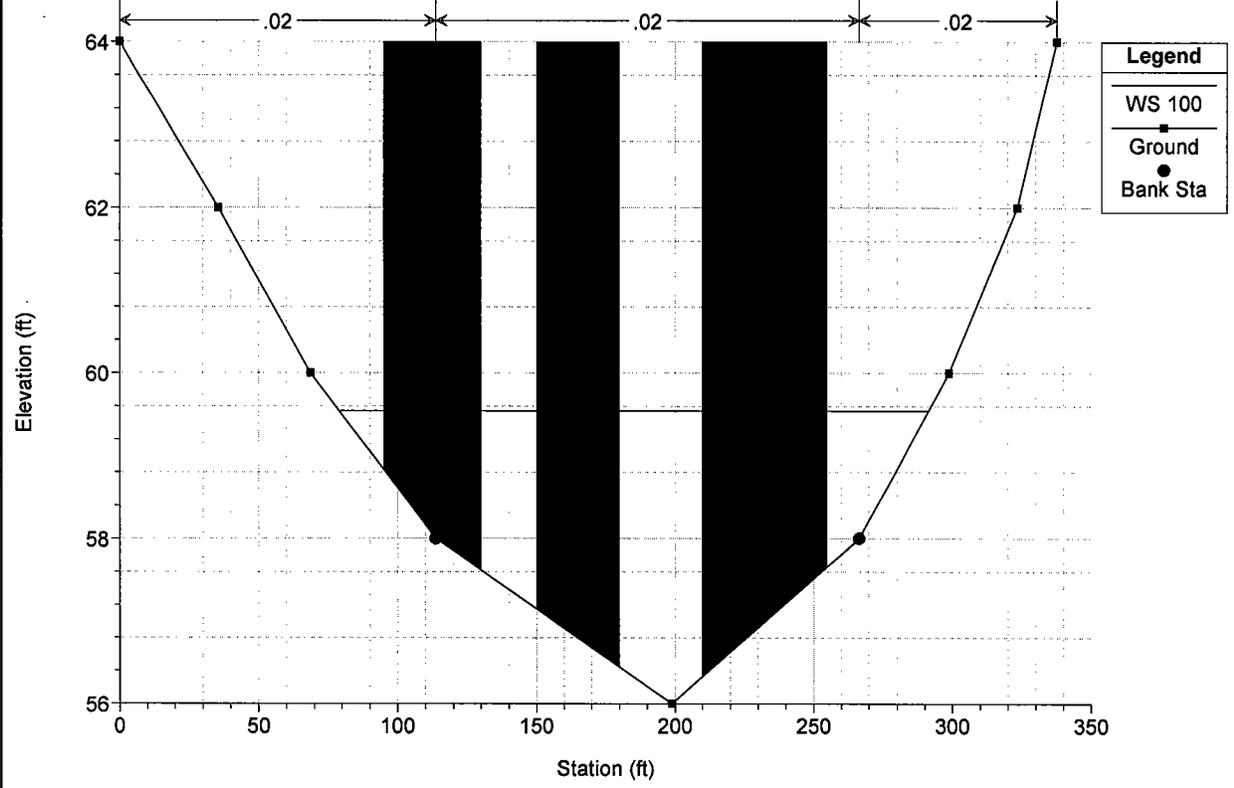
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = 101 RS = 210



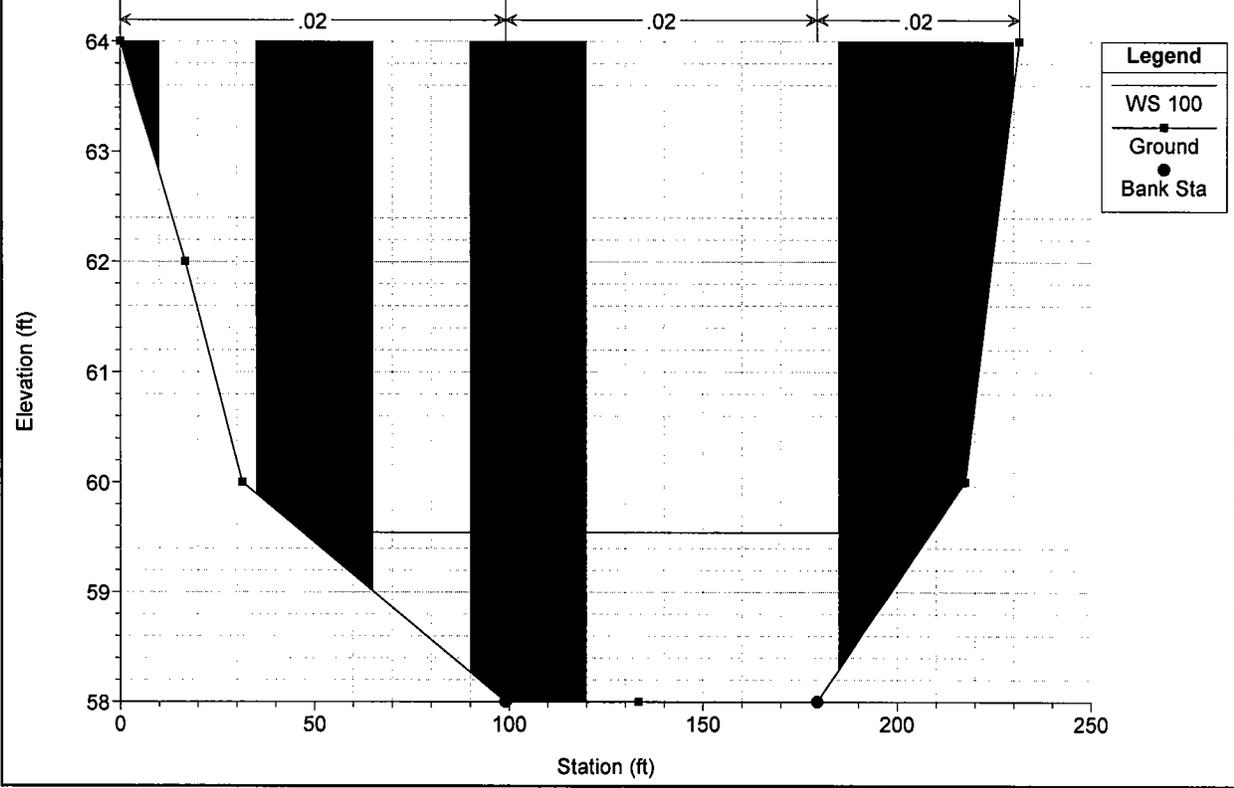
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = 101 RS = 205



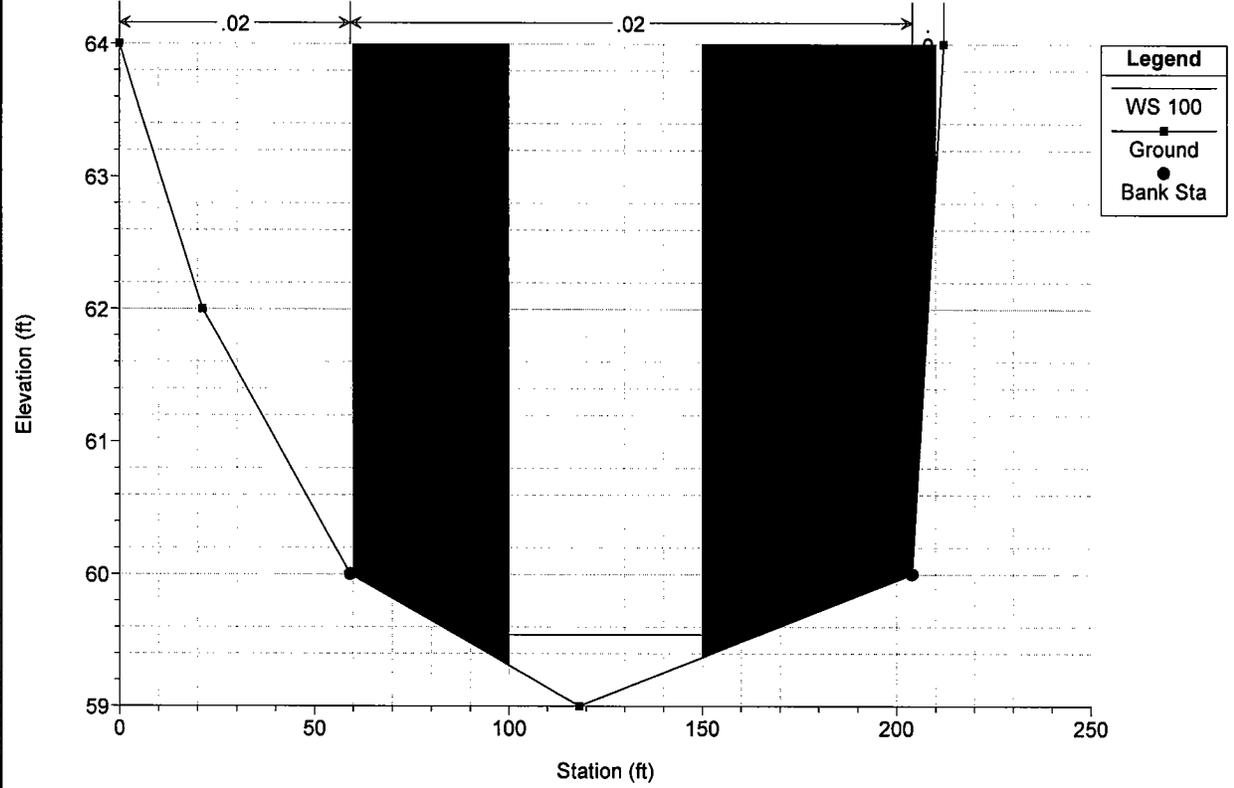
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = 101 RS = 195



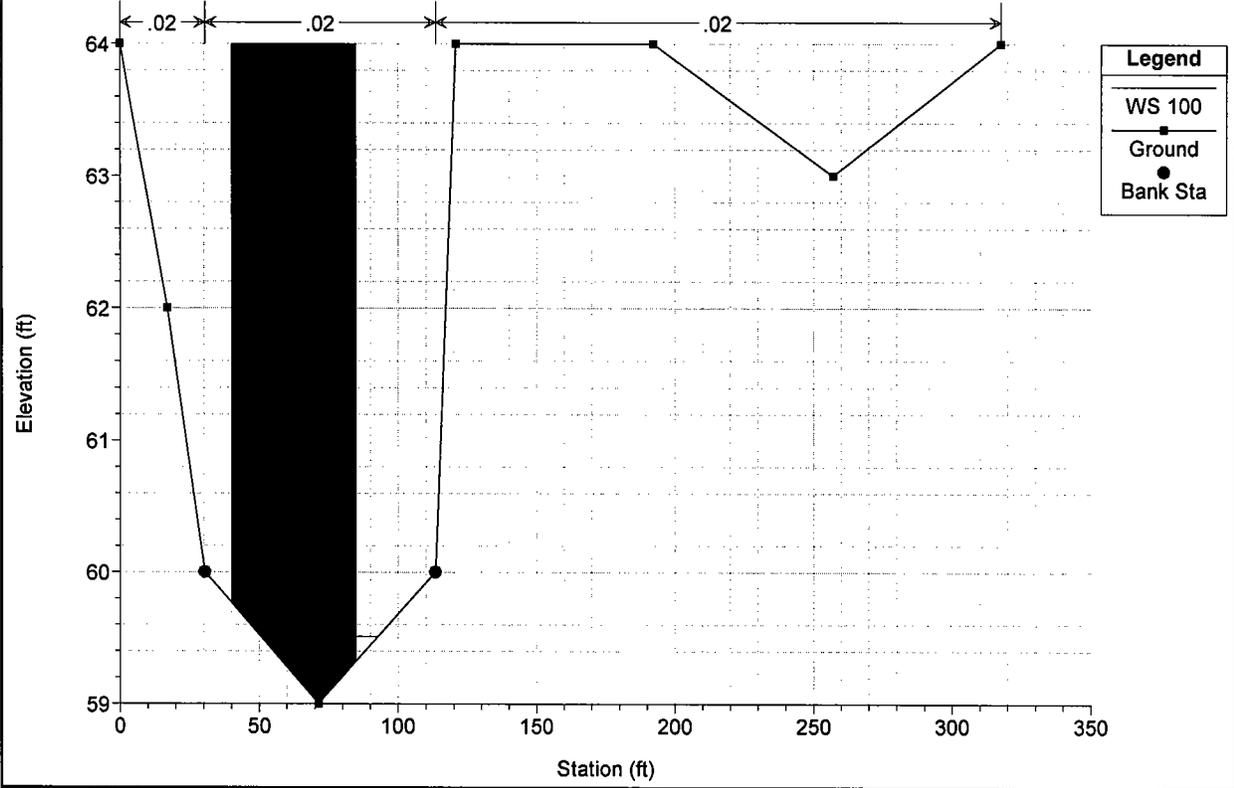
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = 101 RS = 190



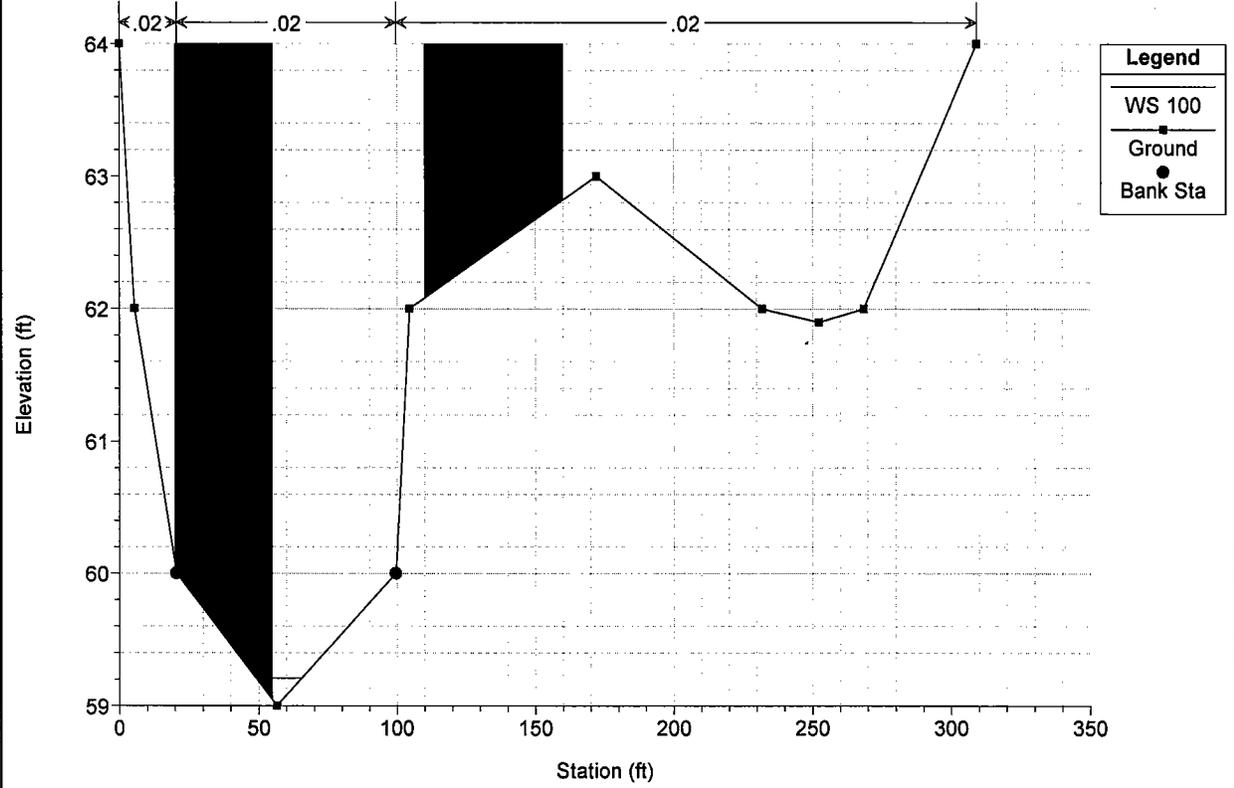
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = 101 RS = 185



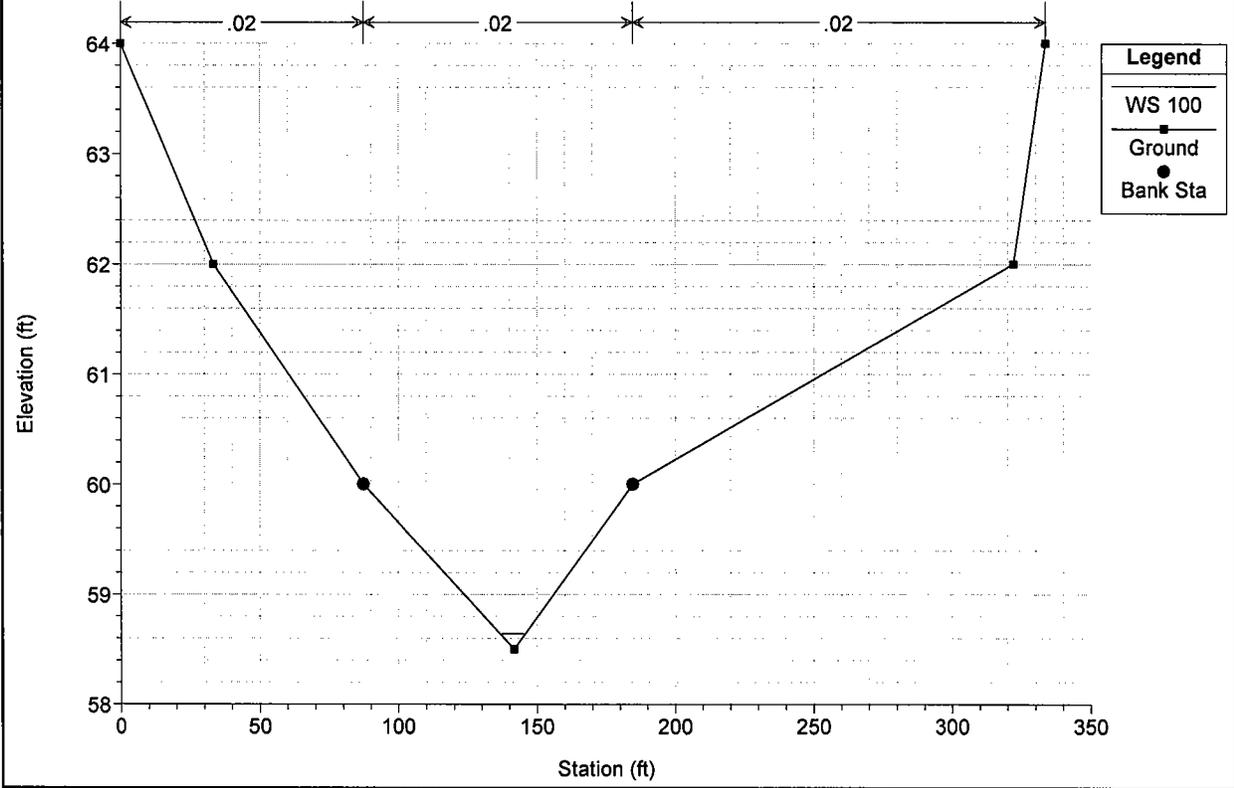
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = 101 RS = 180



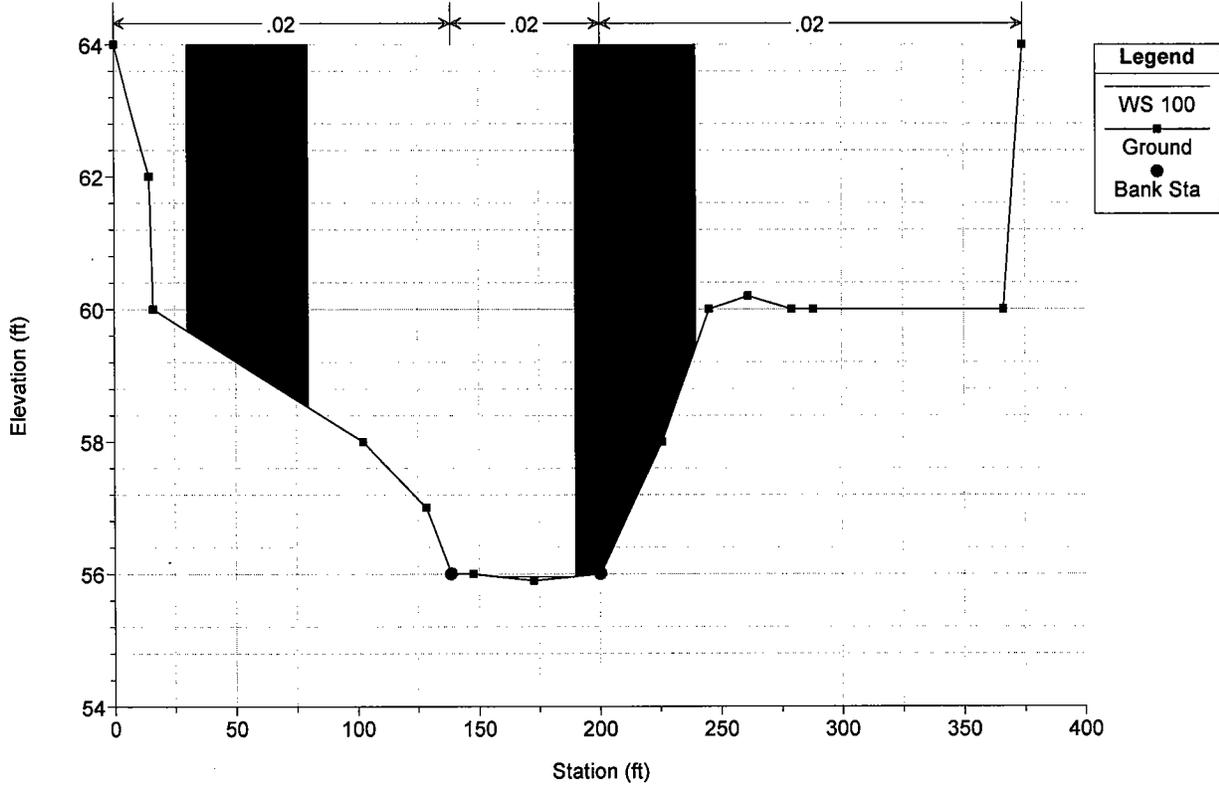
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = 101 RS = 175



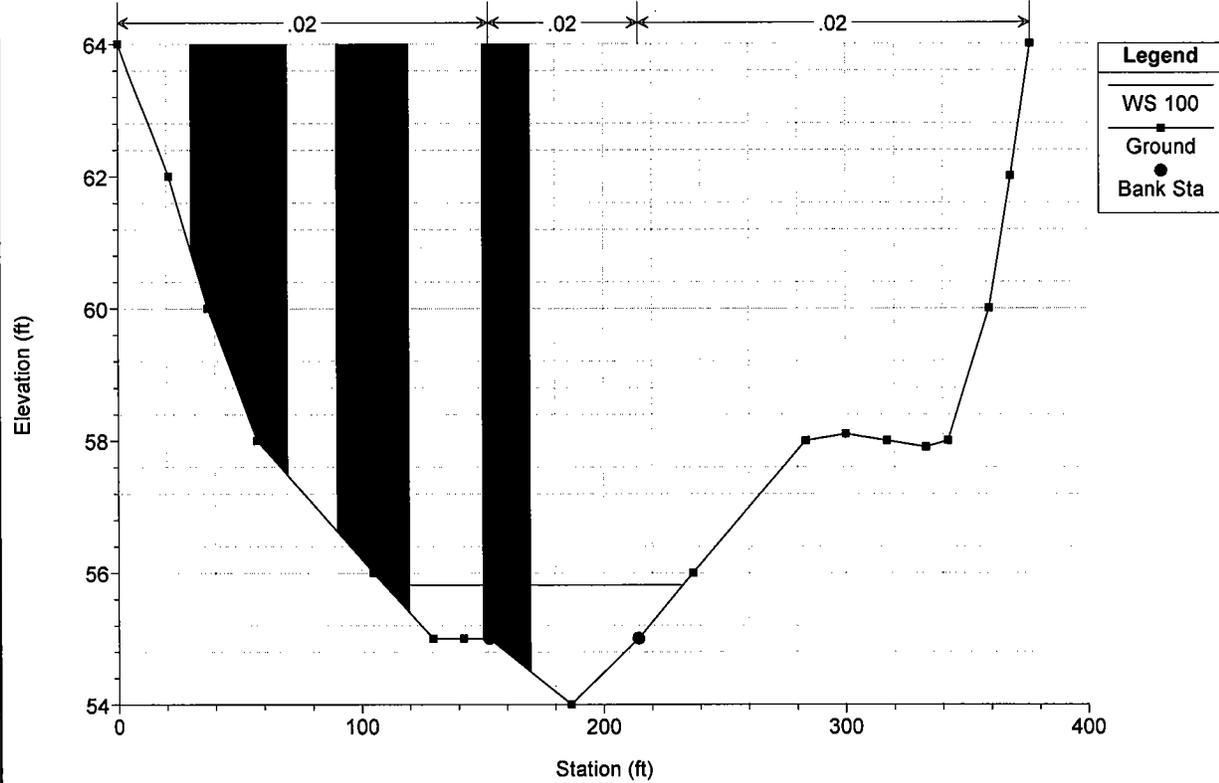
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = 101 RS = 170



Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = 101 RS = 165

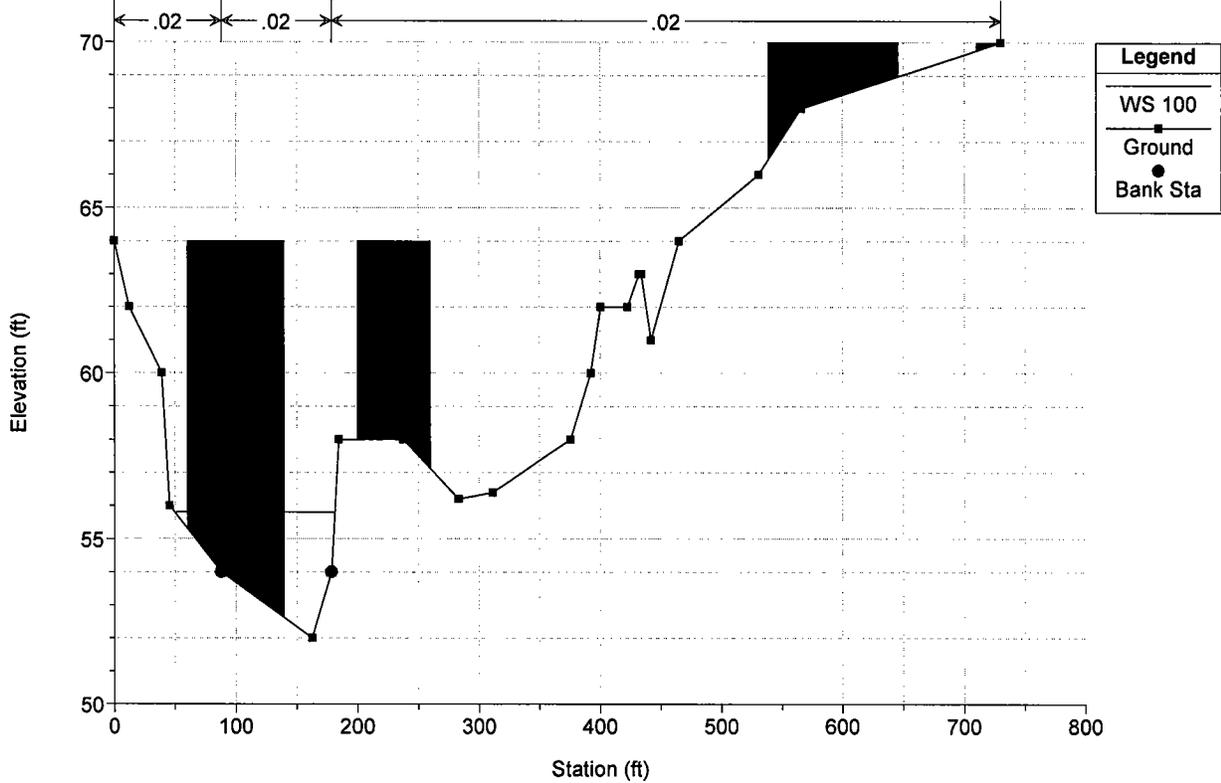


Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = 101 RS = 160

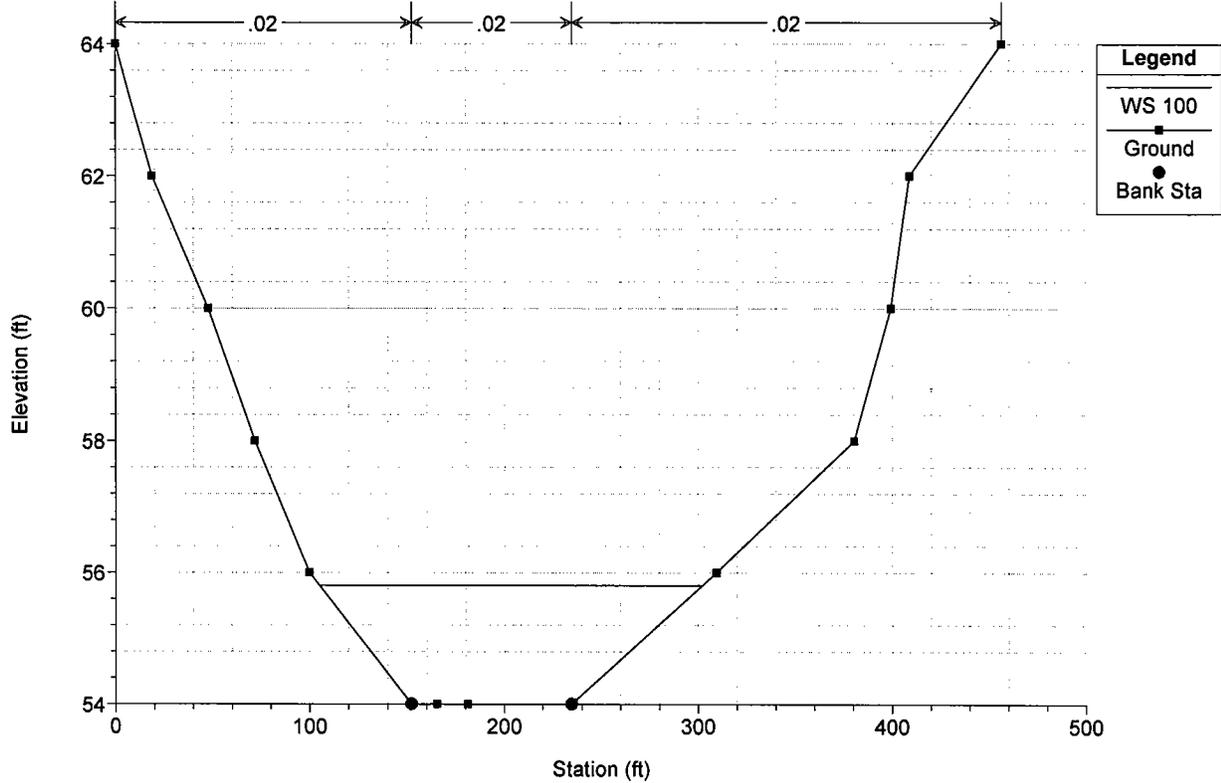


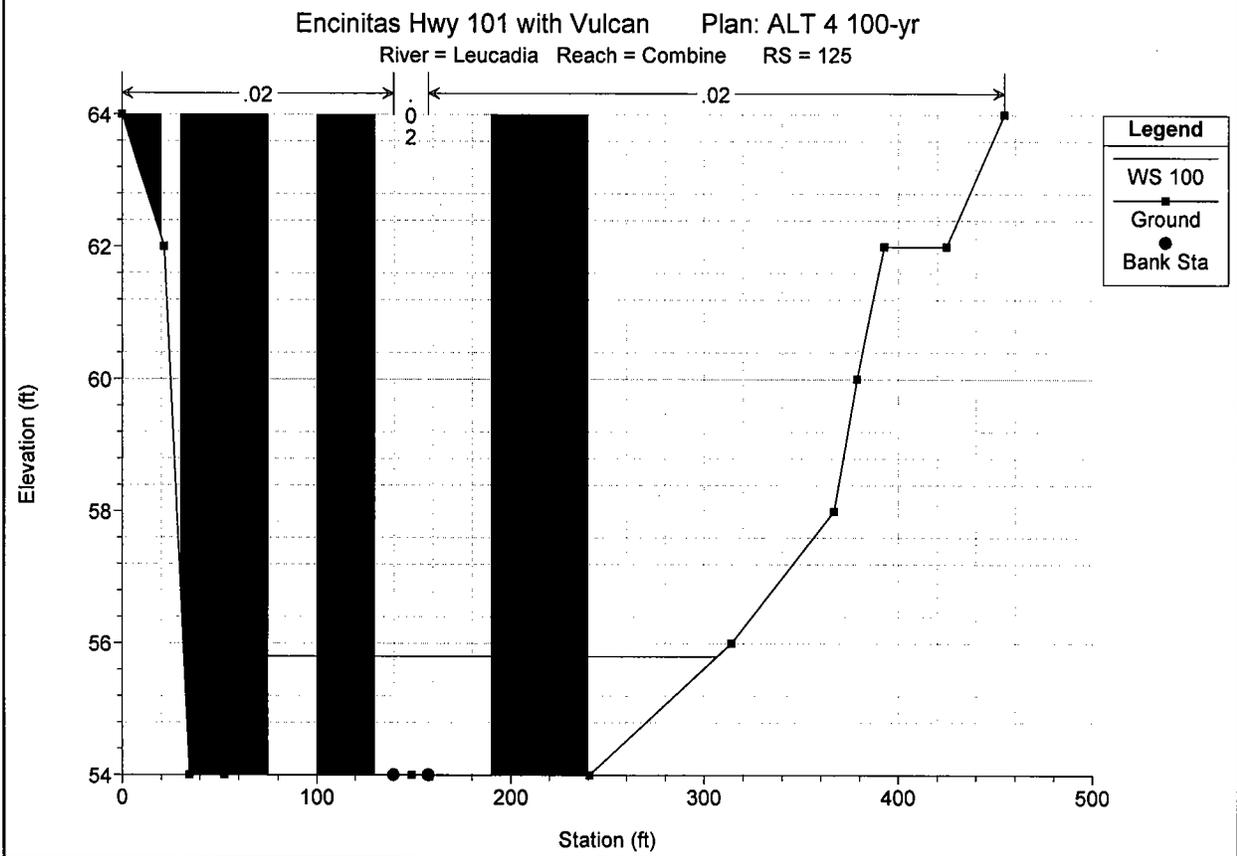
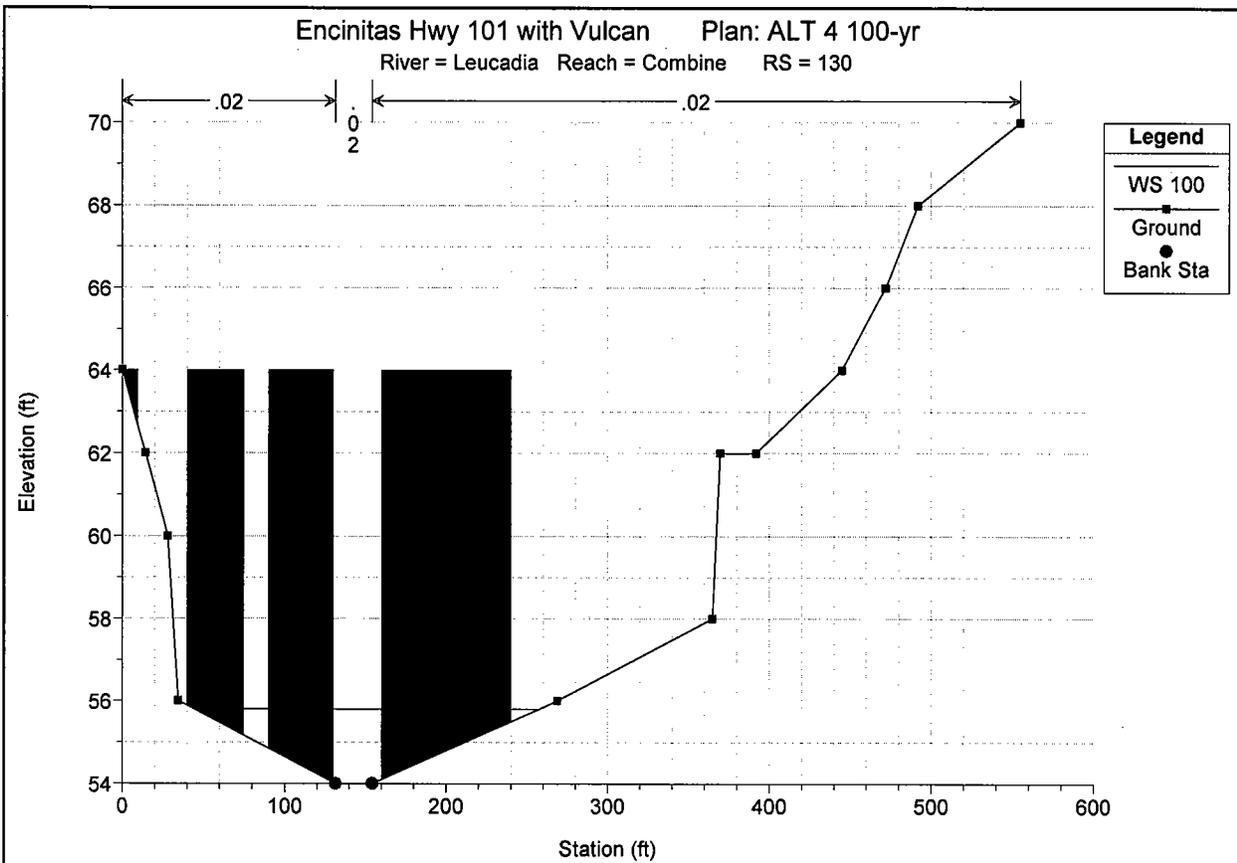


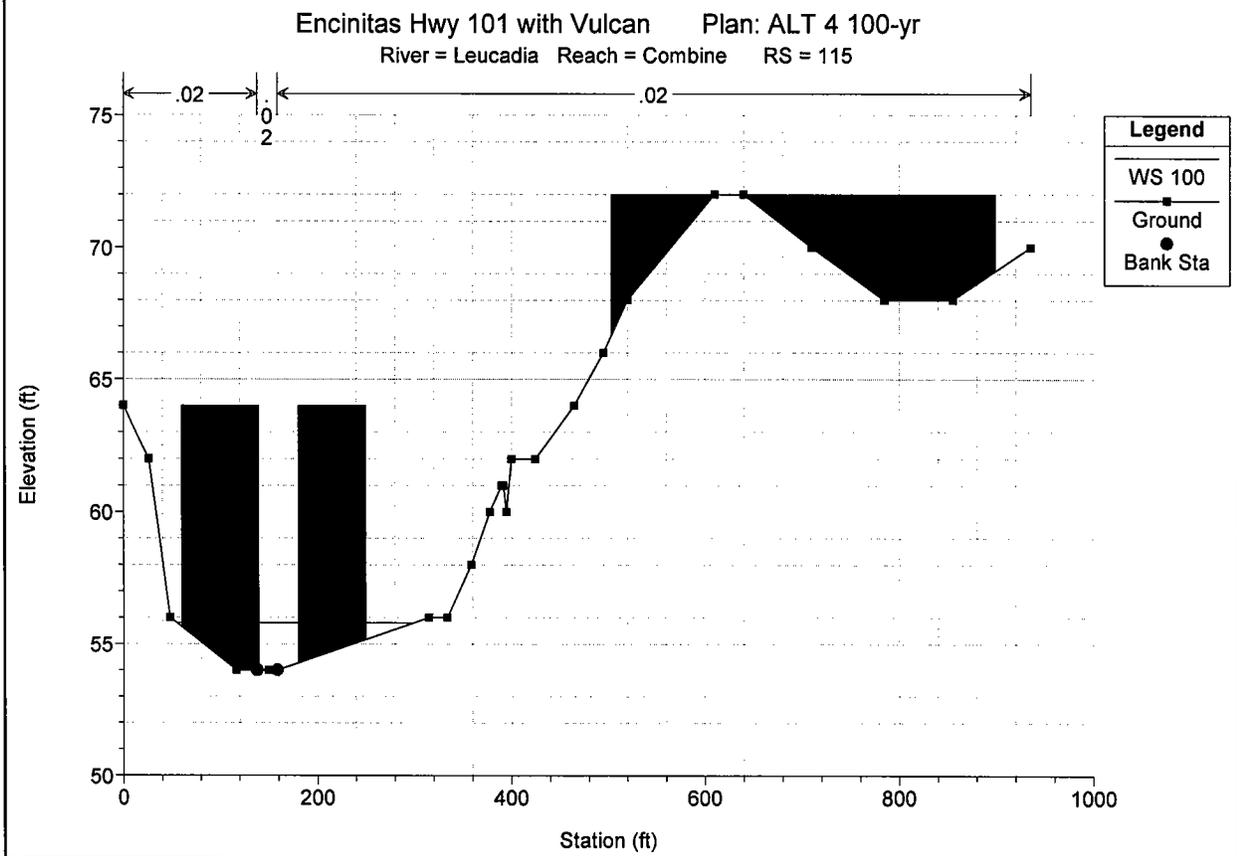
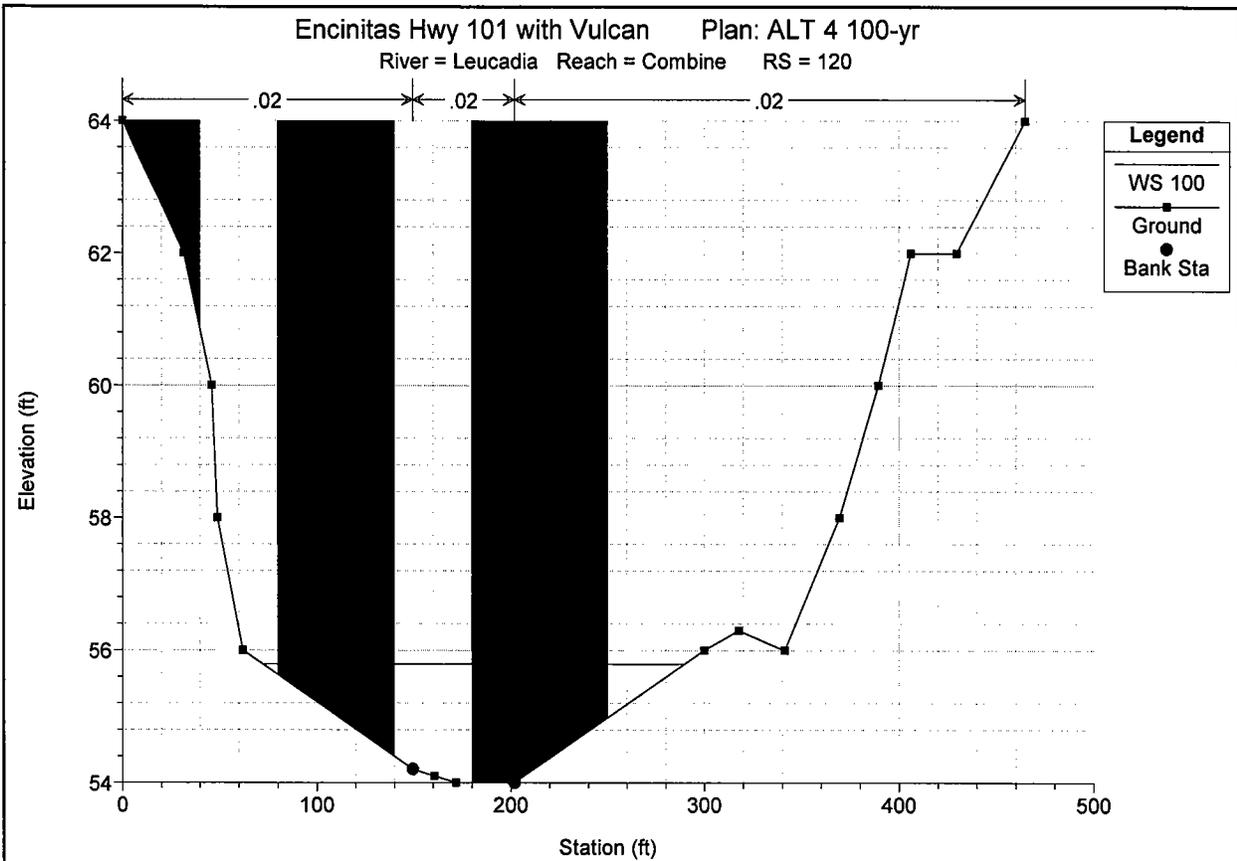
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = Combine RS = 140



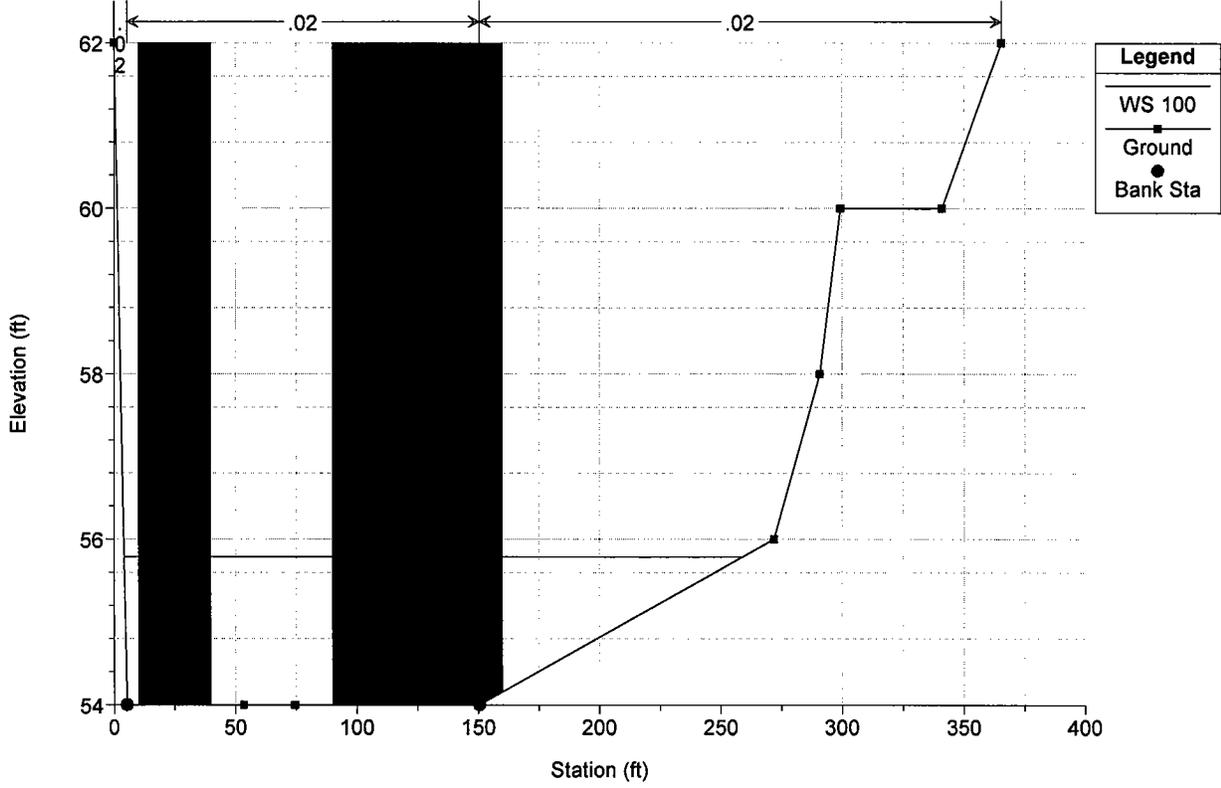
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = Combine RS = 135



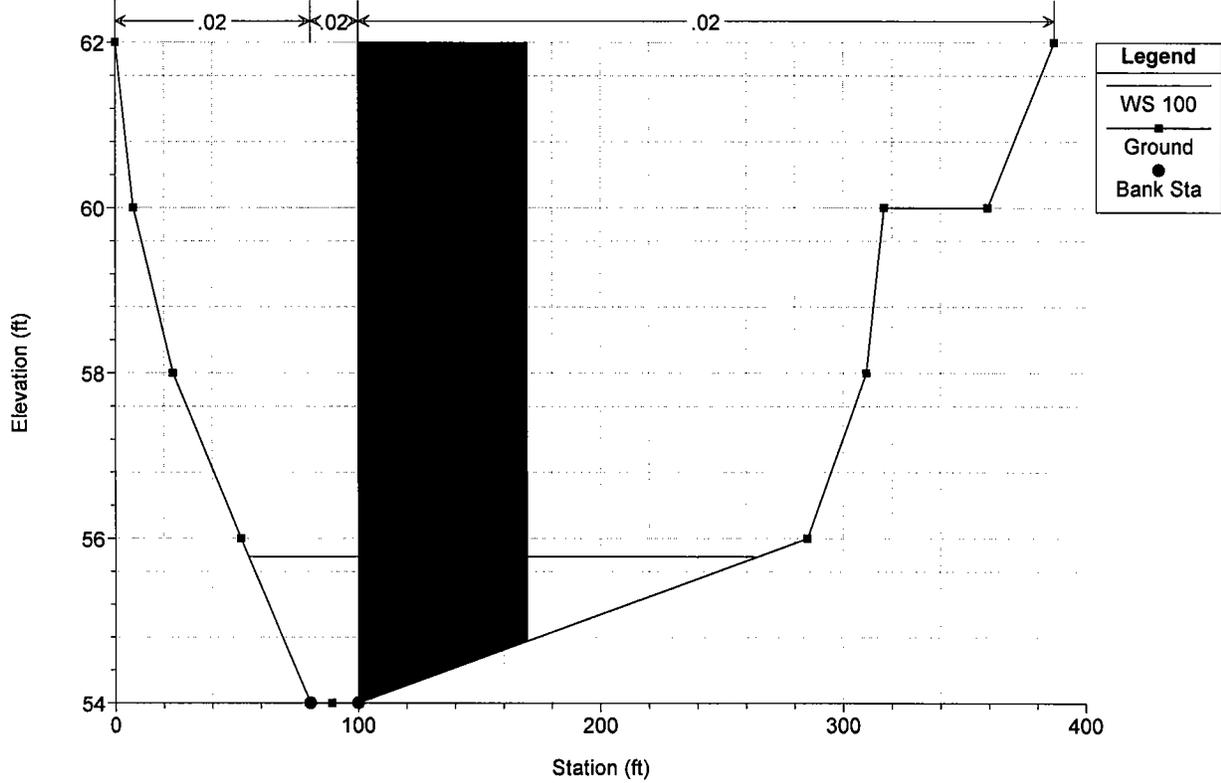




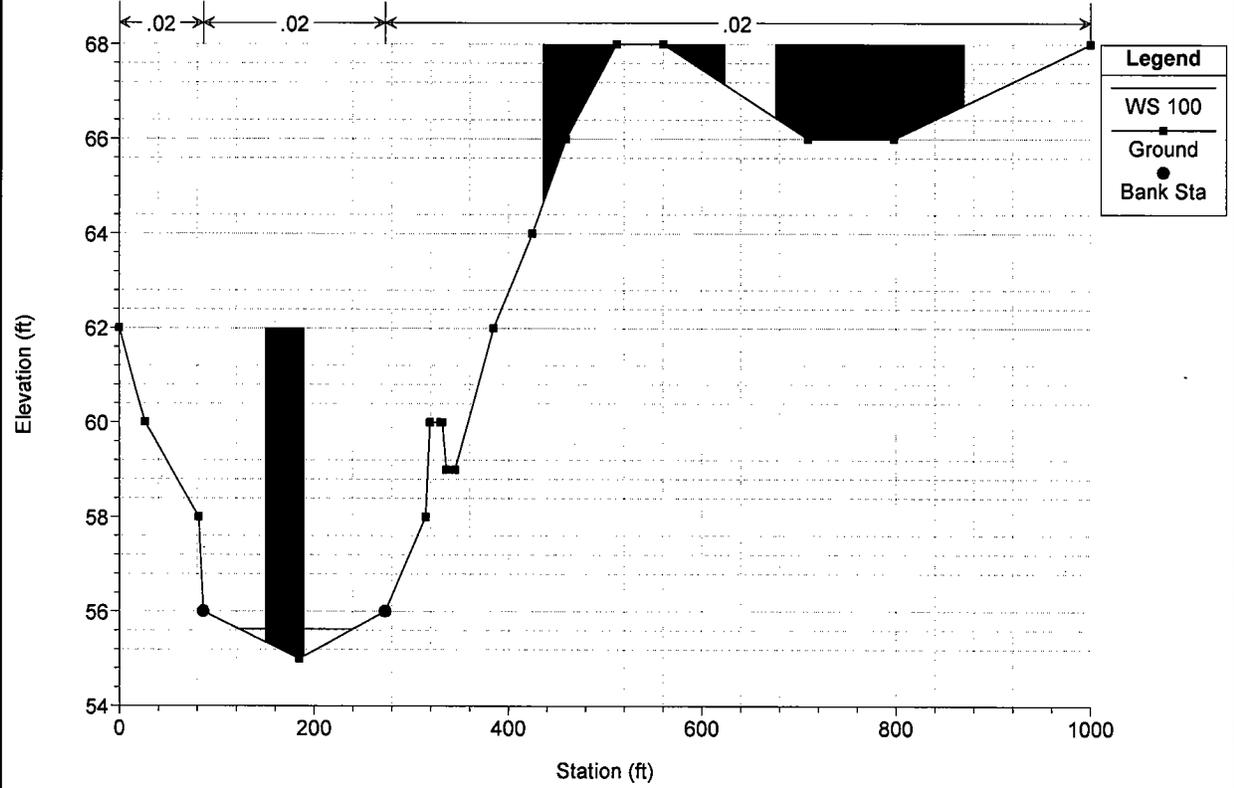
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = Combine RS = 110



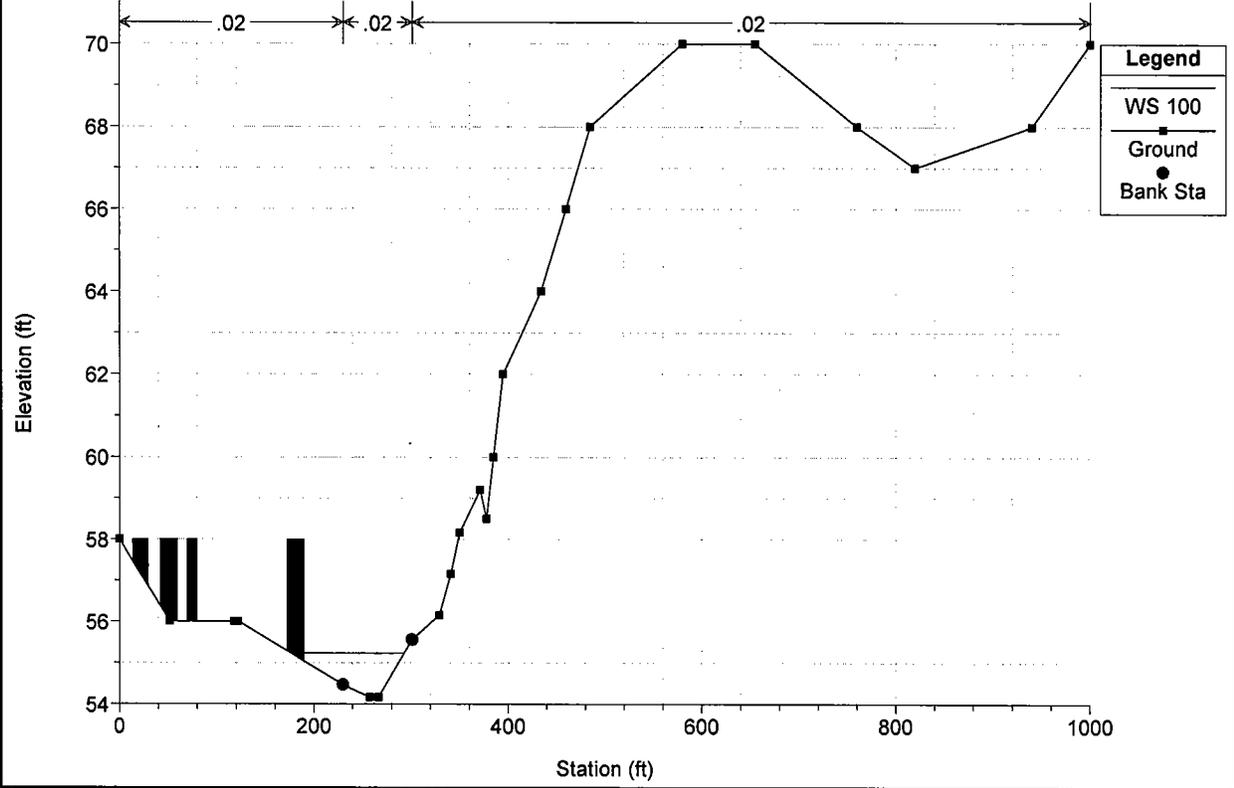
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = Combine RS = 105

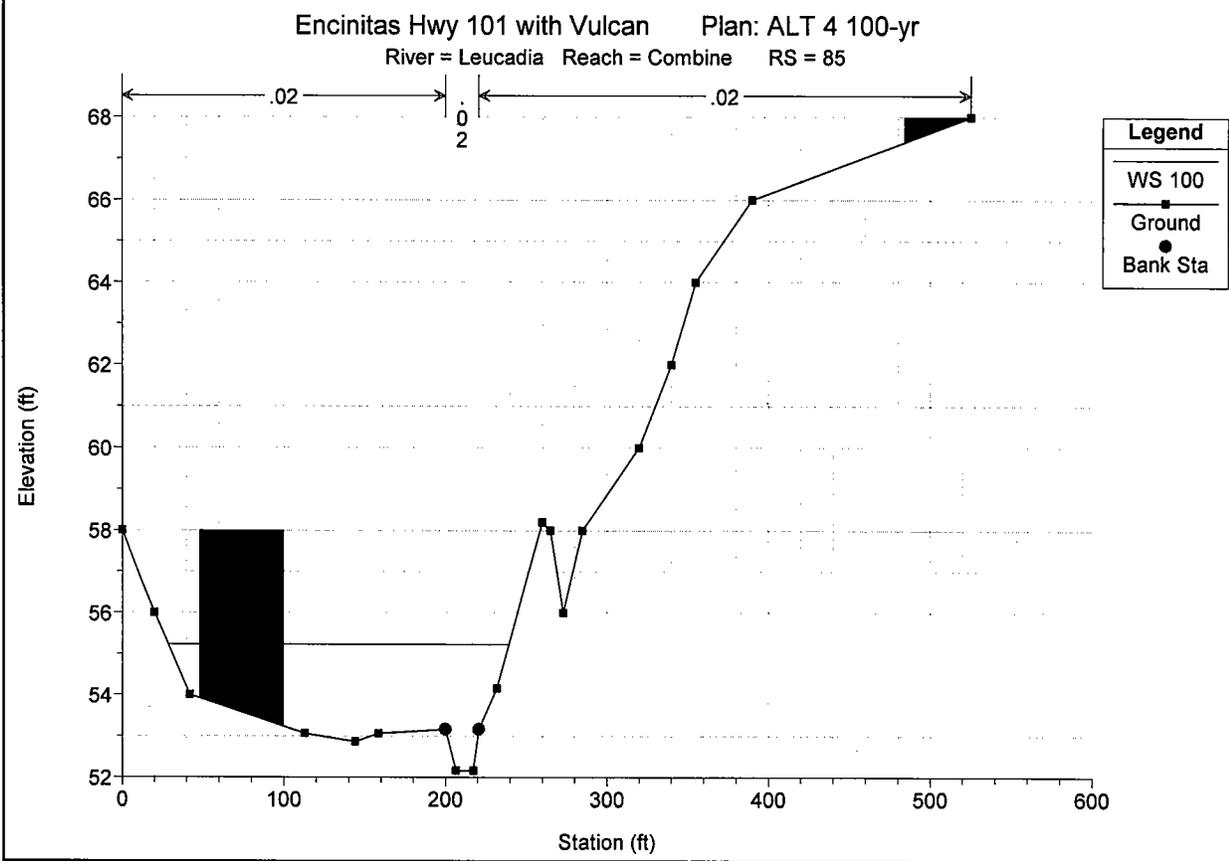
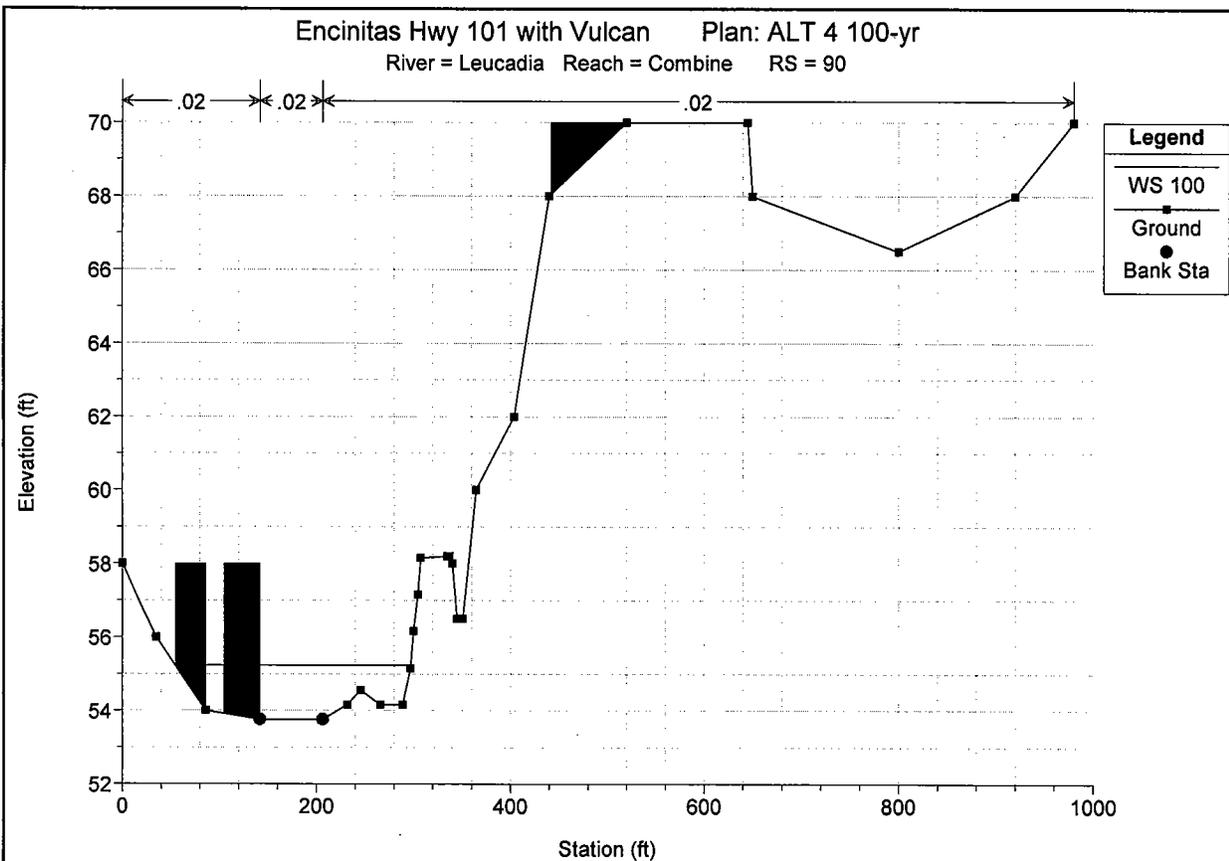


Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = Combine RS = 100

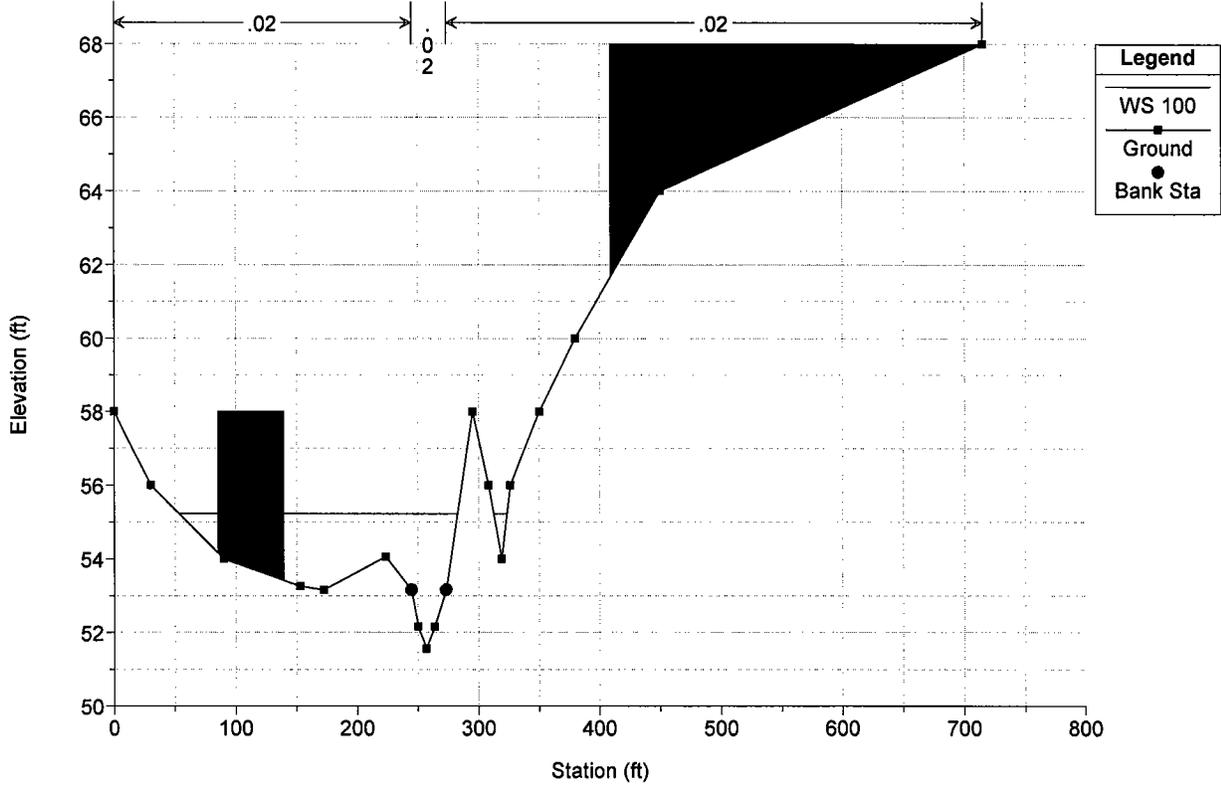


Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = Combine RS = 95

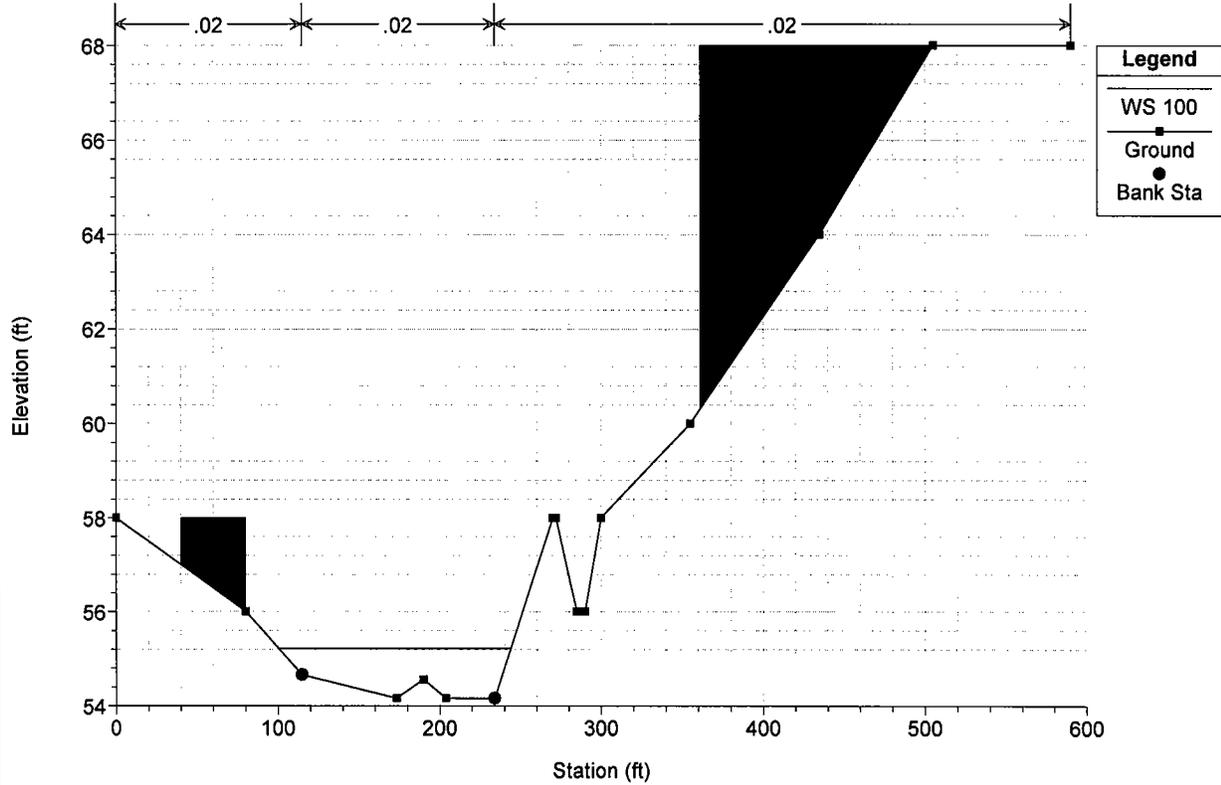




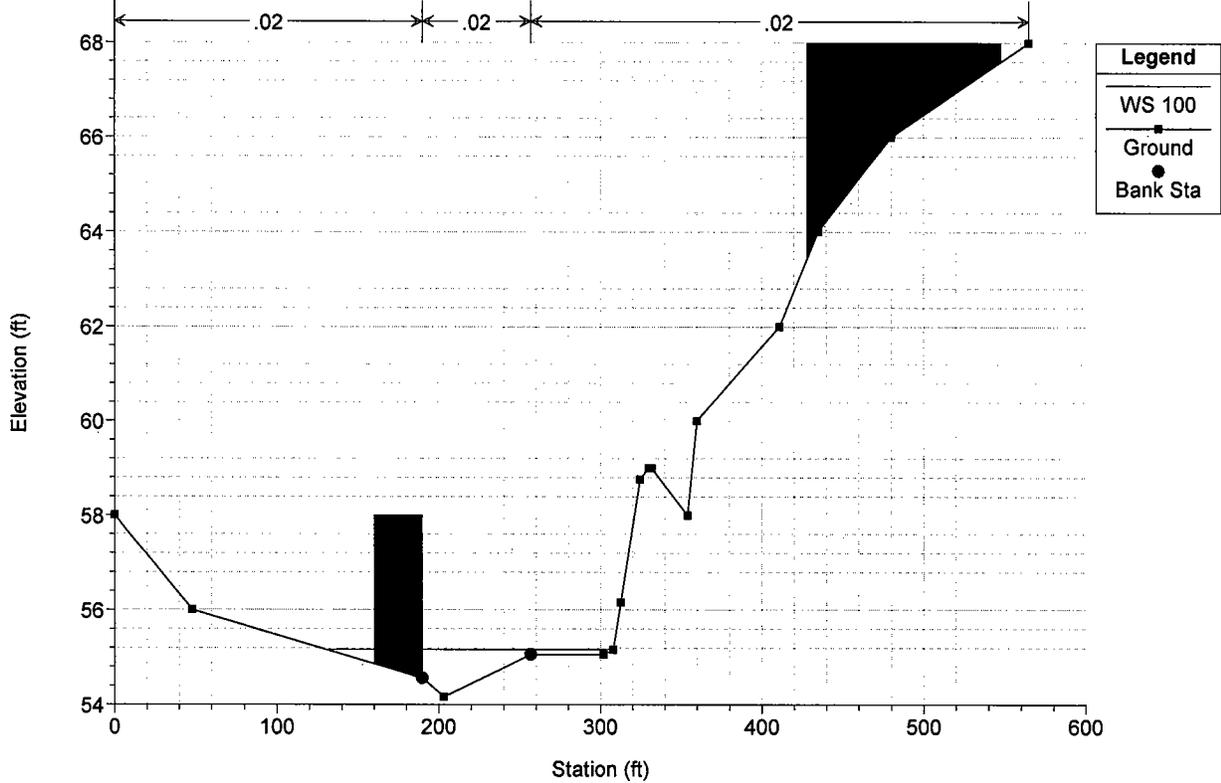
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = Combine RS = 80



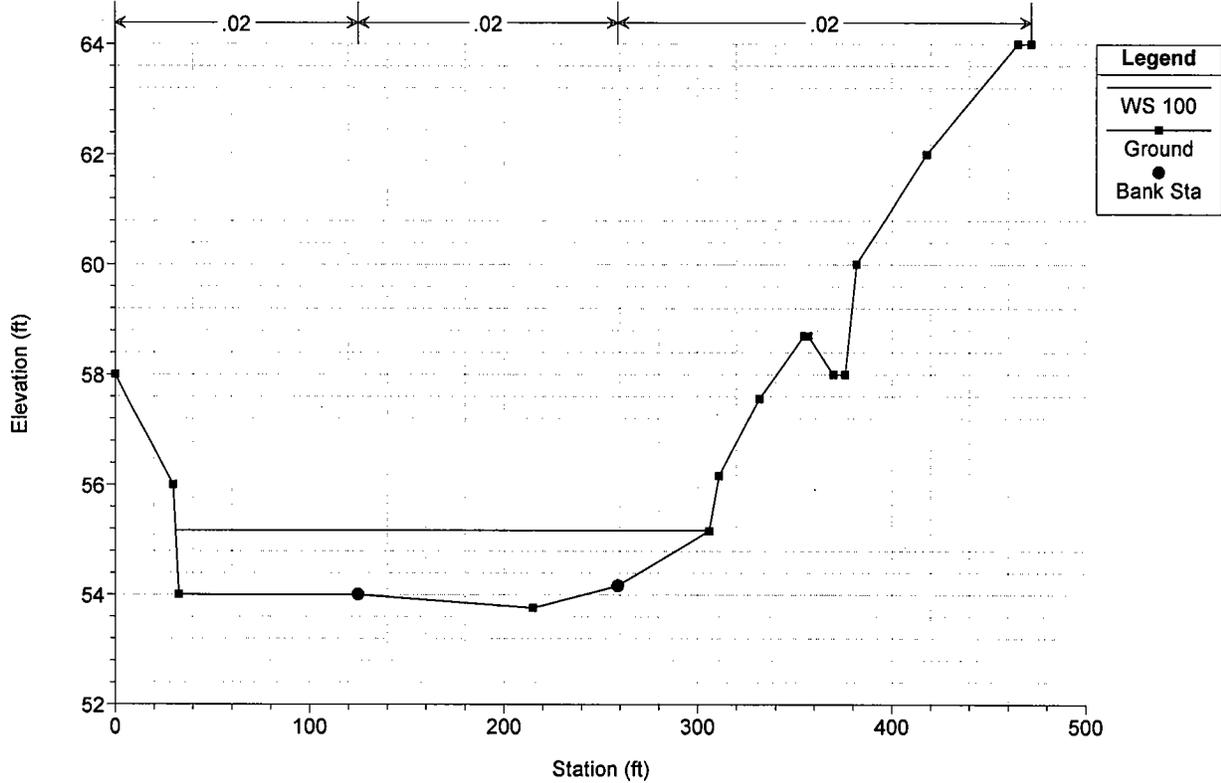
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = Combine RS = 75



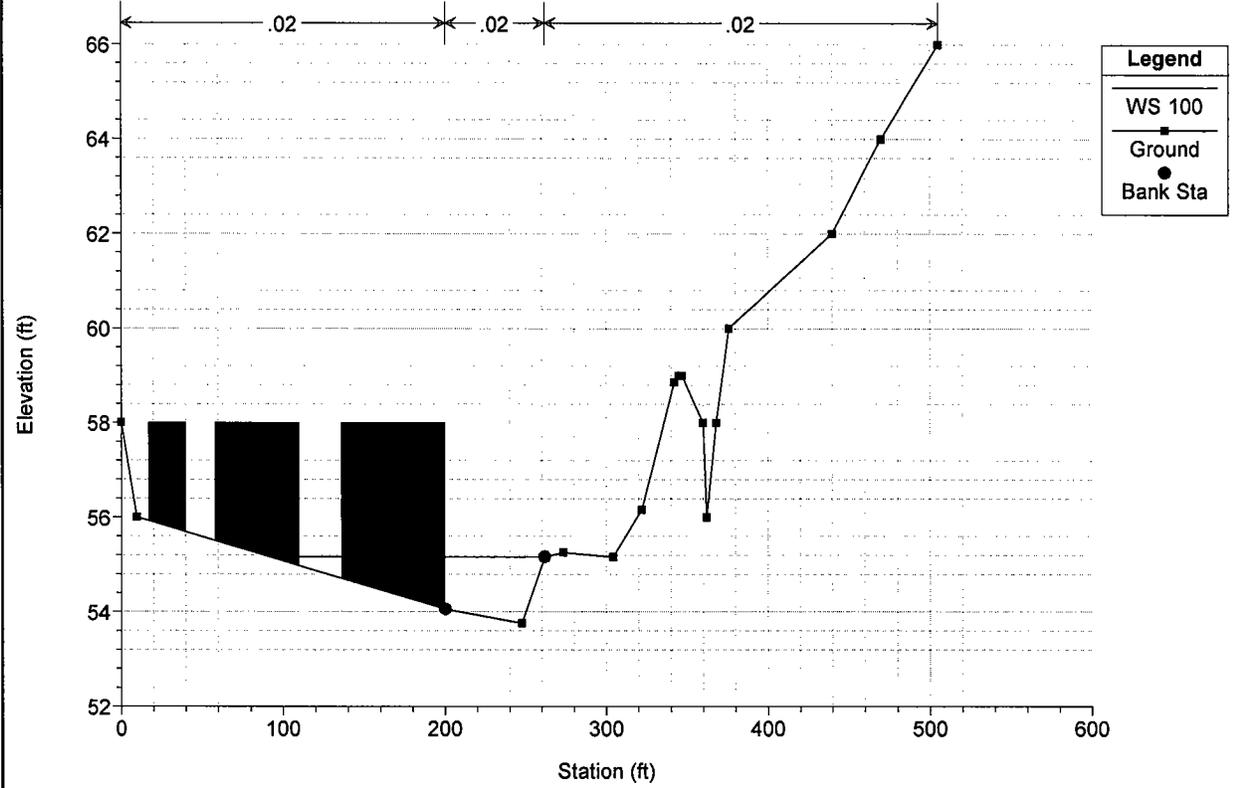
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = Combine RS = 70



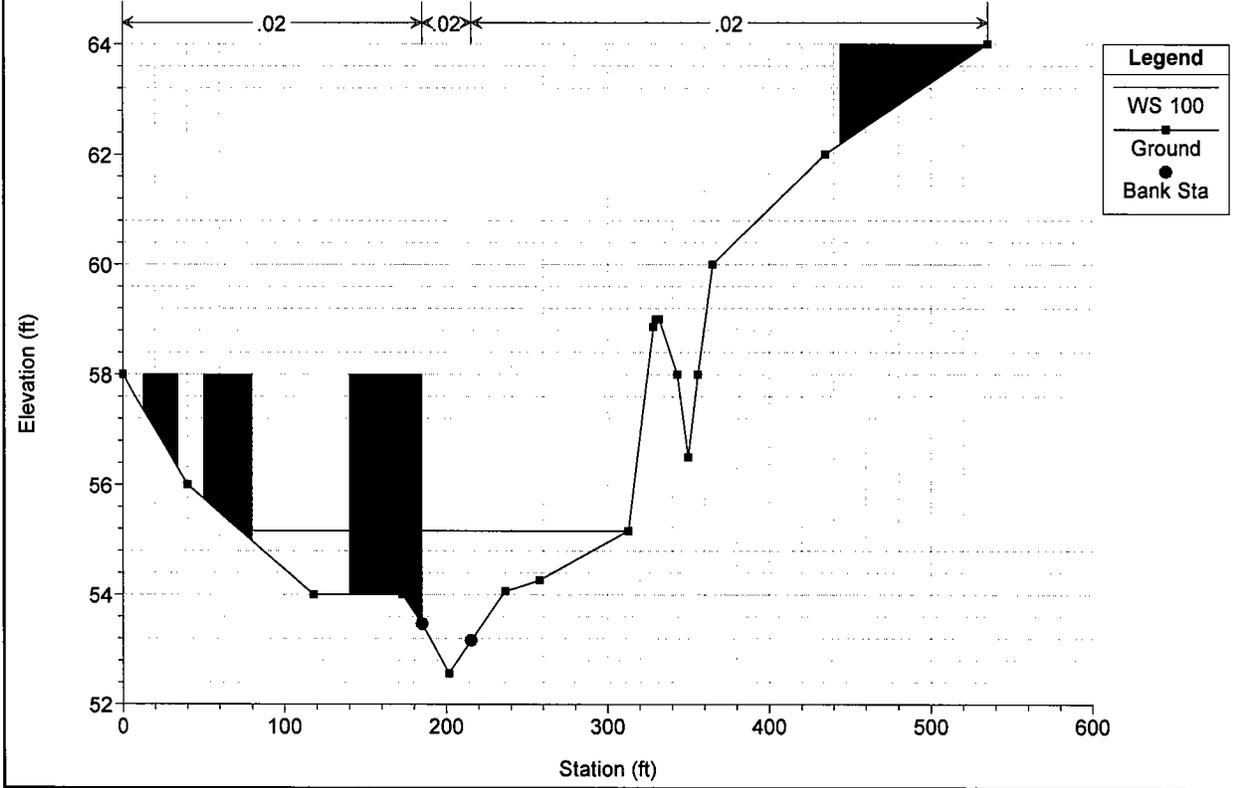
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = Combine RS = 65

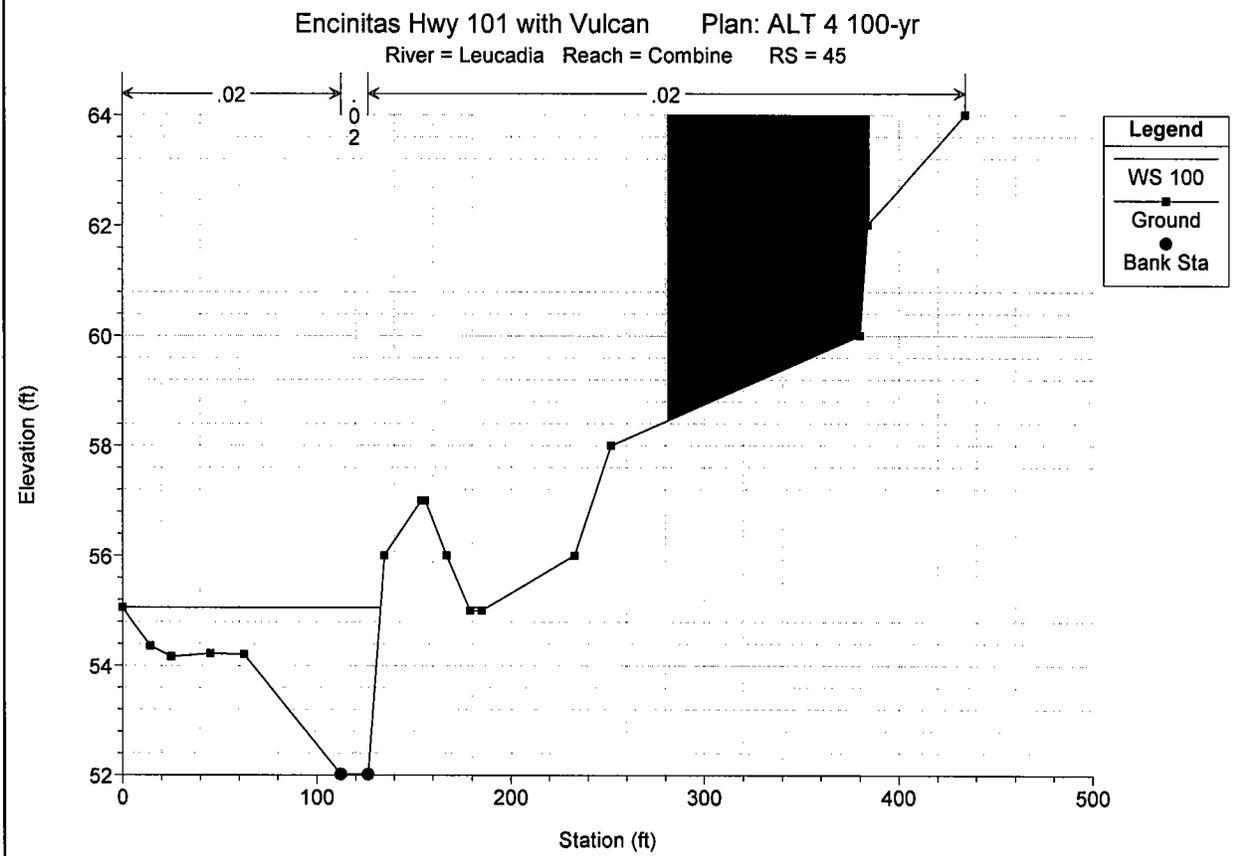
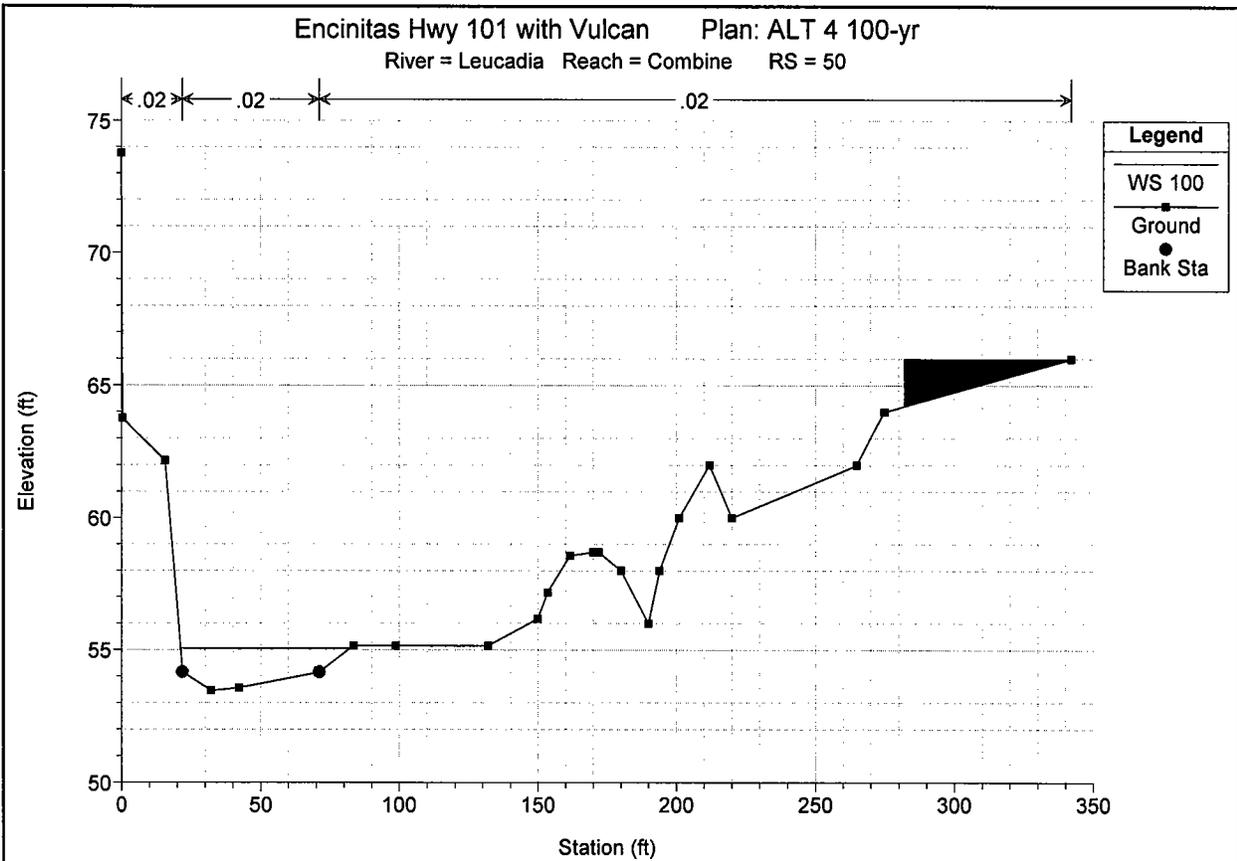


Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = Combine RS = 60

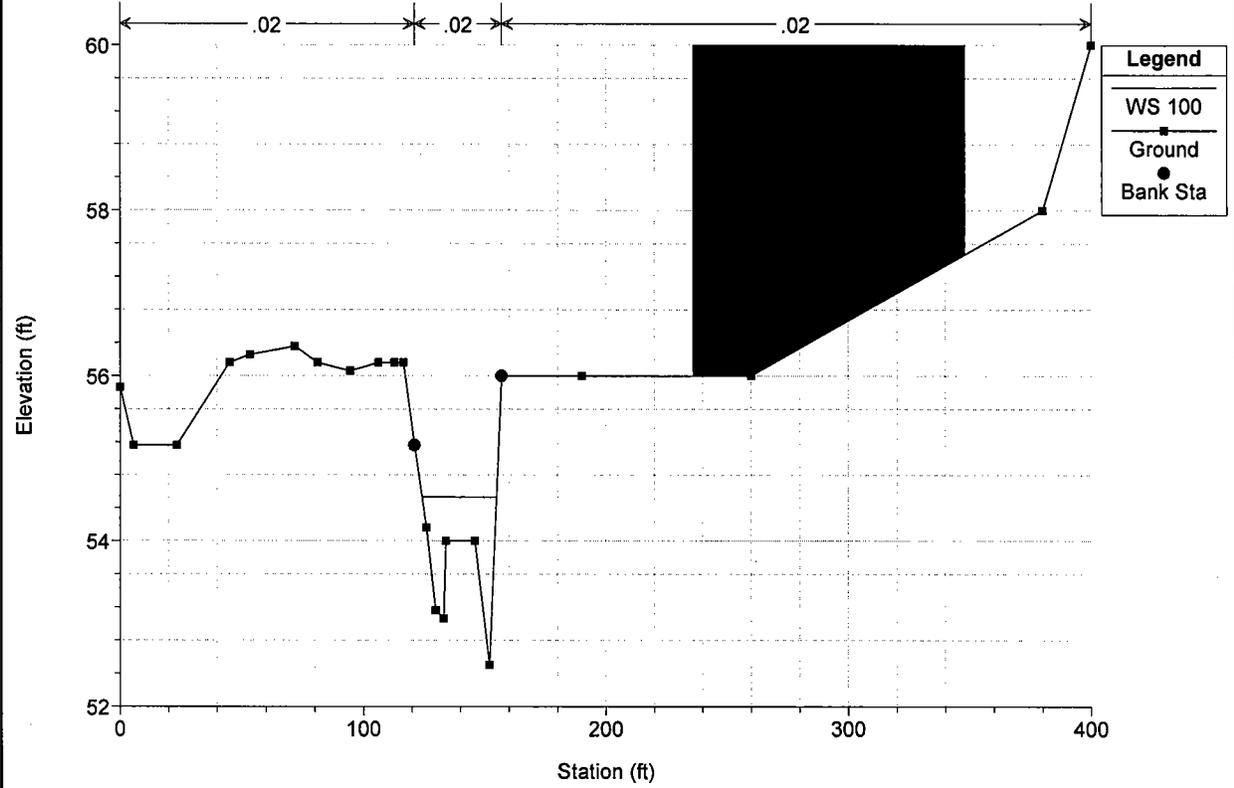


Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = Combine RS = 55

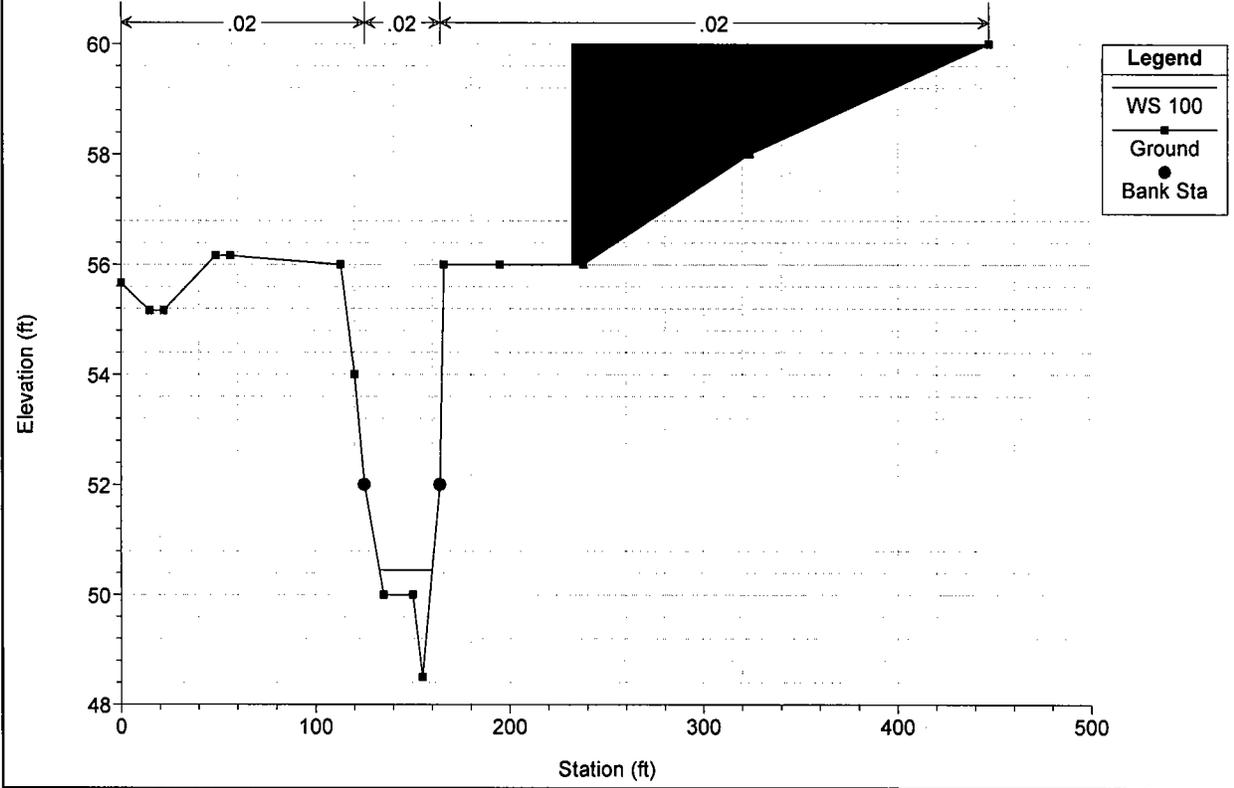




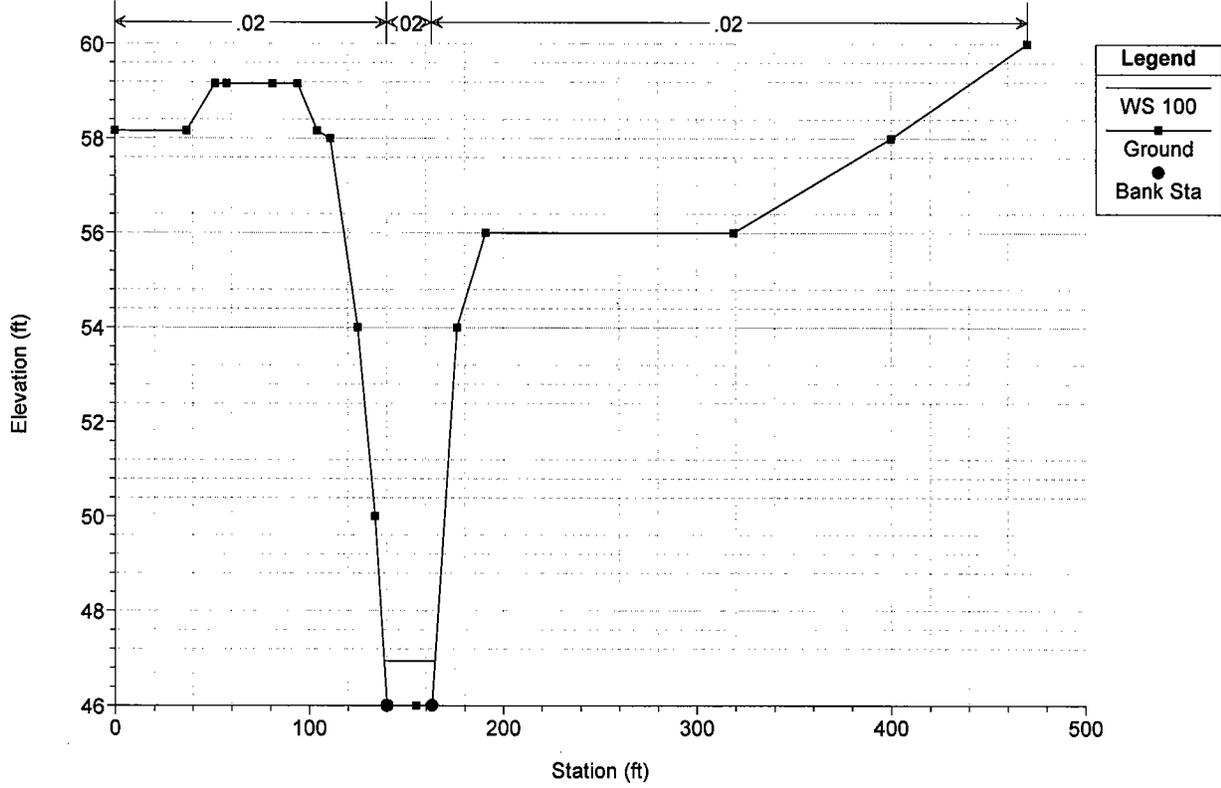
Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = Combine RS = 40



Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = Combine RS = 35



Encinitas Hwy 101 with Vulcan Plan: ALT 4 100-yr  
 River = Leucadia Reach = Combine RS = 30



HEC-RAS Version 3.0.1 Mar 2001  
 U.S. Army Corp of Engineers  
 Hydrologic Engineering Center  
 609 Second Street, Suite D  
 Davis, California 95616-4687  
 (916) 756-1104

```

X   X  XXXXXX   XXXX       XXXX       XX       XXXX
X   X  X       X   X       X   X       X   X   X
X   X  X       X           X   X       X   X   X
XXXXXXXX XXXX   X           XXX XXXX   XXXXXXX XXXX
X   X  X       X           X   X       X   X   X
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PROJECT DATA

Project Title: Encinitas Hwy 101 with Vulcan  
 Project File : 101Vul.prj  
 Run Date and Time: 8/30/2004 6:43:46 AM

Project in English units

Project Description:

ENCINITAS COAST HIGHWAY 101 -100-YR & 10-YR ANALYSIS  
 JN: 14413 DECEMBER 23,  
 2003  
 BASED ON HEC-2 FILENAME: ENC\_1.HC2  
 X-SECTIONS LEFT TO RIGHT LOOKING  
 DOWNSTREAM

PLAN DATA

Plan Title: ALT 4 100-yr  
 Plan File : w:\14413\Hec-Ras 101\101Vul.p01

Geometry Title: 101/Vulcan Combined  
 Geometry File : w:\14413\Hec-Ras 101\101Vul.g07

Flow Title : 101/Vulcan 100yr Qs 10yr diverted  
 Flow File : w:\14413\Hec-Ras 101\101Vul.f21

Plan Description:

10-YEAR RUN\*\* Includes blocked obstructions in alley  
 Varying Qs based on HEC-1  
 FN: 100det8.hcl  
 Extended XS from 95 down to encompass 100-yr  
 floodplain  
 Vertical Datum NAVD 88

Plan Summary Information:

Number of:	Cross Sections =	65	Multitple Openings =	0
	Culverts =	0	Inline Weirs =	0
	Bridges =	0		

Computational Information

Water surface calculation tolerance =	0.003
Critical depth calculaton tolerance =	0.003
Maximum number of interations =	20
Maximum difference tolerance =	0.1
Flow tolerance factor =	0.001

Computation Options

Critical depth computed only where necessary
Conveyance Calculation Method: At breaks in n values only
Friction Slope Method: Average Conveyance
Computational Flow Regime: Mixed Flow

FLOW DATA

Flow Title: 101/Vulcan 100yr Qs 10yr diverted  
 Flow File : w:\14413\Hec-Ras 101\101Vul.f21

Flow Data (cfs)

River	Reach	RS	
Leucadia	Vulcan	3300.14	100
Leucadia	Vulcan	240	13
Leucadia	Vulcan	195	1
Leucadia	101	230	38
Leucadia	101	225.3	1
Leucadia	101	190	1
Leucadia	Combine	140	47
Leucadia	Combine	120	50
Leucadia	Combine	105	51
Leucadia	Combine	90	44
Leucadia	Combine	75	46
Leucadia	Combine	60	56
Leucadia	Combine	50	138

Boundary Conditions

River	Reach	Profile	Upstream	
Downstream				
Leucadia	Vulcan	100	Critical	
Leucadia	101	100	Critical	
Leucadia	Combine	100		Normal S

= .01

GEOMETRY DATA

Geometry Title: 101/Vulcan Combined  
 Geometry File : w:\14413\Hec-Ras 101\101Vul.g07

Reach Connection Table

River	Reach	Upstream Boundary	Downstream Boundary
Leucadia	Vulcan		Junction
Leucadia	101		Junction
Leucadia	Combine	Junction	

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 3300.14

INPUT

Description:

Station Elevation Data		num= 21							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
110	76.16	143	76.56	151	76.16	155	77.16	165	77.56
170	77.56	180	77.16	182.3	74.76	193.6	74.56	196	72.16
204	72.16	206.4	74.56	215.5	74.76	222	74	230	74
240	74.1	245	74	273	74	300	74.46	390	76
420	78								

Manning's n Values

Sta	n Val	Sta	n Val	Sta	n Val
110	.03	196	.035	204	.03

Bank Sta: Left 196 Right 204 Lengths: Left Channel 100 Right Channel 100  
 Left Levee Station= 169.51 Elevation= 77.58 Coeff Contr. .1 Expan. .3

CROSS SECTION RIVER: Leucadia



Left Levee      196      204      100      100      100      .1      .3  
 Station= 169.51      Elevation= 75.38

CROSS SECTION      RIVER: Leucadia  
 REACH: Vulcan      RS: 2800.19

INPUT

Description:  
 Station Elevation Data      num=      17  
 Sta      Elev      Sta      Elev      Sta      Elev      Sta      Elev      Sta      Elev  
 70      70.06      113      69.46      126      70.16      150      71.16      155      73.16  
 160      74.16      164      74.66      169      74.66      174      74.16      175.1      73.56  
 192      73.26      196      69.26      204      69.26      208      73.26      225      74.16  
 456      76      523      78

Manning's n Values      num=      3  
 Sta      n Val      Sta      n Val      Sta      n Val  
 70      .03      196      .035      204      .03

Bank Sta: Left      Right      Lengths: Left Channel      Right      Coeff Contr.      Expan.  
 196      204      100      100      100      .1      .3  
 Left Levee      Station= 168.93      Elevation= 74.71

CROSS SECTION      RIVER: Leucadia  
 REACH: Vulcan      RS: 2700.20

INPUT

Description:  
 Station Elevation Data      num=      18  
 Sta      Elev      Sta      Elev      Sta      Elev      Sta      Elev      Sta      Elev  
 125      68.16      139      68.86      146      69.16      150      70.16      154      71.16  
 160      73.16      165      73.86      170      73.86      175      73.16      176.2      72.26  
 192      71.96      196      67.96      204      67.96      208      71.96      212.73      72.57  
 258      74      423      76      535      78

Manning's n Values      num=      3  
 Sta      n Val      Sta      n Val      Sta      n Val  
 125      .03      196      .035      204      .03

Bank Sta: Left      Right      Lengths: Left Channel      Right      Coeff Contr.      Expan.  
 196      204      100      100      100      .1      .3  
 Left Levee      Station= 170.68      Elevation= 73.86

CROSS SECTION      RIVER: Leucadia  
 REACH: Vulcan      RS: 2600.21

INPUT

Description:  
 Station Elevation Data      num=      20  
 Sta      Elev      Sta      Elev      Sta      Elev      Sta      Elev      Sta      Elev  
 109      66.46      135      66.46      146      68.16      152      69.16      155      70.16  
 157      71.16      162      73.16      165      73.26      170      73.26      173      73.16  
 181      71.16      185.1      70.06      192      69.96      196      65.96      204      65.96  
 208      69.96      215.42      70.99      237      72      286      74      456      76

Manning's n Values      num=      3  
 Sta      n Val      Sta      n Val      Sta      n Val  
 109      .03      196      .035      204      .03

Bank Sta: Left      Right      Lengths: Left Channel      Right      Coeff Contr.      Expan.  
 196      204      100      100      100      .1      .3  
 Left Levee      Station= 170.09      Elevation= 73.26

CROSS SECTION      RIVER: Leucadia  
 REACH: Vulcan      RS: 2500.22

INPUT

Description:  
 Station Elevation Data      num=      17  
 Sta      Elev      Sta      Elev      Sta      Elev      Sta      Elev      Sta      Elev  
 139      65.16      150      68.16      158      71.16      165      72.76      170      72.76  
 175      71.16      182      69.16      184      68.66      192      68.46      196      64.46  
 204      64.46      208      68.46      213.55      69.25      233      70      266      72  
 320      74      498      76

Manning's n Values      num=      3

Sta	n Val	Sta	n Val	Sta	n Val						
139	.03	196	.035	204	.03						
Bank Sta: Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.				
	196	204	100	100		.1	.3				
Left Levee	Station=	170.09	Elevation=	72.78							

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 2400.23

INPUT

Description:  
 Station Elevation Data num= 18

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
95	65.56	142	65.16	160	71.16	165	72.46	170	72.46
175	71.16	180	70.16	183	68	192	67.9	194.8	68.16
202	67.96	206	63.96	214	63.96	218	67.96	221.32	68.78
250	70	263	72	360	74				

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
95	.03	206	.035	214	.03

Bank Sta: Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	206	214	100	100		.1	.3
Left Levee	Station=	169.39	Elevation=	72.47			

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 2300.24

INPUT

Description:  
 Station Elevation Data num= 18

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
2	64.46	129	64.46	141	65.16	160	71.16	165	71.86
170	71.86	175	71.16	185	68.16	190	67	195.2	67.66
202	67.46	206	63.46	214	63.46	218	67.46	221.7	68.36
260	70	316	72	382	74				

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
2	.03	206	.035	214	.03

Bank Sta: Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	206	214	100	100		.1	.3
Left Levee	Station=	170.56	Elevation=	71.89			

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 2200.25

INPUT

Description:  
 Station Elevation Data num= 15

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
140	64.16	160	71.16	165	71.46	170	71.46	172	71.16
182	68.16	184.7	66.86	192.3	66.76	196	62.96	204	62.96
207.7	66.76	217	66.86	260	68	287	70	342	72

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
140	.03	196	.035	204	.03

Bank Sta: Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	196	204	100	100		.1	.3
Left Levee	Station=	170.39	Elevation=	71.43			

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 2100.26

INPUT

Description:  
 Station Elevation Data num= 20

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
144	63.16	164	71.16	165	71.36	170	71.36	175	71.16
182	68.16	186	66	188.3	64.96	193.6	64.86	196	62.46
204	62.46	206.4	64.86	217	65.06	234	66	240	66.1

245 66 248 65.9 252 66 286 68 322 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 144 .03 196 .035 204 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 196 204 15 15 15  
 Left Levee Station= 169.8 Elevation= 71.43

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 245

INPUT  
 Description:  
 Station Elevation Data num= 11  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 70 10 70 16 68 24 66 30 64  
 40 64 70 66 80 66 87 66 122 68  
 180 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .03 30 .035 40 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 30 40 175 175 175  
 .1 .3

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 240

INPUT  
 Description:  
 Station Elevation Data num= 9  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 70 5 70 10 68 20 66 27 64  
 39 64 89 66 185 68 230 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .03 27 .035 39 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 27 39 275 275 275  
 .1 .3

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 235

INPUT  
 Description:  
 Station Elevation Data num= 6  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 68 10 68 15 66 140 66 205 68  
 246 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .03 15 .035 140 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 15 140 120 120 120  
 .1 .3

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 230

INPUT  
 Description:  
 Station Elevation Data num= 11  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 430 70 460 70 520 68 525 68 544 69.8  
 546 69.8 550 68 580 66 715 66 770 68  
 825 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 430 .02 580 .02 715 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 580 715 175 180 185 .1 .3  
 Blocked Obstructions num= 1  
 Sta L Sta R Elev  
 797 825 70

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 225

INPUT

Description:

Station Elevation Data num= 8  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 536 69.8 538 69.8 542 68 595 66 625 66  
 785 66 827 68 835 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 536 .02 595 .02 785 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 595 785 190 185 185 .1 .3  
 Blocked Obstructions num= 1  
 Sta L Sta R Elev  
 692 835 70

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 220

INPUT

Description:

Station Elevation Data num= 7  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 494 69.9 496 69.9 518 68 580 66 876 66  
 900 68 910 72

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 494 .02 580 .02 876 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 580 876 175 175 175 .1 .3

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 215

INPUT

Description:

Station Elevation Data num= 15  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 540 69.9 542 69.9 546 68 552 67.9 556 68  
 565 70 580 70.1 594 70 600 69.9 610 70  
 670 68 815 66 860 66 945 68 995 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 540 .02 546 .02 556 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 546 556 290 290 290 .1 .3  
 Blocked Obstructions num= 1  
 Sta L Sta R Elev  
 765 995 70

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 195

INPUT

Description:

Station Elevation Data num= 15  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 485 70 496 70 505 68 510 68 515 70  
 520 72 525 74 533 74 612 72 652 70  
 695 68 780 66 820 66 920 68 985 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 485 .02 505 .02 510 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 505 510 340 340 340 .1 .3

Blocked Obstructions num= 2  
 Sta L Sta R Elev Sta L Sta R Elev  
 835 903 74 930 985 74

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 175

INPUT

Description:  
 Station Elevation Data num= 7  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 335 68 337 68 344 66 348 65.5 350 66  
 765 68 847 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 335 .02 344 .02 350 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 344 350 225 220 220 .1 .3

Blocked Obstructions num= 2  
 Sta L Sta R Elev Sta L Sta R Elev  
 525 712 70 739 847 70

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 165

INPUT

Description:  
 Station Elevation Data num= 14  
 Sta Elev  
 392 67 394 67 395 66 400 64 410 63  
 418 64 436 66 472 68 512 70 555 72  
 620 72 700 70 795 68 895 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 392 .02 400 .02 418 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 400 418 360 360 360 .1 .3

Blocked Obstructions num= 2  
 Sta L Sta R Elev Sta L Sta R Elev  
 546 781 72 826 895 72

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 150

INPUT

Description:  
 Station Elevation Data num= 12  
 Sta Elev  
 380 65 382 65 385 64 400 63 413 64  
 486 66 520 70 565 74 698 74 750 72  
 967 72 1040 74

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 380 .02 385 .02 413 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 385 413 305 305 305 .1 .3

Blocked Obstructions num= 1  
 Sta L Sta R Elev  
 606 1040 74

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 230

INPUT

Description:  
 Station Elevation Data num= 8  

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	66	25.4	64	30.5	62	88.9	60.2	146	60
243.4	62	278	64	318.4	66				

  
 Manning's n Values num= 3  

Sta	n Val	Sta	n Val	Sta	n Val
0	.02	88.9	.02	146	.02

  
 Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  

Left	Right	Left	Channel	Right	Coeff	Contr.	Expan.
88.9	146	104.1	100.2	136.3		.1	.3

  
 Blocked Obstructions num= 3  

Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta L	Sta R	Elev
50	80	66	145	190	66	285	350	66

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 225.3

INPUT

Description:  
 Station Elevation Data num= 14  

Sta	Elev								
0	66	16	64	32.6	62	78.4	60	126.9	58
133.4	58	139.4	58	203.7	58	210.3	58	216.8	58.5
233.9	60	285.5	62	319.2	64	355	66		

  
 Manning's n Values num= 3  

Sta	n Val	Sta	n Val	Sta	n Val
0	.02	126.9	.02	203.7	.02

  
 Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  

Left	Right	Left	Channel	Right	Coeff	Contr.	Expan.
126.9	203.7	5	5	5		.1	.3

  
 Blocked Obstructions num= 5  

Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta L	Sta R	Elev
5	30	66	130	160	66	180	200	66
210	235	66	300	345	66			

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 225.2

INPUT

Description:  
 Station Elevation Data num= 14  

Sta	Elev								
0	66	16	64	32.6	62	78.4	60	126.9	58
133.4	54	139.4	54	203.7	56	210.3	58	216.8	58.5
233.9	60	285.5	62	319.2	64	355	66		

  
 Manning's n Values num= 3  

Sta	n Val	Sta	n Val	Sta	n Val
0	.02	126.9	.02	203.7	.02

  
 Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  

Left	Right	Left	Channel	Right	Coeff	Contr.	Expan.
126.9	203.7	5	5	5		.1	.3

  
 Blocked Obstructions num= 5  

Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta L	Sta R	Elev
5	30	66	130	160	66	180	200	66
210	235	66	300	345	66			

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 225.1

INPUT

Description:  
 Station Elevation Data num= 14  

Sta	Elev								
0	66	16	64	32.6	62	78.4	60	126.9	58
133.4	58	139.4	58	203.7	58	210.3	58	216.8	58.5
233.9	60	285.5	62	319.2	64	355	66		

  
 Manning's n Values num= 3  

Sta	n Val	Sta	n Val	Sta	n Val
0	.02	126.9	.02	203.7	.02

  
 Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.

Blocked Obstructions	126.9	203.7		134.2	131.9	133.3		.1	.3
	num=		5						
Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta L	Sta R	Elev	
5	30	66	130	160	66	180	200	66	
210	235	66	300	345	66				

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 220

INPUT

Description:

Station Elevation Data	num=		11						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	66	18.9	64	21	62	30.1	60	56.5	58
114.4	57.7	192	58	255	60	292.4	62	321.2	64
343.3	66								

Manning's n Values	num=		3						
Sta	n Val	Sta	n Val	Sta	n Val				
0	.02	56.5	.02	192	.02				

Bank Sta: Left	Right	Lengths: Left	Channel	Right	Coeff	Contr.	Expan.
56.5	192	222.7	215.1	206.1	.1	.3	

Blocked Obstructions	num=		3						
Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta L	Sta R	Elev	
20	60	66	105	140	66	155	190	66	

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 215

INPUT

Description:

Station Elevation Data	num=		14						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	66	10	64	35.7	62	75.9	60	102.5	58
121.6	56	143.9	56	204.1	56	241	56	286	58
307.5	60	345.4	62	377.3	64	381.6	66		

Manning's n Values	num=		3						
Sta	n Val	Sta	n Val	Sta	n Val				
0	.02	121.6	.02	241	.02				

Bank Sta: Left	Right	Lengths: Left	Channel	Right	Coeff	Contr.	Expan.
121.6	241	78.2	80.6	89.6	.1	.3	

Blocked Obstructions	num=		2						
Sta L	Sta R	Elev	Sta L	Sta R	Elev				
10	75	66	160	220	66				

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 210

INPUT

Description:

Station Elevation Data	num=		11						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	66	10.4	64	23.6	62	63.8	60	101.7	58
120.4	56	193.3	56	272.5	56	296.1	58	304.2	60
312.7	66								

Manning's n Values	num=		3						
Sta	n Val	Sta	n Val	Sta	n Val				
0	.02	120.4	.02	272.5	.02				

Bank Sta: Left	Right	Lengths: Left	Channel	Right	Coeff	Contr.	Expan.
120.4	272.5	47.1	45.4	64.5	.1	.3	

Blocked Obstructions	num=		2						
Sta L	Sta R	Elev	Sta L	Sta R	Elev				
20	170	66	210	250	66				

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 205

INPUT

Description:

Station Elevation Data	num=		9						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev

0	64	14	62	58.3	60	89	58	110.7	56
182	56	218.5	56	292.3	58	302.4	64		

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 110.7 .02 218.5 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 110.7 218.5 141.2 142.6 152.6 .1 .3  
 Blocked Obstructions num= 5  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 0 30 64 60 100 64 140 170 64  
 200 225 64 255 280 64

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 195

INPUT  
 Description:  
 Station Elevation Data num= 9  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 64 35.6 62 68.6 60 113.8 58 198.9 56  
 266.6 58 298.8 60 323.4 62 337.5 64

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 113.8 .02 266.6 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 113.8 266.6 143.6 102.4 81.7 .1 .3  
 Blocked Obstructions num= 3  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 95 130 64 150 180 64 210 255 64

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 190

INPUT  
 Description:  
 Station Elevation Data num= 8  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 64 16.8 62 31.4 60 99.1 58 133.4 58  
 179.5 58 217.5 60 231.5 64

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 99.1 .02 179.5 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 99.1 179.5 109.2 93.8 106 .1 .3  
 Blocked Obstructions num= 4  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 0 10 64 35 65 64 90 120 64  
 185 230 64

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 185

INPUT  
 Description:  
 Station Elevation Data num= 6  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 64 21.3 62 59.2 60 118.2 59 204.1 60  
 212.1 64

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 59.2 .02 204.1 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 59.2 204.1 56.4 82.7 111.4 .1 .3  
 Blocked Obstructions num= 2  
 Sta L Sta R Elev Sta L Sta R Elev  
 60 100 64 150 210 64

CROSS SECTION RIVER: Leucadia

REACH: 101 RS: 180

INPUT

Description:

Station Elevation Data			num= 9			Elev Sta Elev Sta Elev Sta					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	64	17	62	30.5	60	71.4	59	113.4	60		
120.7	64	192.2	64	257.1	63	317.6	64				

Manning's n Values			num= 3			Sta n Val Sta n Val Sta n Val		
Sta	n Val	Sta	n Val	Sta	n Val			
0	.02	30.5	.02	113.4	.02			

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	30.5	113.4		83.8	85.3		.1	.3

Blocked Obstructions			num= 2			Sta L Sta R Elev Sta L Sta R Elev		
Sta L	Sta R	Elev	Sta L	Sta R	Elev			
40	85	64	130	190	64			

CROSS SECTION RIVER: Leucadia  
REACH: 101 RS: 175

INPUT

Description:

Station Elevation Data			num= 11			Elev Sta Elev Sta Elev Sta					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	64	5.6	62	20.6	60	56.6	59	99.6	60		
104.6	62	172	63	232	62	252.5	61.9	268.5	62		
309.1	64										

Manning's n Values			num= 3			Sta n Val Sta n Val Sta n Val		
Sta	n Val	Sta	n Val	Sta	n Val			
0	.02	20.6	.02	99.6	.02			

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	20.6	99.6		120.2	124.8		.1	.3

Blocked Obstructions			num= 2			Sta L Sta R Elev Sta L Sta R Elev		
Sta L	Sta R	Elev	Sta L	Sta R	Elev			
20	55	64	110	160	64			

CROSS SECTION RIVER: Leucadia  
REACH: 101 RS: 170

INPUT

Description:

Station Elevation Data			num= 7			Elev Sta Elev Sta Elev Sta					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	64	33.4	62	87.4	60	141.8	58.5	184.7	60		
322	62	333.5	64								

Manning's n Values			num= 3			Sta n Val Sta n Val Sta n Val		
Sta	n Val	Sta	n Val	Sta	n Val			
0	.02	87.4	.02	184.7	.02			

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	87.4	184.7		137.5	137.6		.1	.3

CROSS SECTION RIVER: Leucadia  
REACH: 101 RS: 165

INPUT

Description:

Station Elevation Data			num= 16			Elev Sta Elev Sta Elev Sta					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	64	14.5	62	16	60	102.4	58	128.4	57		
138.5	56	147.5	56	172.9	55.9	200.4	56	225.9	58		
245.3	60	261.4	60.2	279.4	60	288.3	60	366.3	60		
374.3	64										

Manning's n Values			num= 3			Sta n Val Sta n Val Sta n Val		
Sta	n Val	Sta	n Val	Sta	n Val			
0	.02	138.5	.02	200.4	.02			

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	138.5	200.4		309.6	309.5		.1	.3

Blocked Obstructions			num= 2			Sta L Sta R Elev Sta L Sta R Elev		
Sta L	Sta R	Elev	Sta L	Sta R	Elev			

Sta L	Sta R	Elev	Sta L	Sta R	Elev
30	80	64	190	240	64

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 160

INPUT

Description:

Station Elevation Data	num=	19
Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev		
0 64 21 62 37 60 57.5 58 105 56		
129.5 55 142.1 55 152.6 55 186.5 54 214.5 55		
237 56 283.6 58 300.1 58.1 317 58 333 57.9		
342 58 359 60 368 62 376 64		

Manning's n Values	num=	3
Sta n Val Sta n Val Sta n Val		
0 .02 152.6 .02 214.5 .02		

Bank Sta: Left	Right	Lengths: Left	Channel	Right	Coeff	Contr.	Expan.
152.6	214.5	48.6	52.6	51.9	.1	.3	

Blocked Obstructions	num=	3
Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev		
30 70 64 90 120 64 150 170 64		

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 150

INPUT

Description:

Station Elevation Data	num=	15
Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev		
0 64 16 62 24 60 39.5 58 63.4 56		
96.4 54 132.3 54 144.8 53 156.9 52 193.8 54		
220.8 56 297.7 57.7 340.3 58 356.3 60 369.2 64		

Manning's n Values	num=	3
Sta n Val Sta n Val Sta n Val		
0 .02 144.8 .02 193.8 .02		

Bank Sta: Left	Right	Lengths: Left	Channel	Right	Coeff	Contr.	Expan.
144.8	193.8	151.2	154.7	157.7	.1	.3	

Blocked Obstructions	num=	2
Sta L Sta R Elev Sta L Sta R Elev		
20 50 64 190 220 64		

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 145

INPUT

Description:

Station Elevation Data	num=	14
Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev		
0 64 22.3 62 44.3 58 79.3 56 111.6 54		
143.9 52 156.1 52 176.6 52 182.1 58 246 58		
280.5 56.5 384.4 58 398.4 62 411.9 64		

Manning's n Values	num=	3
Sta n Val Sta n Val Sta n Val		
0 .02 143.9 .02 176.6 .02		

Bank Sta: Left	Right	Lengths: Left	Channel	Right	Coeff	Contr.	Expan.
143.9	176.6	175.6	160.5	160.3	.1	.3	

Blocked Obstructions	num=	3
Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev		
40 85 64 115 150 64 180 240 64		

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 140

INPUT

Description:

Station Elevation Data	num=	22
Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev		
0 64 12.5 62 39 60 45.5 56 88 54		
162.6 52 178.6 54 184.6 58 237.6 58 283.1 56.2		

311.6	56.4	375.5	58	392.5	60	400.6	62	422.6	62
432	63	434	63	442	61	465	64	531	66
566	68	730	70						

Manning's n Values num= 3  
 Sta n Val Sta n Val  
 0 .02 88 .02 178.6 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 88 178.6 141.5 123.2 117.1 .1 .3

Blocked Obstructions num= 4  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 60 140 64 200 260 64 539 646 70  
 710 730 70

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 135

INPUT

Description:  
 Station Elevation Data num= 14  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 64 18.7 62 47.7 60 71.8 58 99.9 56  
 152.2 54 165.3 54 181.2 54 234.9 54 309.4 56  
 380.6 58 399.2 60 408.7 62 456.1 64

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 152.2 .02 234.9 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 152.2 234.9 122.2 126.9 132.7 .1 .3

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 130

INPUT

Description:  
 Station Elevation Data num= 14  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 64 14.5 62 28 60 34.5 56 131.4 54  
 154.3 54 268.8 56 365.1 58 370 62 392 62  
 445 64 472 66 492 68 555 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 131.4 .02 154.3 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 131.4 154.3 197.5 197.3 196.3 .1 .3

Blocked Obstructions num= 4  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 0 10 64 40 75 64 90 130 64  
 160 240 64

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 125

INPUT

Description:  
 Station Elevation Data num= 14  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 64 21.6 62 34.6 54 52.6 54 139.7 54  
 149.2 54 157.7 54 240.8 54 314.2 56 366.8 58  
 378.8 60 392.8 62 424.8 62 454.4 64

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 139.7 .02 157.7 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 139.7 157.7 131.2 129.8 132.3 .1 .3

Blocked Obstructions num= 4  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 0 20 64 30 75 64 100 130 64  
 190 240 64

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 120

INPUT

Description:

Station Elevation Data num= 17

Sta	Elev								
0	64	31.6	62	46	60	49.1	58	62.2	56
149.5	54.2	160.5	54.1	171.6	54	202.1	54	299.9	56
317.9	56.3	341.4	56	369.5	58	389.6	60	406.1	62
429.6	62	464.8	64						

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.02	149.5	.02	202.1	.02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 149.5 202.1 86.1 88.2 95.5 .1 .3

Blocked Obstructions num= 3

Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta L	Sta R	Elev
0	40	64	80	140	64	180	250	64

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 115

INPUT

Description:

Station Elevation Data num= 25

Sta	Elev								
0	64	26.5	62	48	56	117	54	138	54
149.5	54	158.5	54	314.9	56	333.9	56	358.8	58
377.9	60	390	61	392	61	395	60	400	62
425	62	465	64	495	66	520	68	610	72
640	72	710	70	785	68	855	68	935	70

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.02	138	.02	158.5	.02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 138 158.5 218.8 211.7 222.6 .1 .3

Blocked Obstructions num= 3

Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta L	Sta R	Elev
60	140	64	180	250	64	503	899	72

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 110

INPUT

Description:

Station Elevation Data num= 10

Sta	Elev								
0	62	5.5	54	53.5	54	74.5	54	150.5	54
271.9	56	290.9	58	299.4	60	340.9	60	365.4	62

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.02	5.5	.02	150.5	.02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 5.5 150.5 180.1 165.1 173.7 .1 .3

Blocked Obstructions num= 2

Sta L	Sta R	Elev	Sta L	Sta R	Elev
10	40	62	90	160	62

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 105

INPUT

Description:

Station Elevation Data num= 12

Sta	Elev								
0	62	7.6	60	23.8	58	51.8	56	80.4	54
89.2	54	100.1	54	285.3	56	309.6	58	316.9	60
359.4	60	387	62						

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 80.4 .02 100.1 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 80.4 100.1 106.7 119.5 229.1 .1 .3

Blocked Obstructions num= 1  
 Sta L Sta R Elev  
 100 170 62

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 100

INPUT

Description:

Station Elevation Data num= 20  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 62 26.6 60 81.5 58 86.5 56 185 55  
 273.2 56 314.6 58 319.3 60 330 60 332 60  
 336 59 345 59 385 62 425 64 460 66  
 512 68 560 68 710 66 798 66 1000 68

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 86.5 .02 273.2 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 86.5 273.2 360 340 360 .1 .3

Blocked Obstructions num= 3  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 150 190 62 436 624 68 676 870 68

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 95

INPUT

Description:

Station Elevation Data num= 24  
 Sta Elev  
 0 58 52 56 118 56 122 56 230 54.46  
 257.9 54.16 266.8 54.16 301.1 55.56 329.4 56.16 341.1 57.16  
 350.3 58.16 371 59.2 378 58.5 385 60 395 62  
 434 64 460 66 485 68 580 70 655 70  
 760 68 820 67 940 68 1000 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 230 .02 301.1 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 230 301.1 365.1 364.9 363 .1 .3

Blocked Obstructions num= 4  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 14 30 58 42 60 58 70 80 58  
 172 190 58

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 90

INPUT

Description:

Station Elevation Data num= 27  
 Sta Elev  
 0 58 35 56 86 54 142 53.76 206.7 53.76  
 231.7 54.16 245.3 54.56 265.7 54.16 288.9 54.16 296.9 55.16  
 299.9 56.16 304.4 57.16 307.3 58.16 335 58.2 337 58.2  
 340 58 345 56.5 351 56.5 365 60 404 62  
 440 68 520 70 645 70 650 68 800 66.5  
 920 68 980 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 142 .02 206.7 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.

142 206.7 356.3 355.5 353.7 .1 .3  
 Blocked Obstructions num= 3  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 55 86 58 105 142 58 442 625 70

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 85

INPUT

Description:  
 Station Elevation Data num= 20  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 58 20 56 42 54 113 53.06 144.1 52.86  
 158.7 53.06 199.9 53.16 206.4 52.16 217.1 52.16 220.7 53.16  
 231.8 54.16 260 58.2 265 58 273 56 285 58  
 320 60 340 62 355 64 390 66 525 68

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 199.9 .02 220.7 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 199.9 220.7 353.7 357.5 356.9 .1 .3

Blocked Obstructions num= 2  
 Sta L Sta R Elev Sta L Sta R Elev  
 48 100 58 484 525 68

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 80

INPUT

Description:  
 Station Elevation Data num= 19  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 58 30 56 90 54 153 53.26 172.5 53.16  
 223.6 54.06 244.7 53.16 250.2 52.16 256.8 51.56 263.6 52.16  
 273.1 53.16 295 58 308 56 319 54 326 56  
 350 58 380 60 450 64 715 68

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 244.7 .02 273.1 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 244.7 273.1 357.5 355.1 356.2 .1 .3

Blocked Obstructions num= 2  
 Sta L Sta R Elev Sta L Sta R Elev  
 85 140 58 409 715 68

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 75

INPUT

Description:  
 Station Elevation Data num= 16  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 58 80 56 115 54.66 173.4 54.16 189.9 54.56  
 203.6 54.16 234 54.16 270 58 272 58 285 56  
 290 56 300 58 355 60 435 64 505 68  
 590 68

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 115 .02 234 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 115 234 488 485 489 .1 .3

Blocked Obstructions num= 2  
 Sta L Sta R Elev Sta L Sta R Elev  
 40 80 58 361 590 68

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 70

INPUT

Description:

Station Elevation Data num= 17

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	58	48	56	190	54.56	203	54.16	257	55.06
301.9	55.06	308.1	55.16	312.8	56.16	324.7	58.76	330	59
332	59	354	58	360	60	411	62	435	64
480	66	565	68						

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.02	190	.02	257	.02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.

190	257	360	359.8	358.2	.1	.3
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Blocked Obstructions num= 2

Sta L	Sta R	Elev	Sta L	Sta R	Elev
160	190	58	428	548	68

CROSS SECTION RIVER: Leucadia  
REACH: Combine RS: 65

INPUT

Description:

Station Elevation Data num= 17

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	58	30	56	33	54	125	54	215	53.76
258.9	54.16	306	55.16	311.1	56.16	331.9	57.56	355	58.7
357	58.7	370	58	376	58	382	60	418	62
465	64	472	64						

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.02	125	.02	258.9	.02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.

125	258.9	384.7	386.9	384.1	.1	.3
-----	-------	-------	-------	-------	----	----

CROSS SECTION RIVER: Leucadia  
REACH: Combine RS: 60

INPUT

Description:

Station Elevation Data num= 18

Sta	Elev								
0	58	10	56	200.3	54.06	247.7	53.76	262.1	55.16
273.3	55.26	304.3	55.16	322.1	56.16	342.1	58.86	345	59
347	59	360	58	362	56	368	58	376	60
440	62	470	64	505	66				

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.02	200.3	.02	262.1	.02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.

200.3	262.1	364.2	363.7	367	.1	.3
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Blocked Obstructions num= 3

Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta L	Sta R	Elev
17	40	58	58	110	58	136	200	58

CROSS SECTION RIVER: Leucadia  
REACH: Combine RS: 55

INPUT

Description:

Station Elevation Data num= 19

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	58	40	56	118	54	173	54	185	53.46
201.7	52.56	215.5	53.16	236.6	54.06	257.9	54.26	313	55.16
328.4	58.86	330	59	332	59	343	58	350	56.5
356	58	365	60	435	62	535	64		

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.02	185	.02	215.5	.02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.

185	215.5	354.4	358.2	348.8	.1	.3
-----	-------	-------	-------	-------	----	----

Blocked Obstructions num= 4  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 13 34 58 50 80 58 140 185 58  
 444 535 64

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 50

INPUT

Description:  
 Station Elevation Data num= 24  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 73.76 3000031 63.76 15.60001 62.16 21.90001 54.16 32.20001 53.46  
 42.3 53.56 71.2 54.16 83.50001 55.16 98.8 55.16 132 55.16  
 149.9 56.16 153.5 57.16 161.6 58.56 170 58.7 172 58.7  
 180 58 190 56 194 58 201 60 212 62  
 220 60 265 62 275 64 342 66

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 21.90001 .02 71.2 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 21.90001 71.2 393.5 397.9 398.7 .1 .3

Blocked Obstructions num= 1  
 Sta L Sta R Elev  
 282 342 66

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 45

INPUT

Description:  
 Station Elevation Data num= 18  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 55.06 14.40001 54.36 25.2 54.16 45.21 54.22 62.73 54.2  
 112.5 52.01 126.52 52.01 135 56 154 57 156 57  
 167 56 179 55 185 55 233 56 252 58  
 380 60 384 62 434 64

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 112.5 .02 126.52 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 112.5 126.52 375 380 385 .1 .3

Blocked Obstructions num= 1  
 Sta L Sta R Elev  
 281 385 64

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 40

INPUT

Description:  
 Station Elevation Data num= 23  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 55.86 5.8 55.16 23.5 55.16 45.2 56.16 53.5 56.26  
 71.9 56.36 81.2 56.16 94.6 56.06 106.1 56.16 112.85 56.16  
 116.5 56.16 121 55.16 126 54.16 129.8 53.16 133 53.06  
 134 54 146 54 152 52.5 157 56 190 56  
 260 56 380 58 400 60

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 121 .02 157 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 121 157 343.5 344.8 345.4 .1 .3

Blocked Obstructions num= 1  
 Sta L Sta R Elev  
 236 348 60

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 35

INPUT

Description:

Station Elevation Data		num= 17		Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	55.66	14.7	55.16	22.1	55.16	48.8	56.16	56.3	56.16		
113	56	120	54	125	52	135	50	150	50		
155	48.5	164	52	166	56	195	56	238	56		
324	58	447	60								

Manning's n Values		num= 3		Sta	n Val	Sta	n Val	Sta	n Val
0	.02	125	.02	164	.02				

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	125	164		345.5	336.8		.1	.3

Blocked Obstructions		num= 1		Sta L	Sta R	Elev
				232	447	60

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 30

INPUT

Description:

Station Elevation Data		num= 18		Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	58.16	36.8	58.1651.59999	59.1657.59999	59.16	81.3	59.16	81.3	59.16		
94.39999	59.16	104.2	58.16	111	58	125	54	134	50		
140	46	155	46	163	46	176	54	191	56		
319	56	400	58	470	60						

Manning's n Values		num= 3		Sta	n Val	Sta	n Val
0	.02	140	.02	163	.02		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	140	163		0	0		.1	.3

SUMMARY OF MANNING'S N VALUES

River:Leucadia

Reach	River Sta.	n1	n2	n3
Vulcan	3300.14	.03	.035	.03
Vulcan	3200.15	.03	.035	.03
Vulcan	3100.16	.03	.035	.03
Vulcan	3000.17	.03	.035	.03
Vulcan	2900.18	.03	.035	.03
Vulcan	2800.19	.03	.035	.03
Vulcan	2700.20	.03	.035	.03
Vulcan	2600.21	.03	.035	.03
Vulcan	2500.22	.03	.035	.03
Vulcan	2400.23	.03	.035	.03
Vulcan	2300.24	.03	.035	.03
Vulcan	2200.25	.03	.035	.03
Vulcan	2100.26	.03	.035	.03
Vulcan	245	.03	.035	.03
Vulcan	240	.03	.035	.03
Vulcan	235	.03	.035	.03
Vulcan	230	.02	.02	.02
Vulcan	225	.02	.02	.02
Vulcan	220	.02	.02	.02
Vulcan	215	.02	.02	.02
Vulcan	195	.02	.02	.02
Vulcan	175	.02	.02	.02
Vulcan	165	.02	.02	.02
Vulcan	150	.02	.02	.02
101	230	.02	.02	.02
101	225.3	.02	.02	.02
101	225.2	.02	.02	.02
101	225.1	.02	.02	.02
101	220	.02	.02	.02
101	215	.02	.02	.02

101	210	.02	.02	.02
101	205	.02	.02	.02
101	195	.02	.02	.02
101	190	.02	.02	.02
101	185	.02	.02	.02
101	180	.02	.02	.02
101	175	.02	.02	.02
101	170	.02	.02	.02
101	165	.02	.02	.02
101	160	.02	.02	.02
101	150	.02	.02	.02
101	145	.02	.02	.02
Combine	140	.02	.02	.02
Combine	135	.02	.02	.02
Combine	130	.02	.02	.02
Combine	125	.02	.02	.02
Combine	120	.02	.02	.02
Combine	115	.02	.02	.02
Combine	110	.02	.02	.02
Combine	105	.02	.02	.02
Combine	100	.02	.02	.02
Combine	95	.02	.02	.02
Combine	90	.02	.02	.02
Combine	85	.02	.02	.02
Combine	80	.02	.02	.02
Combine	75	.02	.02	.02
Combine	70	.02	.02	.02
Combine	65	.02	.02	.02
Combine	60	.02	.02	.02
Combine	55	.02	.02	.02
Combine	50	.02	.02	.02
Combine	45	.02	.02	.02
Combine	40	.02	.02	.02
Combine	35	.02	.02	.02
Combine	30	.02	.02	.02

SUMMARY OF REACH LENGTHS

River: Leucadia

Reach	River Sta.	Left	Channel	Right
Vulcan	3300.14	100	100	100
Vulcan	3200.15	100	100	100
Vulcan	3100.16	100	100	100
Vulcan	3000.17	100	100	100
Vulcan	2900.18	100	100	100
Vulcan	2800.19	100	100	100
Vulcan	2700.20	100	100	100
Vulcan	2600.21	100	100	100
Vulcan	2500.22	100	100	100
Vulcan	2400.23	100	100	100
Vulcan	2300.24	100	100	100
Vulcan	2200.25	100	100	100
Vulcan	2100.26	15	15	15
Vulcan	245	175	175	175
Vulcan	240	275	275	275
Vulcan	235	120	120	120
Vulcan	230	175	180	185
Vulcan	225	190	185	185
Vulcan	220	175	175	175
Vulcan	215	290	290	290
Vulcan	195	340	340	340
Vulcan	175	225	220	220
Vulcan	165	360	360	360
Vulcan	150	305	305	305
101	230	104.1	100.2	136.3
101	225.3	5	5	5
101	225.2	5	5	5
101	225.1	134.2	131.9	133.3
101	220	222.7	215.1	206.1
101	215	78.2	80.6	89.6
101	210	47.1	45.4	64.5

101	205	141.2	142.6	152.6
101	195	143.6	102.4	81.7
101	190	109.2	93.8	106
101	185	56.4	82.7	111.4
101	180	83.8	85.3	85.6
101	175	120.2	124.8	122.1
101	170	137.5	137.6	138.7
101	165	309.6	309.5	308.6
101	160	48.6	52.6	51.9
101	150	151.2	154.7	157.7
101	145	175.6	160.5	160.3
Combine	140	141.5	123.2	117.1
Combine	135	122.2	126.9	132.7
Combine	130	197.5	197.3	196.3
Combine	125	131.2	129.8	132.3
Combine	120	86.1	88.2	95.5
Combine	115	218.8	211.7	222.6
Combine	110	180.1	165.1	173.7
Combine	105	106.7	119.5	229.1
Combine	100	360	340	360
Combine	95	365.1	364.9	363
Combine	90	356.3	355.5	353.7
Combine	85	353.7	357.5	356.9
Combine	80	357.5	355.1	356.2
Combine	75	488	485	489
Combine	70	360	359.8	358.2
Combine	65	384.7	386.9	384.1
Combine	60	364.2	363.7	367
Combine	55	354.4	358.2	348.8
Combine	50	393.5	397.9	398.7
Combine	45	375	380	385
Combine	40	343.5	344.8	345.4
Combine	35	345.5	336.8	337.3
Combine	30	0	0	0

SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS  
River: Leucadia

Reach	River Sta.	Contr.	Expan.
Vulcan	3300.14	.1	.3
Vulcan	3200.15	.1	.3
Vulcan	3100.16	.1	.3
Vulcan	3000.17	.1	.3
Vulcan	2900.18	.1	.3
Vulcan	2800.19	.1	.3
Vulcan	2700.20	.1	.3
Vulcan	2600.21	.1	.3
Vulcan	2500.22	.1	.3
Vulcan	2400.23	.1	.3
Vulcan	2300.24	.1	.3
Vulcan	2200.25	.1	.3
Vulcan	2100.26	.1	.3
Vulcan	245	.1	.3
Vulcan	240	.1	.3
Vulcan	235	.1	.3
Vulcan	230	.1	.3
Vulcan	225	.1	.3
Vulcan	220	.1	.3
Vulcan	215	.1	.3
Vulcan	195	.1	.3
Vulcan	175	.1	.3
Vulcan	165	.1	.3
Vulcan	150	.1	.3
101	230	.1	.3
101	225.3	.1	.3
101	225.2	.1	.3
101	225.1	.1	.3
101	220	.1	.3
101	215	.1	.3
101	210	.1	.3
101	205	.1	.3

101	195	.1	.3
101	190	.1	.3
101	185	.1	.3
101	180	.1	.3
101	175	.1	.3
101	170	.1	.3
101	165	.1	.3
101	160	.1	.3
101	150	.1	.3
101	145	.1	.3
Combine	140	.1	.3
Combine	135	.1	.3
Combine	130	.1	.3
Combine	125	.1	.3
Combine	120	.1	.3
Combine	115	.1	.3
Combine	110	.1	.3
Combine	105	.1	.3
Combine	100	.1	.3
Combine	95	.1	.3
Combine	90	.1	.3
Combine	85	.1	.3
Combine	80	.1	.3
Combine	75	.1	.3
Combine	70	.1	.3
Combine	65	.1	.3
Combine	60	.1	.3
Combine	55	.1	.3
Combine	50	.1	.3
Combine	45	.1	.3
Combine	40	.1	.3
Combine	35	.1	.3
Combine	30	.1	.3

**ATTACHMENT 3**

**ALTERNATIVE 5**

**10-YEAR AND 100-YEAR**

**HEC-1 ANALYSES**

**ALTERNATIVE 5**  
**10-YEAR HEC-1 ANALYSIS**

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*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*      JUN 1998                *
*      VERSION 4.1             *
*
* RUN DATE 18AUG04 TIME 07:38:46 *
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

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X   X  XXXXXXXX  XXXXX      X
X   X X          X   X      XX
X   X X          X          X
XXXXXXX XXXX    X          XXXXX X
X   X X          X          X
X   X X          X   X      X
X   X  XXXXXXXX  XXXXX      XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

ENCINITAS 14413  
 10-YR ALT 5  
 10A5.hcl

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

\*DIAGRAM

1 ID \*\*\*\*\*

2 ID ENCINITAS COAST HWY 101 J-14413 8-17-04

3 ID ALTERNATIVE 5 - COMBO ALT 1 + ALT 2C

4 ID 10-YR GRADE NORTHBOUND LANES OF HWY 101

5 ID FROM APPROXIMATELY JUPITER TO MOOREGATE

6 ID AT A CONSTANT SLOPE OF 0.1%

7 ID BASINS 9B, 10,AND 11 ARE UNDETAINED AND ROUTED VIA TRAP

8 ID CHANNEL. ALL BASINS U/S ARE DETAINED.

9 ID FN: 10A5.HC1

10 ID \*\*\*\*\*

11 ID ENCINITAS COAST HWY 101 J-14413 5-25-04

12 ID ALTERNATIVE 2 OPTION C - 10-YR GRADE NORTHBOUND LANES OF

13 ID HWY 101 FROM APPROXIMATELY JUPITER TO MOOREGATE

14 ID AT A CONSTANT SLOPE OF 0.1%

15 ID BASINS 9B, 10,AND 11 ARE UNDETAINED AND ROUTED VIA TRAP

16 ID CHANNEL. ALL BASINS U/S ARE DETAINED.

17 ID FN: 10A2C.HC1

18 ID \*\*\*\*\*

19 ID ENCINITAS COAST HWY 101 J-14413 3-19-04

20 ID INCLUDES DIVERSION INTO STORM DRAIN BASED ON ORIFICE PLATE

21 ID Qs

22 ID FN: 10DET5R.HC1

23 ID \*\*\*\*\*

24 ID ENCINITAS COAST HWY 101 J-14413 01/12/04

25 ID SAME AS BELOW EXCEPT CHANGED SV,SQ,SE CARDS BASED ON

26 ID HEC-RAS FN: 101.PRJ (PLAN 12)

27 ID INCLUDES ROUTING THROUGH ALLEY AT UPSTREAM OF END OF STUDY

28 ID FN: 10DET5.HC1

29 ID \*\*\*\*\*

30 ID ENCINITAS COAST HWY 101 J-14413 01/05/04

31 ID SAME AS BELOW EXCEPT 10-YEAR (CN CHANGED FOR PZN=1.5),

32 ID RATING CURVE SV,SQ,SE CARDS CHANGED BASED ON HEC-RAS FN:

33 ID 101.PRJ (PLAN 101 R7)

34 ID BASIN AREAS FOR 7-11 CHANGED BACK TO ORINGAL (2,5,10-YR)

35 ID SIZE THAT DOES NOT INCLUDE AREA EAST OF THE RR TRACKS;

36 ID LAG CHANGED BACK TO ORIGINAL, CN CHANGED BACK TO ORIGINAL

37 ID BASED ON HEC-1 FN:PRO5R1.HC1

38 ID FN: 10DET3.HC1

39 ID \*\*\*\*\*

40 ID ENCINITAS COAST HWY 101 J-14413 12/31/03

41 ID SAME AS BELOW EXCEPT MOVED LOCATION OF CONFLUENCE BTWN

42 ID EAST SIDE OF RR TRACKS (BASINS 1A,1,1B,2,&6) TO BASIN 4,

43 ID WHICH WAS ORIGINALLY MODELED AT BASIN 7 (LEUCADIA)

44 ID FN: 100DET3.HC1

45 ID \*\*\*\*\*

46 ID ENCINITAS COAST HWY 101 J-14413 12/29/03

47 ID 100-YEAR RUN WITH BASIN AREAS EXTENDED TO THE RIDGE EAST OF

48 ID THE RR TRACKS. PI CARDS CHANGED FOR 100-YR BASED ON FN: E100.HC1

49 ID LAG AND CURVE NUMBERS CHANGED FOR 100-YEAR.

50 ID FN:100DET.HC1

51 ID BASIN AREAS ALSO CHANGED FOR 7 THROUGH 11. STORAGE RATING

52 ID CURVES BASED ON HEC-RAS OUTPUT FN: 101.PRJ (PLAN 101 R3)

53 ID \*\*\*\*\*

54 ID ENCINITAS COAST HWY 101

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

55      ID    J-14413
56      ID    SEPT 25, 2003
57      ID    MODIFIED EXISTING RUN TO MODEL PROPOSED DETENTION OF BASINS
58      ID    1A, 1B, 1, 2, 3, 4, 5, 6, AND 8
59      ID    DETENTION CARDS SA/SV, SQ, SE OBTAINED FROM FN: DSI_5R.HC1
60      ID    *****
61      ID    ENCINITAS- COAST HIGHWAY 101
62      ID    JOB # 14413
63      ID    09-12-03
64      ID    MODIFIED PUMP Q TO 1.7 CFS, AND ROUTING OF BASINS 9A, 9B, AND 9
65      ID    FROM PUMP STATION THROUGH 10" LATERAL, CONFLUENCING
66      ID    WITH MAIN LINE AT AT CONNECTION 3 INSTEAD OF CONNECTION 2
67      ID    ALSO CHANGED ROUTING THROUGH MAIN LINE FROM LINE G TO CONNECTION
68      ID    2, TO LINE G TO CONNECTION 3
69      ID    *****
70      ID    ENCINITAS- COAST HIGHWAY 101
71      ID    JOB # 14413
72      ID    09-04-03
73      ID    MODIFIED CURVE NUMBER AND REMOVED % IMPERVIOUS
74      ID    *****
75      ID    ENCINITAS- COAST HIGHWAY 101
76      ID    JOB # 14413
77      ID    06-03-03
78      ID    POST-IMPROVEMENT (EXISTING) CONDITION          FN: 101EX_5.HC1
79      ID    5-YEAR, 24-HR STORM EVENT
80      ID    LAG CALCULATION ARE BASED OFF OF NRCS METHOD
81      ID    AND ARE A FUNCTION OF RUNOFF COEF. AND VELOCITY
82      ID    NESTED STORM PER COUNTY OF SAN DIEGO HYDROLOGY MANUAL
83      ID    COPYRIGHT 2003 RICK ENGINEERING COMPANY
84      ID    6HR RAINFALL IS 1.6 INCHES
85      ID    24HR RAINFALL IS 2.5 INCHES
86      ID    TOTAL BASIN AREA IS .5 SQUARE MILES

*** FREE ***
87      IT      5 01JAN90 1200 300
88      IO      5

89      KK      1A
90      KO      0      0      0      0      21
91      KM      NESTED STORM PER COUNTY OF SAN DIEGO HYDROLOGY MANUAL
92      KM      COPYRIGHT 2003 RICK ENGINEERING COMPANY
93      KM      THE FOLLOWING IT CARD MUST BE USED IN YOUR DATA SET
94      KM      IT 5 01JAN90 1200 300
95      KM      6HR RAINFALL IS 1.8 INCHES
96      KM      24HR RAINFALL IS 3 INCHES
97      KM      DAR30 = .9942
98      KM      DAR60 = .997
99      KM      DAR180 = .998
100     KM      DAR360 = .9985
101     KM      DAR1440 = .999
102     KM      BASIN AREA IS .5 SQUARE MILES
103     KM      ***10-YR PRECIP. DATA*****
104     IN      5 01JAN90 1200 300
105     PI      .00384 .00385 .00386 .00388 .00389 .0039 .00391 .00393 .00394 .00396
106     PI      .00397 .00399 .004 .00401 .00402 .00404 .00405 .00407 .00408 .0041
107     PI      .00411 .00413 .00414 .00416 .00418 .0042 .00421 .00423 .00424 .00426
    
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LINE	ID	1	2	3	4	5	6	7	8	9	10
108	PI	.00427	.0043	.00431	.00433	.00434	.00437	.00438	.0044	.00441	.00444
109	PI	.00445	.00448	.00449	.00451	.00453	.00455	.00457	.00459	.00461	.0046
110	PI	.00465	.00468	.00469	.00472	.00473	.00476	.00478	.00481	.00482	.0048
111	PI	.00487	.0049	.00492	.00495	.00497	.005	.00502	.00505	.00507	.0051
112	PI	.00512	.00516	.00517	.00521	.00523	.00527	.00529	.00533	.00535	.0053
113	PI	.00541	.00545	.00547	.00551	.00553	.00558	.0056	.00565	.00567	.00572
114	PI	.00574	.00579	.00581	.00586	.00589	.00594	.00597	.00602	.00605	.0061
115	PI	.00613	.00619	.00622	.00628	.00631	.00637	.0064	.00647	.0065	.00657
116	PI	.0066	.00667	.0067	.00678	.00681	.00689	.00693	.00701	.00705	.00713
117	PI	.00717	.00726	.0073	.00739	.00744	.00754	.00759	.00769	.00774	.00784
118	PI	.0079	.00801	.00806	.00818	.00824	.00837	.00843	.00856	.00863	.00877
119	PI	.00884	.00899	.00907	.00895	.00903	.00919	.00928	.00946	.00956	.0097
120	PI	.00985	.01006	.01017	.0104	.01052	.01078	.01091	.01118	.01133	.01163
121	PI	.01179	.01213	.01231	.01269	.01289	.01331	.01354	.01406	.01432	.0148
122	PI	.01518	.01583	.01619	.01696	.01738	.01832	.01884	.01999	.02065	.0221
123	PI	.02299	.02498	.02615	.02939	.03111	.03554	.03846	.04652	.05299	.0778
124	PI	.10962	.39292	.0624	.04212	.03313	.02748	.02393	.02136	.01939	.01783
125	PI	.01656	.0155	.0146	.01378	.01309	.01249	.01196	.01148	.01104	.01065
126	PI	.01029	.00996	.00965	.00937	.00911	.00915	.00892	.0087	.0085	.0083
127	PI	.00812	.00795	.00779	.00763	.00749	.00735	.00722	.00709	.00697	.0068
128	PI	.00674	.00663	.00653	.00643	.00634	.00625	.00616	.00607	.00599	.0059
129	PI	.00584	.00576	.00569	.00562	.00556	.00549	.00543	.00537	.00531	.0052
130	PI	.00519	.00514	.00508	.00503	.00498	.00493	.00488	.00484	.00479	.0047
131	PI	.0047	.00466	.00462	.00458	.00454	.0045	.00446	.00443	.00439	.00435
132	PI	.00432	.00428	.00425	.00422	.00419	.00415	.00412	.00409	.00406	.0040
133	PI	.00401	.00398	.00395	.00392	.0039	.00387	.00384	0	0	0
134	PI	0	0	0	0	0	0	0	0	0	0
135	PI	0	0								
136	BA	0.01									
137	LS	0	60								
138	UD	0.139									
139	KK	RT1A									
140	KM	ROUTE RUNOFF FROM BASIN 1A THROUGH BASIN 1 (ALONG HW 101)									
141	RS	3	STOR	-1							
142	RC	0.02	0.02	0.02	3225	0.0068					
143	RX	0	5	10	15	20	25	30	35		
144	RY	2	2	1.5	1	1	1.5	2	2		
145	KK	1B									
146	BA	0.03									
147	LS	0	65								
148	UD	0.163									
149	KK	RT1B									
150	KM	ROUTE RUNOFF FROM BASIN 1B THROUGH BASIN 1 (ALONG ORPHEUS ST.)									
151	RS	1	STOR	-1							
152	RC	0.02	0.02	0.02	1125						
153	RX	0	5	10	15	20	25	30	35		
154	RY	2	2	1.5	1	1	1.5	2	2		

LINE	ID	1	2	3	4	5	6	7	8	9	10
155	KK	RT1B									
156	KM	ROUTE RUNOFF FROM BASIN 1B THROUGH BASIN 1 (ALONG HW 101)									
157	RS	1	STOR	-1							
158	RC	0.02	0.02	0.02	1250						
159	RX	0	5	10	15	20	25	30	35		
160	RY	2	2	1.5	1	1	1.5	2	2		
161	KK	B1									
162	BA	0.09									
163	LS	0	61								
164	UD	0.282									
165	KK	Q@1									
166	KM	COMBINE BASINS 1A, 1B AND BASIN 1									
167	HC	3									
168	KKQ1_in101										
169	KM	10-YEAR FLOW IN HYW 101 WITH 10-YR FLOWS DIVERTED TO STORM DRAIN									
170	DT	10YR_SD									
171	DI	0	15	70							
172	DQ	0	15	15							
173	KK	DET_11A,1B									
174	KM	DETAIN RUNOFF FROM BASIN 1, 1B AND 1A									
175	RS	1	STOR	-1							
176	SV	2.01	3.34	4.01	5.84	9.54	11.85				
177	SQ	1	50	100	250	500	750				
178	SE	68.47	69.39	69.85	70.76	71.75	72.27				
179	KK	B2									
180	BA	0.06									
181	LS	0	67								
182	UD	0.145									
183	KK	Q@2									
184	KM	COMBINE BASIN 1A, 1B AND BASIN 1 WITH BASIN 2									
185	HC	2									
186	KKQ2_in101										
187	KM	10-YEAR FLOW IN HYW 101 WITH 10-YR FLOWS DIVERTED TO STORM DRAIN									
188	DT	10YR_SD									
189	DI	0	19	130							
190	DQ	0	19	19							
191	KK	DET_2									
192	KM	DETAIN BASINS 1A, 1 AND 2									
193	RS	1	STOR	-1							
194	SV	2.17	4.58	5.69	7.93	10.6	13.16				
195	SQ	1	50	100	250	500	750				
196	SE	66.73	67.37	67.63	68.09	68.54	68.92				



LINE	ID	1	2	3	4	5	6	7	8	9	10
240	KKQ4_in101										
241	KM	10-YEAR FLOW IN HYW 101 WITH 10-YR FLOWS DIVERTED TO STORM DRAIN									
242	DT	10YR_SD									
243	DI	0	7	160							
244	DQ	0	7	7							
245	KK	DET4									
246	KM	DETAIN BASIN 4									
247	KO	0	0	0	0	21					
248	RS	1	STOR	-1							
249	SV	4.98	6.46	6.98	7.34	7.62	7.88				
250	SQ	0.1	20	40	60	80	100				
251	SE	59.14	59.75	59.95	60.09	60.20	60.29				
252	KK	B5									
253	BA	0.02									
254	LS	0	68								
255	UD	0.084									
256	KK	Q@5									
257	KM	COMBINE 3,4,&5									
258	HC	2									
259	KKQ5_in101										
260	KM	10-YEAR FLOW IN HYW 101 WITH 10-YR FLOWS DIVERTED TO STORM DRAIN									
261	DT	10YR_SD									
262	DI	0	9	190							
263	DQ	0	9	9							
264	KK	DET5									
265	KM	DETAIN BASIN 5									
266	KO	0	0	0	0	21					
267	RS	1	STOR	-1							
268	SV	2.31	3.34	3.78	4.14	4.47	4.8				
269	SQ	0.1	20	40	60	80	100				
270	SE	57.52	57.97	58.13	58.24	58.34	58.43				
271	KK	B7									
272	KM	BASIN 7									
273	BA	0.02									
274	LS	0	66								
275	UD	0.129									
276	KK	5+7									
277	KM	COMBINE BASINS 5 WITH 7									
278	HC	2									
		* HC 3									
279	KKQ7_in101										
280	KM	10-YEAR FLOW IN HYW 101 WITH 10-YR FLOWS DIVERTED TO STORM DRAIN									
281	DT	10YR_SD									
282	DI	0	6	250							
283	DQ	0	6	6							

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
284	KK Q@7
285	KM COMBINE 3,4,5,7 AND 1,2,6 (EAST OF TRACKS)
286	HC 2
	* KK COMBINE
	* KM DIVERT 1 CFS TO LINE E STORM DRAIN
	* DT DIVE 0 1
	* DI 0 1 200
	* DQ 0 1 1
287	KK DET7
288	KM DETAIN AT BASIN 7
289	KO 0 0 0 0 21
290	RS 1 STOR -1
291	SV 2.2 3.16 3.57 3.9 4.29 4.69
292	SQ 0.1 20 40 60 80 100
293	SE 55.05 55.40 55.54 55.64 55.76 55.88
294	KK B8
295	BA 0.01
296	LS 0 71
297	UD 0.128
298	KK Q@8
299	KM COMBINE BASINS 1A,1,1B,2,6,3,4,5,&7 WITH BASIN 8
300	HC 2
	* KM DIVERT 1 CFS TO LINE G OF STORM DRAIN
	* DT DIVG 0 1
	* DI 0 1 200
	* DQ 0 1 1
301	KK DET8
302	KM DETAIN BASIN 8
303	KO 0 0 0 0 21
304	RS 1 STOR -1
305	SV 1.4 2.14 2.46 2.71 3.03 3.38
306	SQ 0.1 20 40 60 80 100
307	SE 55.05 55.40 55.53 55.63 55.75 55.87
308	KK B9A
309	BA 0.02
310	LS 0 69
311	UD 0.120
312	KK Q@9A
313	KM COMBINE BASINS 1A,1,1B,2,6,3,4,5,7,&8 WITH BASIN 9A
314	HC 2
315	KK DET9A
316	KM DETAIN AT BASIN 9A
317	KO 0 0 0 0 21
318	RS 1 STOR -1
319	SV .95 2.17 2.72 3.22 3.64 4.11
320	SQ 0.1 20 40 60 80 100
321	SE 54.51 54.99 55.18 55.35 55.50 55.66





SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT

LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
89	1A	
	V	
	V	
139	RT1A	
	.	
	.	
145	.	1B
	.	V
	.	V
149	.	RT1B
	.	V
	.	V
155	.	RT1B
	.	.
	.	.
161	.	B1
	.	.
	.	.
165	Q@1.....	
	.	
	.	
170	.	-----> 10YR_SD
168	Q1_in101	
	V	
	V	
173	DET_1	
	.	
	.	
179	.	B2
	.	.
	.	.
183	Q@2.....	
	.	
	.	
188	.	-----> 10YR_SD
186	Q2_in101	
	V	
	V	
191	DET_2	
	.	
	.	
197	.	B6
	.	.
	.	.
201	Q@6.....	
	.	
	.	
206	.	-----> 10YR_SD
204	Q6_in101	
	V	
	V	
209	DET_6	
	.	

```
217 . B3
.
.
223 . -----> 10YR_SD
221 . Q3_in101
. V
. V
226 . DET3
.
.
233 . B4
.
.
237 . Q@4.....
.
.
242 . -----> 10YR_SD
240 . Q4_in101
. V
. V
245 . DET4
.
.
252 . B5
.
.
256 . Q@5.....
.
.
261 . -----> 10YR_SD
259 . Q5_in101
. V
. V
264 . DET5
.
.
271 . B7
.
.
276 . 5+7.....
.
.
281 . -----> 10YR_SD
279 . Q7_in101
.
.
284 . Q@7.....
. V
. V
287 . DET7
.
.
294 . B8
.
.
298 . Q@8.....
. V
. V
301 . DET8
```

```

.
.
308      .      B9A
.
.
312      Q@9A.....
      V
      V
315      DET9A
.
.
322      .      B9
.
.
326      Q@9.....
.
.
331      .----->  PUMP
329      DVPHOEBE
      V
      V
334      DET9
.
.
341      .      B9B
.
.
345      Q@9B.....
      V
      V
348      RT9B
.
.
353      .      B10
.
.
357      Q@10.....
      V
      V
360      RT10
.
.
365      .      B11
.
.
369      Q@11.....
      V
      V
372      RT11

```

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

\*\*\*\*\*  
\*  
\* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
\* JUN 1998 \*  
\* VERSION 4.1 \*  
\*  
\* RUN DATE 18AUG04 TIME 07:38:46 \*  
\*  
\*\*\*\*\*

\*\*\*\*\*  
\*  
\* U.S. ARMY CORPS OF ENGINEERS  
\* HYDROLOGIC ENGINEERING CENTER  
\* 609 SECOND STREET  
\* DAVIS, CALIFORNIA 95616  
\* (916) 756-1104  
\*  
\*\*\*\*\*

\*\*\*\*\*  
ENCINITAS COAST HWY 101 J-14413 8-17-04  
ALTERNATIVE 5 - COMBO ALT 1 + ALT 2C  
10-YR GRADE NORTHBOUND LANES OF HWY 101  
FROM APPROXIMATELY JUPITER TO MOOREGATE  
AT A CONSTANT SLOPE OF 0.1%  
BASINS 9B, 10, AND 11 ARE UNDETAINED AND ROUTED VIA TRAP  
CHANNEL. ALL BASINS U/S ARE DETAINED.  
FN: 10A5.HC1  
\*\*\*\*\*  
ENCINITAS COAST HWY 101 J-14413 5-25-04  
ALTERNATIVE 2 OPTION C - 10-YR GRADE NORTHBOUND LANES OF  
HWY 101 FROM APPROXIMATELY JUPITER TO MOOREGATE  
AT A CONSTANT SLOPE OF 0.1%  
BASINS 9B, 10, AND 11 ARE UNDETAINED AND ROUTED VIA TRAP  
CHANNEL. ALL BASINS U/S ARE DETAINED.  
FN: 10A2C.HC1  
\*\*\*\*\*  
ENCINITAS COAST HWY 101 J-14413 3-19-04  
INCLUDES DIVERSION INTO STORM DRAIN BASED ON ORIFICE PLATE  
Qs  
FN: 10DET5R.HC1  
\*\*\*\*\*  
ENCINITAS COAST HWY 101 J-14413 01/12/04  
SAME AS BELOW EXCEPT CHANGED SV, SQ, SE CARDS BASED ON  
HEC-RAS FN: 101.PRJ (PLAN 12)  
INCLUDES ROUTING THROUGH ALLEY AT UPSTREAM OF END OF STUDY  
FN: 10DET5.HC1  
\*\*\*\*\*  
ENCINITAS COAST HWY 101 J-14413 01/05/04  
SAME AS BELOW EXCEPT 10-YEAR (CN CHANGED FOR PZN=1.5),  
RATING CURVE SV, SQ, SE CARDS CHANGED BASED ON HEC-RAS FN:  
101.PRJ (PLAN 101 R7)  
BASIN AREAS FOR 7-11 CHANGED BACK TO ORIGINAL (2,5,10-YR)  
SIZE THAT DOES NOT INCLUDE AREA EAST OF THE RR TRACKS;  
LAG CHANGED BACK TO ORIGINAL, CN CHANGED BACK TO ORIGINAL  
BASED ON HEC-1 FN: PROSR1.HC1  
FN: 10DET3.HC1  
\*\*\*\*\*  
ENCINITAS COAST HWY 101 J-14413 12/31/03  
SAME AS BELOW EXCEPT MOVED LOCATION OF CONFLUENCE BTWN  
EAST SIDE OF RR TRACKS (BASINS 1A, 1, 1B, 2, & 6) TO BASIN 4,  
WHICH WAS ORIGINALLY MODELED AT BASIN 7 (LEUCADIA)  
FN: 100DET3.HC1  
\*\*\*\*\*  
ENCINITAS COAST HWY 101 J-14413 12/29/03

100-YEAR RUN WITH BASIN AREAS EXTENDED TO THE RIDGE EAST OF  
THE RR TRACKS. PI CARDS CHANGED FOR 100-YR BASED ON FN: E100.HC1  
LAG AND CURVE NUMBERS CHANGED FOR 100-YEAR.

FN:100DET.HC1

BASIN AREAS ALSO CHANGED FOR 7 THROUGH 11. STORAGE RATING  
CURVES BASED ON HEC-RAS OUTPUT FN: 101.PRJ (PLAN 101 R3)

\*\*\*\*\*

ENCINITAS COAST HWY 101

J-14413

SEPT 25, 2003

MODIFIED EXISTING RUN TO MODEL PROPOSED DETENTION OF BASINS  
1A, 1B, 1, 2, 3, 4, 5, 6, AND 8

DETENTION CARDS SA/SV, SQ, SE OBTAINED FROM FN: DSI\_5R.HC1

\*\*\*\*\*

ENCINITAS- COAST HIGHWAY 101

JOB # 14413

09-12-03

MODIFIED PUMP Q TO 1.7 CFS, AND ROUTING OF BASINS 9A, 9B, AND 9  
FROM PUMP STATION THROUGH 10" LATERAL, CONFLUENCING  
WITH MAIN LINE AT AT CONNECTION 3 INSTEAD OF CONNECTION 2  
ALSO CHANGED ROUTING THROUGH MAIN LINE FROM LINE G TO CONNECTION  
2, TO LINE G TO CONNECTION 3

\*\*\*\*\*

ENCINITAS- COAST HIGHWAY 101

JOB # 14413

09-04-03

MODIFIED CURVE NUMBER AND REMOVED % IMPERVIOUS

\*\*\*\*\*

ENCINITAS- COAST HIGHWAY 101

JOB # 14413

06-03-03

POST-IMPROVEMENT (EXISTING) CONDITION FN: 101EX\_5.HC1

5-YEAR, 24-HR STORM EVENT

LAG CALCULATION ARE BASED OFF OF NRCS METHOD

AND ARE A FUNCTION OF RUNOFF COEF. AND VELOCITY

NESTED STORM PER COUNTY OF SAN DIEGO HYDROLOGY MANUAL

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6HR RAINFALL IS 1.6 INCHES

24HR RAINFALL IS 2.5 INCHES

TOTAL BASIN AREA IS .5 SQUARE MILES

88 IO

OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE

IT

HYDROGRAPH TIME DATA

NMIN	5	MINUTES IN COMPUTATION INTERVAL
IDATE	1JAN90	STARTING DATE
ITIME	1200	STARTING TIME
NQ	300	NUMBER OF HYDROGRAPH ORDINATES
NDDATE	2JAN90	ENDING DATE
NDTIME	1255	ENDING TIME
ICENT	19	CENTURY MARK

COMPUTATION INTERVAL .08 HOURS

TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS

DRAINAGE AREA

SQUARE MILES

PRECIPITATION DEPTH INCHES  
LENGTH, ELEVATION FEET  
FLOW CUBIC FEET PER SECOND  
STORAGE VOLUME ACRE-FEET  
SURFACE AREA ACRES  
TEMPERATURE DEGREES FAHRENHEIT

\*\*\* \*\*

\*\*\*\*\*

\* \*

89 KK \* 1A \*

\* \*

\*\*\*\*\*

90 KO OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE  
IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
ISAV2 300 LAST ORDINATE PUNCHED OR SAVED  
TIMINT .083 TIME INTERVAL IN HOURS

\*\*\* \*\*

\*\*\*\*\*

\* \*

209 KK \* DET\_6 \*

\* \*

\*\*\*\*\*

210 KO OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE  
IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
ISAV2 300 LAST ORDINATE PUNCHED OR SAVED  
TIMINT .083 TIME INTERVAL IN HOURS

\*\*\* \*\*

\*\*\*\*\*

\* \*

226 KK \* DET3 \*

\* \*

\*\*\*\*\*

228 KO            OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	300	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

\*\*\* \*\*

\*\*\*\*\*

\*            \*

245 KK            \*            DET4            \*

\*            \*

\*\*\*\*\*

247 KO            OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	300	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

\*\*\* \*\*

\*\*\*\*\*

\*            \*

264 KK            \*            DET5            \*

\*            \*

\*\*\*\*\*

266 KO            OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	300	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

\*\*\* \*\*

\*\*\*\*\*  
\* \*  
\* DET7 \*  
\* \*  
\*\*\*\*\*

287 KK

289 KO

OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE  
IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
ISAV2 300 LAST ORDINATE PUNCHED OR SAVED  
TIMINT .083 TIME INTERVAL IN HOURS

\*\*\* \*\*

\*\*\*\*\*  
\* \*  
\* DET8 \*  
\* \*  
\*\*\*\*\*

301 KK

303 KO

OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE  
IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
ISAV2 300 LAST ORDINATE PUNCHED OR SAVED  
TIMINT .083 TIME INTERVAL IN HOURS

\*\*\* \*\*

\*\*\*\*\*  
\* \*  
\* DET9A \*  
\* \*  
\*\*\*\*\*

315 KK

317 KO

OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE  
IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
ISAV2 300 LAST ORDINATE PUNCHED OR SAVED

TIMINT .083 TIME INTERVAL IN HOURS

\*\*\* \*\*

\*\*\*\*\*

\* \*

334 KK \* DET9 \*

\* \*

\*\*\*\*\*

336 KO OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	300	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	1A	2.	16.08	0.	0.	0.	.01		
ROUTED TO	RT1A	1.	16.58	0.	0.	0.	.01	1.12	16.58
HYDROGRAPH AT	1B	10.	16.17	1.	0.	0.	.03		
ROUTED TO	RT1B	0.	.00	0.	0.	0.	.03	2.88	24.92
ROUTED TO	RT1B	0.	.00	0.	0.	0.	.03	2.00	.00
HYDROGRAPH AT	B1	15.	16.25	3.	1.	1.	.09		
3 COMBINED AT	Q@1	15.	16.25	3.	1.	1.	.13		
DIVERSION TO	10YR_SD	15.	16.25	3.	1.	1.	.13		
HYDROGRAPH AT	Q1_in101	0.	16.25	0.	0.	0.	.13		
ROUTED TO	DET_1	1.	.08	1.	1.	1.	.13	68.47	.00
HYDROGRAPH AT	B2	25.	16.08	3.	1.	1.	.06		
2 COMBINED AT	Q@2	26.	16.08	4.	2.	2.	.19		
DIVERSION TO	10YR_SD	19.	16.08	4.	2.	2.	.19		
HYDROGRAPH AT	Q2_in101	7.	16.08	0.	0.	0.	.19		
ROUTED TO	DET_2	1.	.08	1.	1.	1.	.19	66.73	.00
HYDROGRAPH AT	B6	23.	16.25	5.	1.	1.	.06		
2 COMBINED AT	Q@6	24.	16.25	6.	2.	2.	.25		
DIVERSION TO	10YR_SD	16.	16.25	5.	2.	2.	.25		
HYDROGRAPH AT	Q6_in101	8.	16.25	0.	0.	0.	.25		
ROUTED TO	DET_6	3.	16.50	0.	0.	0.	.25	62.45	16.50
HYDROGRAPH AT	B3	11.	16.08	1.	0.	0.	.02		
DIVERSION TO	10YR_SD	11.	16.08	1.	0.	0.	.02		
HYDROGRAPH AT	Q3_in101	0.	16.08	0.	0.	0.	.02		
ROUTED TO	DET3	0.	.08	0.	0.	0.	.02	59.37	.00
HYDROGRAPH AT	B4	8.	16.00	1.	0.	0.	.02		
2 COMBINED AT	Q@4	8.	16.00	1.	0.	0.	.04		

DIVERSION TO	10YR_SD	7.	16.00	1.	0.	0.	.04		
HYDROGRAPH AT	Q4_in101	1.	16.00	0.	0.	0.	.04		
ROUTED TO	DET4	0.	.08	0.	0.	0.	.04	59.14	.00
HYDROGRAPH AT	B5	10.	16.08	1.	0.	0.	.02		
2 COMBINED AT	Q@5	10.	16.08	1.	0.	0.	.06		
DIVERSION TO	10YR_SD	9.	16.08	1.	0.	0.	.06		
HYDROGRAPH AT	Q5_in101	1.	16.08	0.	0.	0.	.06		
ROUTED TO	DET5	0.	.08	0.	0.	0.	.06	57.52	.00
HYDROGRAPH AT	B7	8.	16.08	1.	0.	0.	.02		
2 COMBINED AT	5+7	8.	16.08	1.	0.	0.	.08		
DIVERSION TO	10YR_SD	6.	16.08	1.	0.	0.	.08		
HYDROGRAPH AT	Q7_in101	2.	16.08	0.	0.	0.	.08		
2 COMBINED AT	Q@7	3.	16.50	0.	0.	0.	.33		
ROUTED TO	DET7	1.	17.08	0.	0.	0.	.33	55.07	17.08
HYDROGRAPH AT	B8	6.	16.08	1.	0.	0.	.01		
2 COMBINED AT	Q@8	6.	16.08	1.	0.	0.	.34		
ROUTED TO	DET8	3.	16.25	1.	0.	0.	.34	55.09	16.25
HYDROGRAPH AT	B9A	11.	16.08	1.	0.	0.	.02		
2 COMBINED AT	Q@9A	12.	16.08	2.	1.	1.	.36		
ROUTED TO	DET9A	5.	16.42	2.	1.	1.	.36	54.62	16.42
HYDROGRAPH AT	B9	16.	16.17	2.	1.	1.	.04		
2 COMBINED AT	Q@9	20.	16.17	4.	1.	1.	.40		
DIVERSION TO	PUMP	4.	16.17	3.	1.	1.	.40		
HYDROGRAPH AT	DVPHOEBE	16.	16.17	2.	0.	0.	.40		
ROUTED TO	DET9	4.	16.67	1.	0.	0.	.40	54.36	16.67
HYDROGRAPH AT	B9B	15.	16.08	2.	1.	0.	.03		
2 COMBINED AT	Q@9B	15.	16.08	3.	1.	1.	.43		
ROUTED TO	RT9B	10.	16.25	3.	1.	1.	.43	.57	16.25
HYDROGRAPH AT	B10	16.	16.00	1.	0.	0.	.02		
2 COMBINED AT	Q@10	19.	16.00	4.	1.	1.	.45		

ROUTED TO	RT10	16.	16.17	4.	1.	1.	.45	.70	16.17
HYDROGRAPH AT	B11	23.	16.08	3.	1.	1.	.04		
2 COMBINED AT	Q@11	39.	16.08	7.	2.	2.	.49		
ROUTED TO	RT11	27.	16.25	7.	2.	2.	.49	.87	16.25

\*\*\* NORMAL END OF HEC-1 \*\*\*

**ALTERNATIVE 5**  
**100-YEAR HEC-1 ANALYSIS**

```

*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*      JUN 1998                *
*      VERSION 4.1             *
*
* RUN DATE 17AUG04 TIME 14:41:36 *
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

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X   X  XXXXXXXX  XXXXX      X
X   X X         X   X      XX
X   X X         X           X
XXXXXXXX XXXX   X           XXXXX X
X   X X         X           X
X   X X         X   X      X
X   X  XXXXXXXX  XXXXX      XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

ENCINITAS 14413  
 100-4R ALT 5  
 100A5.hcl

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

\*DIAGRAM

1 ID \*\*\*\*\*

2 ID ENCINITAS COAST HWY 101 J-14413 7-14-04

3 ID COMBO OF ALTERNATIVE 1 + ALTERNAVE 2C - SAME AS BELOW EXCEPT

4 ID GRADE NORTHBOUND LANES OF HWY 101 FROM APPROXIMATELY

5 ID JUPITER TO MOOREGATE AT A CONSTANT SLOPE OF 0.1% AND

6 ID OVERFLOW STORM DRAIN SYSTEM TO DIVERT 10-YEAR FLOW AT BASIN 7

7 ID BASINS 9B, 10, AND 11 ARE UNDETAINED AND ROUTED VIA TRAP

8 ID CHANNEL. ALL BASINS U/S ARE DETAINED.

9 ID FN: 100A5.HC1

10 ID \*\*\*\*\*

11 ID ENCINITAS COAST HWY 101 J-14413 5-25-04

12 ID ALTERNATIVE 2 OPTION C - GRADE NORTHBOUND LANES OF

13 ID HWY 101 FROM APPROXIMATELY JUPITER TO MOOREGATE

14 ID AT A CONSTANT SLOPE OF 0.1%

15 ID BASINS 9B, 10, AND 11 ARE UNDETAINED AND ROUTED VIA TRAP

16 ID CHANNEL. ALL BASINS U/S ARE DETAINED.

17 ID FN: 100A2C.HC1

18 ID \*\*\*\*\*

19 ID ENCINITAS COAST HWY 101 J-14413 03-04-04

20 ID INCLUDES DIVERSION AT EACH INLET (Q=1 CFS DUE TO ORIFICE

21 ID PLATES) AND DIVERSION AT PHOEBE PUMP STATION

22 ID STORAGE RATING CURVES FOR BASINS 1, 2, AND 6 ARE BASED ON

23 ID VULCAN ONLY HEC-RAS RUN

24 ID STORAGE RATING CURVES FOR BASINS 7-11 ARE BASED ON THE

25 ID 101/VULCAN COMBINED HEC-RAS RUN

26 ID BLOCKED OBSTRUCTIONS ARE INCLUDED FOR THE ALLEY AND VULCAN

27 ID \*\*\*\*\*

28 ID ENCINITAS COAST HWY 101 J-14413 12/29/03

29 ID 100-YEAR RUN WITH BASIN AREAS EXTENDED TO THE RIDGE EAST OF

30 ID THE RR TRACKS. PI CARDS CHANGED FOR 100-YR BASED ON FN: E100.HC1

31 ID LAG AND CURVE NUMBERS CHANGED FOR 100-YEAR.

32 ID FN:100DET.HC1

33 ID BASIN AREAS ALSO CHANGED FOR 7 THROUGH 11. STORAGE RATING

34 ID CURVES BASED ON HEC-RAS OUTPUT FN: 101.PRJ (PLAN 101 R3)

35 ID \*\*\*\*\*

36 ID ENCINITAS COAST HWY 101

37 ID J-14413

38 ID SEPT 25, 2003

39 ID MODIFIED EXISTING RUN TO MODEL PROPOSED DETENTION OF BASINS

40 ID 1A, 1B, 1, 2, 3, 4, 5, 6, AND 8

41 ID DETENTION CARDS SA/SV, SQ, SE OBTAINED FROM FN: DSI\_5R.HC1

42 ID \*\*\*\*\*

43 ID ENCINITAS- COAST HIGHWAY 101

44 ID JOB # 14413

45 ID 09-12-03

46 ID MODIFIED PUMP Q TO 1.7 CFS, AND ROUTING OF BASINS 9A, 9B, AND 9

47 ID FROM PUMP STATION THROUGH 10" LATERAL, CONFLUENCING

48 ID WITH MAIN LINE AT AT CONNECTION 3 INSTEAD OF CONNECTION 2

49 ID ALSO CHANGED ROUTING THROUGH MAIN LINE FROM LINE G TO CONNECTION

50 ID 2, TO LINE G TO CONNECTION 3

51 ID \*\*\*\*\*

52 ID ENCINITAS- COAST HIGHWAY 101

53 ID JOB # 14413

54 ID 09-04-03

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
55      ID  MODIFIED CURVE NUMBER AND REMOVED % IMPERVIOUS
56      ID  *****
57      ID  ENCINITAS- COAST HIGHWAY 101
58      ID  JOB # 14413
59      ID  06-03-03
60      ID  POST-IMPROVEMENT (EXISTING) CONDITION          FN: 101EX_5.HC1
61      ID  5-YEAR, 24-HR STORM EVENT
62      ID  LAG CALCULATION ARE BASED OFF OF NRCS METHOD
63      ID  AND ARE A FUNCTION OF RUNOFF COEF. AND VELOCITY
64      ID  NESTED STORM PER COUNTY OF SAN DIEGO HYDROLOGY MANUAL
65      ID  COPYRIGHT 2003 RICK ENGINEERING COMPANY
66      ID  6HR RAINFALL IS  1.6  INCHES
67      ID  24HR RAINFALL IS  2.5  INCHES
68      ID  TOTAL BASIN AREA IS  .5  SQUARE MILES

*** FREE ***

69      IT      5 01JAN90    1200    300
70      IO      5

71      KK      1A
72      KO      0      0      0      0      21
73      KM  NESTED STORM PER COUNTY OF SAN DIEGO HYDROLOGY MANUAL
74      KM  COPYRIGHT 2003 RICK ENGINEERING COMPANY
75      KM  THE FOLLOWING IT CARD MUST BE USED IN YOUR DATA SET
76      KM  IT 5 01JAN90 1200 300
77      KM  6HR RAINFALL IS  2.5  INCHES
78      KM  24HR RAINFALL IS  4  INCHES
79      KM  DAR30 = .989908
80      KM  DAR60 = .99478
81      KM  DAR180 = .99652
82      KM  DAR360 = .99739
83      KM  DAR1440 = .99826
84      KM  BASIN AREA IS  .87  SQUARE MILES
85      IN      5 01JAN90    1200    300
86      PI  .0047 .00473 .00474 .00476 .00477 .00479 .00481 .00483 .00484 .00486
87      PI  .00488 .0049 .00491 .00494 .00495 .00497 .00499 .00501 .00502 .00505
88      PI  .00506 .00509 .0051 .00513 .00514 .00517 .00518 .00521 .00522 .00525
89      PI  .00527 .0053 .00531 .00534 .00536 .00539 .0054 .00543 .00545 .00548
90      PI  .0055 .00553 .00554 .00558 .00559 .00563 .00565 .00568 .0057 .00573
91      PI  .00575 .00579 .00581 .00584 .00586 .0059 .00592 .00596 .00598 .00602
92      PI  .00604 .00608 .0061 .00614 .00616 .00621 .00623 .00627 .0063 .00634
93      PI  .00636 .00641 .00643 .00648 .00651 .00656 .00658 .00663 .00666 .0067
94      PI  .00674 .00679 .00682 .00688 .0069 .00696 .00699 .00705 .00708 .00714
95      PI  .00717 .00724 .00727 .00733 .00737 .00743 .00747 .00754 .00758 .0076
96      PI  .00768 .00776 .0078 .00788 .00792 .008 .00804 .00812 .00817 .00826
97      PI  .0083 .00839 .00844 .00853 .00858 .00868 .00873 .00884 .00889 .009
98      PI  .00906 .00917 .00923 .00935 .00941 .00954 .0096 .00973 .0098 .00994
99      PI  .01001 .01016 .01024 .01039 .01047 .01064 .01072 .0109 .01099 .01118
100     PI  .01127 .01147 .01158 .01244 .01255 .01278 .0129 .01315 .01328 .01355
101     PI  .01369 .01398 .01414 .01446 .01462 .01497 .01515 .01553 .01573 .0161
102     PI  .01638 .01684 .01709 .01761 .01789 .01848 .0188 .01956 .01992 .02069
103     PI  .02111 .02201 .0225 .02357 .02415 .02544 .02616 .02777 .02867 .03072
104     PI  .0319 .03466 .03629 .04117 .04353 .04959 .05361 .06433 .07327 .10759
105     PI  .15159 .54336 .08629 .05863 .0463 .03812 .03321 .02965 .02693 .02478
106     PI  .02302 .02155 .0203 .01913 .01818 .01735 .01661 .01594 .01534 .01479
107     PI  .01429 .01384 .01342 .01303 .01266 .01168 .01137 .01108 .01081 .0105

```

LINE	ID	1	2	3	4	5	6	7	8	9	10
108	PI	.01031	.01009	.00987	.00967	.00947	.00929	.00911	.00895	.00879	.0086
109	PI	.00849	.00835	.00821	.00808	.00796	.00784	.00772	.00761	.0075	.0074
110	PI	.0073	.0072	.00711	.00702	.00693	.00685	.00676	.00669	.00661	.00653
111	PI	.00646	.00639	.00632	.00625	.00619	.00612	.00606	.006	.00594	.00588
112	PI	.00582	.00577	.00572	.00566	.00561	.00556	.00551	.00546	.00542	.0053
113	PI	.00533	.00528	.00524	.0052	.00516	.00512	.00507	.00504	.005	.00496
114	PI	.00492	.00489	.00485	.00482	.00478	.00475	.00472	0	0	0
115	PI	0	0	0	0	0	0	0	0	0	0
116	PI	0	0								
117	BA	0.01									
118	LS	0	69								
119	UD	0.139									
120	KK	RT1A									
121	KM	ROUTE RUNOFF FROM BASIN 1A THROUGH BASIN 1 (ALONG HW 101)									
122	RS	3	STOR	-1							
123	RC	0.02	0.02	0.02	3225	0.0068					
124	RX	0	5	10	15	20	25	30	35		
125	RY	2	2	1.5	1	1	1.5	2	2		
126	KK	1B									
127	BA	0.03									
128	LS	0	74								
129	UD	0.163									
130	KK	RT1B									
131	KM	ROUTE RUNOFF FROM BASIN 1B THROUGH BASIN 1 (ALONG ORPHEUS ST.)									
132	RS	1	STOR	-1							
133	RC	0.02	0.02	0.02	1125						
134	RX	0	5	10	15	20	25	30	35		
135	RY	2	2	1.5	1	1	1.5	2	2		
136	KK	RT1B									
137	KM	ROUTE RUNOFF FROM BASIN 1B THROUGH BASIN 1 (ALONG HW 101)									
138	RS	1	STOR	-1							
139	RC	0.02	0.02	0.02	1250						
140	RX	0	5	10	15	20	25	30	35		
141	RY	2	2	1.5	1	1	1.5	2	2		
142	KK	1									
143	BA	0.09									
144	LS	0	71								
145	UD	0.282									
146	KK	Q&1									
147	KM	COMBINE BASINS 1A, 1B AND BASIN 1									
148	HC	3									
149	KKQ1_in101										
150	KM	100-YEAR FLOW IN HYW 101 WITH 10-YR FLOWS DIVERTED TO STORM DRAIN									
151	DT	10YR_SD									
152	DI	0	15	70							
153	DQ	0	15	15							

LINE	ID	1	2	3	4	5	6	7	8	9	10
154	KK	DET_11A,1B									
155	KM	DETAIN RUNOFF FROM BASIN 1, 1B AND 1A									
156	RS	1	STOR	-1							
157	SV	2.01	3.34	4.01	5.84	9.54	11.85				
158	SQ	1	50	100	250	500	750				
159	SE	68.47	69.39	69.85	70.76	71.75	72.27				
160	KK	2									
161	BA	0.06									
162	LS	0	76								
163	UD	0.145									
164	KK	Q&2									
165	KM	COMBINE BASIN 1A AND BASIN 1 WITH BASIN 2									
166	HC	2									
167	KKQ2_in101										
168	KM	100-YEAR FLOW IN HYW 101 WITH 10-YR FLOWS DIVERTED TO STORM DRAIN									
169	DT	10YR_SD									
170	DI	0	19	130							
171	DQ	0	19	19							
172	KK	DET_2									
173	KM	DETAIN BASINS 1A, 1 AND 2									
174	RS	1	STOR	-1							
175	SV	2.17	4.58	5.69	7.93	10.6	13.16				
176	SQ	1	50	100	250	500	750				
177	SE	66.73	67.37	67.63	68.09	68.54	68.92				
178	KK	6									
179	BA	0.06									
180	LS	0	81								
181	UD	0.323									
182	KK	Q@6									
183	KM	COMBINE BASIN 1A,1B, 1 & 2 WITH BASIN 6									
184	HC	2									
185	KKQ6_in101										
186	KM	100-YEAR FLOW IN HYW 101 WITH 10-YR FLOWS DIVERTED TO STORM DRAIN									
187	DT	10YR_SD									
188	DI	0	16	250							
189	DQ	0	16	16							
190	KK	DET_6									
191	KO	0	0	0	0	21					
192	KM	DETAIN 6									
193	RS	1	STOR	-1							
194	SV	.02	.27	.43	.8	1.4	1.99				
195	SQ	1	50	100	250	500	750				
196	SE	64.16	65.03	65.31	65.81	66.38	66.85				



LINE	ID	1	2	3	4	5	6	7	8	9	10
240	KKQ5_in101										
241	KM	100-YEAR FLOW IN HYW 101 WITH 10-YR FLOWS DIVERTED TO STORM DRAIN									
242	DT	10YR_SD									
243	DI	0	9	190							
244	DQ	0	9	9							
245	KK	DET5									
246	KM	DETAIN BASIN 5									
247	KO	0	0	0	0	21					
248	RS	1	STOR	-1							
249	SV	1.35	2.32	2.8	3.92	5.58	7.1				
250	SQ	1	50	100	250	500	750				
251	SE	57.76	58.39	58.64	59.17	59.81	60.31				
252	KK	B7									
253	KM	BASIN 7									
254	BA	0.04									
255	LS	0	75								
256	UD	0.300									
257	KK	5+7									
258	KM	COMBINE BASIN 5 WITH BASIN 7									
259	HC	2									
260	KKQ7_in101										
261	KM	100-YEAR FLOW IN HYW 101 WITH 10-YR FLOWS DIVERTED TO STORM DRAIN									
262	DT	10YR_SD									
263	DI	0	6	250							
264	DQ	0	6	6							
265	KK	Q@7									
266	KM	COMBINE 3,4,5,7 AND 1,2,6 (EAST OF TRACKS)									
267	HC	2									
268	KK	DET7									
269	KM	DETAIN AT BASIN 7									
270	KO	0	0	0	0	21					
271	RS	1	STOR	-1							
272	SV	1.37	2.26	2.71	3.74	5.47	6.99				
273	SQ	1	50	100	250	500	750				
274	SE	55.22	55.79	56.03	56.49	57.15	57.66				
275	KK	B8									
276	BA	0.06									
277	LS	0	71								
278	UD	0.090									
279	KK	Q@8									
280	KM	COMBINE BASINS 1A,1,1B,2,6,3,4,5,&7 WITH BASIN 8									
281	HC	2									

LINE	ID	1	2	3	4	5	6	7	8	9	10
282	KK	DET8									
283	KM	DETAIN BASIN 8									
284	KO	0	0	0	0	21					
285	RS	1	STOR	-1							
286	SV	0.72	1.44	1.79	2.6	3.97	5.1				
287	SQ	1	50	100	250	500	750				
288	SE	55.22	55.78	55.99	56.40	57.03	57.52				
289	KK	B9A									
290	BA	0.10									
291	LS	0	71								
292	UD	0.110									
293	KK	Q@9A									
294	KM	COMBINE BASINS 1A,1,1B,2,6,3,4,5,7,&8 WITH BASIN 9A									
295	HC	2									
296	KK	DET9A									
297	KM	DETAIN AT BASIN 9A									
298	KO	0	0	0	0	21					
299	RS	1	STOR	-1							
300	SV	1.31	3.19	4.13	6.62	10.46	13.34				
301	SQ	1	50	100	250	500	750				
302	SE	54.63	55.26	55.51	56.09	56.81	57.33				
303	KK	B9									
304	BA	0.10									
305	LS	0	73								
306	UD	0.11									
307	KK	Q@9									
308	KM	COMBINE BASINS 1A,1,1B,2,6,3,4,5,7,8,&9A WITH BASIN 9									
309	HC	2									
310	KK	COMBINE									
311	KM	DIVERT 5 CFS AT PHOEBE PUMP STATION									
312	DT	PUMP	0	3.5							
313	DI	0	3.5	200							
314	DQ	0	3.5	3.5							
315	KK	DET9									
316	KM	DETAIN AT BASIN 9									
317	KO	0	0	0	0	21					
318	RS	1	STOR	-1							
319	SV	2.1	4.34	5.45	8.83	13.19	16.35				
320	SQ	1	50	100	250	500	750				
321	SE	54.36	55.07	55.36	56.01	56.76	57.26				
322	KK	B9B									
323	BA	0.09									
324	LS	0	74								
325	UD	0.12									



LINE	ID	1	2	3	4	5	6	7	8	9	10
353	KK	RT11									
354	KM	ROUTE BASIN 11 ALONG 101									
355	RC	.018	.018	.018	1650	.001					
356	RX	0	10	15	20	25	30	30	30		
357	RY	2	0.4	0.3	0.2	0.1	0	1	2		
358	ZZ										

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT

LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
71	1A	
	V	
	V	
120	RT1A	
	.	
	.	
126	.	1B
	.	V
	.	V
130	.	RT1B
	.	V
	.	V
136	.	RT1B
	.	.
	.	.
142	.	.
	.	.
	.	.
146	Q&1.....	
	.	
	.	
151	.	-----> 10YR_SD
149	Q1_in101	
	V	
	V	
154	DET_1	
	.	
	.	
160	.	2
	.	.
	.	.
164	Q&2.....	
	.	
	.	
169	.	-----> 10YR_SD
167	Q2_in101	
	V	
	V	
172	DET_2	
	.	
	.	
178	.	6
	.	.
	.	.
182	Q@6.....	
	.	
	.	
187	.	-----> 10YR_SD
185	Q6_in101	
	V	
	V	
190	DET_6	
	.	

```
.
197 .          B3
.
.
203 .          .-----> 10YR_SD
201 .   Q3_in101
.     V
.     V
206 .          DET3
.
.
213 .          .          B4
.
.
217 .          3+4.....
.
.
222 .          .-----> 10YR_SD
220 .   Q4_in101
.     V
.     V
225 .          DET4
.
.
232 .          .          B5
.
.
237 .          Q@5.....
.
.
242 .          .-----> 10YR_SD
240 .   Q5_in101
.     V
.     V
245 .          DET5
.
.
252 .          .          B7
.
.
257 .          5+7.....
.
.
262 .          .-----> 10YR_SD
260 .   Q7_in101
.
.
265 .   Q@7.....
.     V
.     V
268 .   DET7
.
.
275 .          .          B8
.
.
279 .   Q@8.....
.     V
.     V
282 .   DET8
```

```

.
.
289 .          B9A
.
.
293 Q@9A.....
.
V
.
V
296 DET9A
.
.
303 .          B9
.
.
307 Q@9.....
.
.
312 .----->    PUMP
310 COMBINE
.
V
.
V
315 DET9
.
.
322 .          B9B
.
.
326 Q@9B.....
.
V
.
V
329 RT9B
.
.
334 .          B10
.
.
338 Q@10.....
.
V
.
V
341 RT10
.
.
346 .          B11
.
.
350 Q@11.....
.
V
.
V
353 RT11

```

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

\*\*\*\*\*  
\*  
\* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
\* JUN 1998 \*  
\* VERSION 4.1 \*  
\*  
\* RUN DATE 17AUG04 TIME 14:41:36 \*  
\*  
\*\*\*\*\*

\*\*\*\*\*  
\*  
\* U.S. ARMY CORPS OF ENGINEERS  
\* HYDROLOGIC ENGINEERING CENTER  
\* 609 SECOND STREET  
\* DAVIS, CALIFORNIA 95616  
\* (916) 756-1104  
\*  
\*\*\*\*\*

\*\*\*\*\*  
ENCINITAS COAST HWY 101 J-14413 7-14-04  
COMBO OF ALTERNATIVE 1 + ALTERNAVE 2C - SAME AS BELOW EXCEPT  
GRADE NORTHBOUND LANES OF HWY 101 FROM APPROXIMATELY  
JUPITER TO MOOREGATE AT A CONSTANT SLOPE OF 0.1% AND  
OVERFLOW STORM DRAIN SYSTEM TO DIVERT 10-YEAR FLOW AT BASIN 7  
BASINS 9B, 10, AND 11 ARE UNDETAINED AND ROUTED VIA TRAP  
CHANNEL. ALL BASINS U/S ARE DETAINED.  
FN: 100A5.HC1

\*\*\*\*\*  
ENCINITAS COAST HWY 101 J-14413 5-25-04  
ALTERNATIVE 2 OPTION C - GRADE NORTHBOUND LANES OF  
HWY 101 FROM APPROXIMATELY JUPITER TO MOOREGATE  
AT A CONSTANT SLOPE OF 0.1%  
BASINS 9B, 10, AND 11 ARE UNDETAINED AND ROUTED VIA TRAP  
CHANNEL. ALL BASINS U/S ARE DETAINED.  
FN: 100A2C.HC1

\*\*\*\*\*  
ENCINITAS COAST HWY 101 J-14413 03-04-04  
INCLUDES DIVERSION AT EACH INLET (Q=1 CFS DUE TO ORIFICE  
PLATES) AND DIVERSION AT PHOEBE PUMP STATION  
STORAGE RATING CURVES FOR BASINS 1, 2, AND 6 ARE BASED ON  
VULCAN ONLY HEC-RAS RUN  
STORAGE RATING CURVES FOR BASINS 7-11 ARE BASED ON THE  
101/VULCAN COMBINED HEC-RAS RUN  
BLOCKED OBSTRUCTIONS ARE INCLUDED FOR THE ALLEY AND VULCAN  
\*\*\*\*\*

ENCINITAS COAST HWY 101 J-14413 12/29/03  
100-YEAR RUN WITH BASIN AREAS EXTENDED TO THE RIDGE EAST OF  
THE RR TRACKS. PI CARDS CHANGED FOR 100-YR BASED ON FN: E100.HC1  
LAG AND CURVE NUMBERS CHANGED FOR 100-YEAR.  
FN: 100DET.HC1

BASIN AREAS ALSO CHANGED FOR 7 THROUGH 11. STORAGE RATING  
CURVES BASED ON HEC-RAS OUTPUT FN: 101.PRJ (PLAN 101 R3)  
\*\*\*\*\*

ENCINITAS COAST HWY 101  
J-14413  
SEPT 25, 2003  
MODIFIED EXISTING RUN TO MODEL PROPOSED DETENTION OF BASINS  
1A, 1B, 1, 2, 3, 4, 5, 6, AND 8  
DETENTION CARDS SA/SV, SQ, SE OBTAINED FROM FN: DSI\_5R.HC1  
\*\*\*\*\*  
ENCINITAS- COAST HIGHWAY 101  
JOB # 14413  
09-12-03  
MODIFIED PUMP Q TO 1.7 CFS, AND ROUTING OF BASINS 9A, 9B, AND 9

FROM PUMP STATION THROUGH 10" LATERAL, CONFLUENCING  
WITH MAIN LINE AT AT CONNECTION 3 INSTEAD OF CONNECTION 2  
ALSO CHANGED ROUTING THROUGH MAIN LINE FROM LINE G TO CONNECTION  
2, TO LINE G TO CONNECTION 3

\*\*\*\*\*  
ENCINITAS- COAST HIGHWAY 101

JOB # 14413  
09-04-03

MODIFIED CURVE NUMBER AND REMOVED % IMPERVIOUS  
\*\*\*\*\*

ENCINITAS- COAST HIGHWAY 101  
JOB # 14413

06-03-03  
POST-IMPROVEMENT (EXISTING) CONDITION      FN: 101EX\_5.HC1  
5-YEAR, 24-HR STORM EVENT  
LAG CALCULATION ARE BASED OFF OF NRCS METHOD  
AND ARE A FUNCTION OF RUNOFF COEF. AND VELOCITY  
NESTED STORM PER COUNTY OF SAN DIEGO HYDROLOGY MANUAL  
COPYRIGHT 2003 RICK ENGINEERING COMPANY  
6HR RAINFALL IS 1.6 INCHES  
24HR RAINFALL IS 2.5 INCHES  
TOTAL BASIN AREA IS .5 SQUARE MILES

70 IO            OUTPUT CONTROL VARIABLES

IPRNT            5    PRINT CONTROL  
IPLOT            0    PLOT CONTROL  
QSCAL            0.    HYDROGRAPH PLOT SCALE

IT            HYDROGRAPH TIME DATA

NMIN            5    MINUTES IN COMPUTATION INTERVAL  
IDATE           1JAN90    STARTING DATE  
ITIME           1200    STARTING TIME  
NQ              300    NUMBER OF HYDROGRAPH ORDINATES  
NDDATE          2JAN90    ENDING DATE  
NDTIME          1255    ENDING TIME  
ICENT           19    CENTURY MARK

COMPUTATION INTERVAL      .08 HOURS  
TOTAL TIME BASE          24.92 HOURS

ENGLISH UNITS

DRAINAGE AREA            SQUARE MILES  
PRECIPITATION DEPTH      INCHES  
LENGTH, ELEVATION        FEET  
FLOW                      CUBIC FEET PER SECOND  
STORAGE VOLUME            ACRE-FEET  
SURFACE AREA              ACRES  
TEMPERATURE               DEGREES FAHRENHEIT

\*\*\*\*\*

\*\*\*\*\*  
\*            \*  
71 KK      \*            1A      \*  
\*            \*  
\*\*\*\*\*

72 KO

OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	300	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

\*\*\* \*\*

\*\*\*\*\*

\* \*

190 KK \* DET\_6 \*

\* \*

\*\*\*\*\*

191 KO

OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	300	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

\*\*\* \*\*

\*\*\*\*\*

\* \*

206 KK \* DET3 \*

\* \*

\*\*\*\*\*

208 KO

OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	300	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

\*\*\* \*\*

\*\*\*\*\*

\* \*  
225 KK \* DET4 \*  
\* \*  
\*\*\*\*\*

227 KO OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE  
IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
ISAV2 300 LAST ORDINATE PUNCHED OR SAVED  
TIMINT .083 TIME INTERVAL IN HOURS

\*\*\* \*\*

\*\*\*\*\*

\* \*  
245 KK \* DET5 \*  
\* \*  
\*\*\*\*\*

247 KO OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE  
IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
ISAV2 300 LAST ORDINATE PUNCHED OR SAVED  
TIMINT .083 TIME INTERVAL IN HOURS

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\* \*  
268 KK \* DET7 \*  
\* \*  
\*\*\*\*\*

270 KO OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE  
IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
ISAV2 300 LAST ORDINATE PUNCHED OR SAVED  
TIMINT .083 TIME INTERVAL IN HOURS

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\* \*

282 KK \* DET8 \*

\* \*

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284 KO OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	300	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

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\* \*

296 KK \* DET9A \*

\* \*

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298 KO OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	300	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

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\* \*

315 KK \* DET9 \*

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317 KO OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE

IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	300	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

WARNING --- ROUTED OUTFLOW ( 152.) IS GREATER THAN MAXIMUM OUTFLOW ( 145.) IN STORAGE-OUTFLOW TABLE

WARNING --- ROUTED OUTFLOW ( 151.) IS GREATER THAN MAXIMUM OUTFLOW ( 145.) IN STORAGE-OUTFLOW TABLE

WARNING --- ROUTED OUTFLOW ( 159.) IS GREATER THAN MAXIMUM OUTFLOW ( 145.) IN STORAGE-OUTFLOW TABLE

WARNING --- ROUTED OUTFLOW ( 186.) IS GREATER THAN MAXIMUM OUTFLOW ( 145.) IN STORAGE-OUTFLOW TABLE

WARNING --- ROUTED OUTFLOW ( 178.) IS GREATER THAN MAXIMUM OUTFLOW ( 145.) IN STORAGE-OUTFLOW TABLE

WARNING --- ROUTED OUTFLOW ( 162.) IS GREATER THAN MAXIMUM OUTFLOW ( 145.) IN STORAGE-OUTFLOW TABLE

WARNING --- ROUTED OUTFLOW ( 150.) IS GREATER THAN MAXIMUM OUTFLOW ( 145.) IN STORAGE-OUTFLOW TABLE

WARNING --- ROUTED OUTFLOW ( 190.) IS GREATER THAN MAXIMUM OUTFLOW ( 145.) IN STORAGE-OUTFLOW TABLE

WARNING --- ROUTED OUTFLOW ( 260.) IS GREATER THAN MAXIMUM OUTFLOW ( 145.) IN STORAGE-OUTFLOW TABLE

WARNING --- ROUTED OUTFLOW ( 276.) IS GREATER THAN MAXIMUM OUTFLOW ( 145.) IN STORAGE-OUTFLOW TABLE

WARNING --- ROUTED OUTFLOW ( 255.) IS GREATER THAN MAXIMUM OUTFLOW ( 145.) IN STORAGE-OUTFLOW TABLE

WARNING --- ROUTED OUTFLOW ( 225.) IS GREATER THAN MAXIMUM OUTFLOW ( 145.) IN STORAGE-OUTFLOW TABLE

WARNING --- ROUTED OUTFLOW ( 198.) IS GREATER THAN MAXIMUM OUTFLOW ( 145.) IN STORAGE-OUTFLOW TABLE

WARNING --- ROUTED OUTFLOW ( 178.) IS GREATER THAN MAXIMUM OUTFLOW ( 145.) IN STORAGE-OUTFLOW TABLE

WARNING --- ROUTED OUTFLOW ( 163.) IS GREATER THAN MAXIMUM OUTFLOW ( 145.) IN STORAGE-OUTFLOW TABLE

WARNING --- ROUTED OUTFLOW ( 152.) IS GREATER THAN MAXIMUM OUTFLOW ( 145.) IN STORAGE-OUTFLOW TABLE

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	1A	9.	16.08	1.	0.	0.	.01		
ROUTED TO	RT1A	6.	16.42	1.	0.	0.	.01	1.31	16.42
HYDROGRAPH AT	1B	31.	16.08	4.	1.	1.	.03		
ROUTED TO	RT1B	0.	.00	0.	0.	0.	.03	5.63	24.92
ROUTED TO	RT1B	0.	.00	0.	0.	0.	.03	2.00	.00
HYDROGRAPH AT	1	62.	16.25	11.	3.	3.	.09		
3 COMBINED AT	Q&1	67.	16.25	12.	4.	4.	.13		
DIVERSION TO	10YR_SD	15.	16.25	8.	3.	3.	.13		
HYDROGRAPH AT	Q1_in101	52.	16.25	4.	1.	1.	.13		
ROUTED TO	DET_1	13.	16.67	2.	1.	1.	.13	68.70	16.67
HYDROGRAPH AT	2	72.	16.08	9.	3.	3.	.06		
2 COMBINED AT	Q&2	73.	16.08	11.	4.	4.	.19		
DIVERSION TO	10YR_SD	19.	16.08	9.	3.	3.	.19		
HYDROGRAPH AT	Q2_in101	54.	16.08	3.	1.	1.	.19		
ROUTED TO	DET_2	1.	.08	1.	1.	1.	.19	66.73	.00
HYDROGRAPH AT	6	55.	16.25	11.	3.	3.	.06		
2 COMBINED AT	Q@6	56.	16.25	12.	4.	4.	.25		
DIVERSION TO	10YR_SD	16.	16.25	8.	4.	4.	.25		
HYDROGRAPH AT	Q6_in101	40.	16.25	3.	1.	1.	.25		
ROUTED TO	DET_6	38.	16.33	4.	2.	2.	.25	64.82	16.33
HYDROGRAPH AT	B3	30.	16.08	3.	1.	1.	.02		
DIVERSION TO	10YR_SD	11.	16.08	3.	1.	1.	.02		
HYDROGRAPH AT	Q3_in101	19.	16.08	1.	0.	0.	.02		
ROUTED TO	DET3	1.	.08	1.	1.	1.	.02	59.68	.00
HYDROGRAPH AT	B4	27.	16.00	3.	1.	1.	.02		
2 COMBINED AT	3+4	28.	16.00	4.	2.	2.	.04		

DIVERSION TO	10YR_SD	7.	16.00	3.	2.	2.	.04		
HYDROGRAPH AT	Q4_in101	21.	16.00	1.	0.	0.	.04		
ROUTED TO	DET4	1.	.08	1.	1.	1.	.04	59.54	.00
HYDROGRAPH AT	B5	28.	16.08	3.	1.	1.	.02		
2 COMBINED AT	Q@5	29.	16.08	4.	2.	2.	.06		
DIVERSION TO	10YR_SD	9.	16.08	3.	2.	2.	.06		
HYDROGRAPH AT	Q5_in101	20.	16.08	1.	0.	0.	.06		
ROUTED TO	DET5	1.	.08	1.	1.	1.	.06	57.76	.00
HYDROGRAPH AT	B7	31.	16.25	6.	2.	2.	.04		
2 COMBINED AT	5+7	32.	16.25	7.	3.	3.	.10		
DIVERSION TO	10YR_SD	6.	16.25	4.	2.	2.	.10		
HYDROGRAPH AT	Q7_in101	26.	16.25	2.	1.	1.	.10		
2 COMBINED AT	Q@7	62.	16.33	6.	2.	2.	.35		
ROUTED TO	DET7	47.	16.50	6.	2.	2.	.35	55.75	16.50
HYDROGRAPH AT	B8	69.	16.08	7.	2.	2.	.06		
2 COMBINED AT	Q@8	78.	16.08	14.	5.	4.	.41		
ROUTED TO	DET8	57.	16.50	14.	5.	4.	.41	55.81	16.50
HYDROGRAPH AT	B9A	114.	16.08	12.	4.	4.	.10		
2 COMBINED AT	Q@9A	158.	16.08	26.	8.	8.	.51		
ROUTED TO	DET9A	90.	16.33	26.	8.	8.	.51	55.46	16.33
HYDROGRAPH AT	B9	123.	16.08	13.	4.	4.	.10		
2 COMBINED AT	Q@9	173.	16.08	39.	12.	12.	.61		
DIVERSION TO	PUMP	4.	16.08	4.	2.	2.	.61		
HYDROGRAPH AT	COMBINE	170.	16.08	36.	10.	10.	.61		
ROUTED TO	DET9	106.	16.42	34.	10.	10.	.61	55.39	16.42
HYDROGRAPH AT	B9B	111.	16.08	12.	4.	4.	.09		
2 COMBINED AT	Q@9B	159.	16.08	46.	14.	13.	.70		
ROUTED TO	RT9B	152.	16.17	46.	14.	13.	.70	2.05	16.17
HYDROGRAPH AT	B10	62.	16.08	7.	2.	2.	.05		
2 COMBINED AT	Q@10	186.	16.17	53.	16.	15.	.75		

ROUTED TO	RT10	186.	16.17	53.	16.	15.	.75	2.29	16.17
HYDROGRAPH AT	B11	141.	16.08	18.	6.	5.	.12		
2 COMBINED AT	Q@11	313.	16.17	70.	21.	21.	.87		
ROUTED TO	RT11	276.	16.25	70.	21.	21.	.87	2.94	16.25

\*\*\* NORMAL END OF HEC-1 \*\*\*

**ATTACHMENT 4**

**ALTERNATIVE 5  
10-YEAR AND 100-YEAR  
HEC-RAS ANALYSES**

**ALTERNATIVE 5**  
**10-YEAR HEC-RAS ANALYSIS**

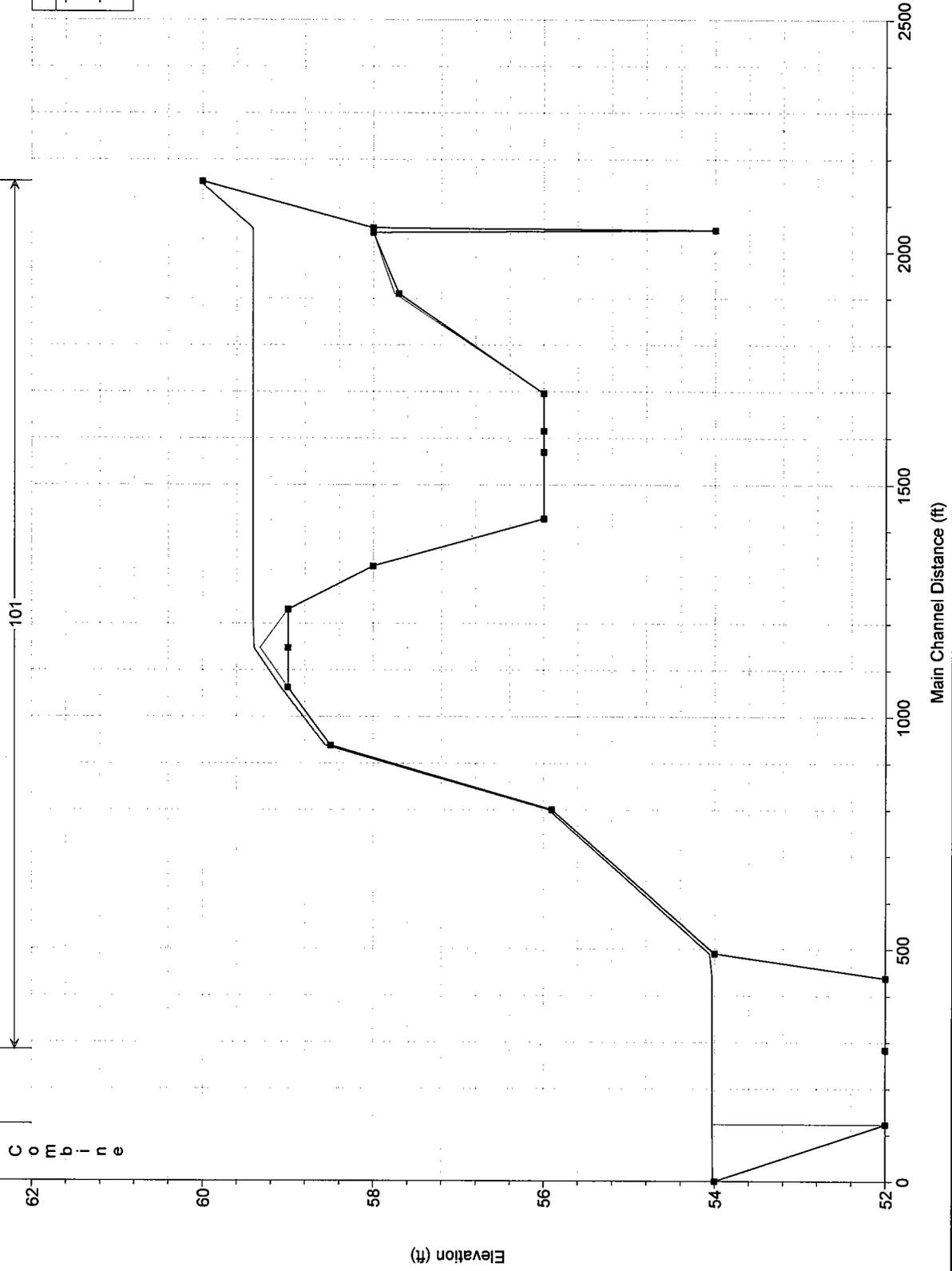
HEC-RAS Plan: 105cut Profile: 100

Reach	River Sta	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Vulcan	3300.14	1.00	72.16	72.24	72.24	72.28	0.042115	1.59	0.63	8.16	1.00
Vulcan	3200.15	1.00	71.16	71.32	71.24	71.33	0.003637	0.76	1.32	8.31	0.33
Vulcan	3100.16	1.00	70.76	70.91	70.84	70.92	0.004658	0.82	1.23	8.30	0.37
Vulcan	3000.17	1.00	70.26	70.40	70.34	70.41	0.005501	0.86	1.17	8.29	0.40
Vulcan	2900.18	1.00	69.76	69.91	69.84	69.92	0.004387	0.81	1.25	8.31	0.36
Vulcan	2800.19	1.00	69.26	69.40	69.34	69.41	0.006034	0.89	1.14	8.28	0.42
Vulcan	2700.20	1.00	67.96	68.03	68.03	68.08	0.050347	1.68	0.60	8.15	1.09
Vulcan	2600.21	1.00	65.96	66.86	66.04	66.86	0.000011	0.13	8.05	9.81	0.02
Vulcan	2500.22	1.00	64.46	66.86	64.54	66.86	0.000000	0.04	25.01	12.81	0.01
Vulcan	2400.23	1.00	63.96	66.86	64.04	66.86	0.000000	0.04	31.66	13.81	0.00
Vulcan	2300.24	1.00	63.46	66.86	63.54	66.86	0.000000	0.03	38.81	14.81	0.00
Vulcan	2200.25	1.00	62.96	66.86	63.04	66.86	0.000000	0.03	46.96	32.44	0.00
Vulcan	2100.26	1.00	62.46	66.86	62.54	66.86	0.000000	0.01	129.37	82.28	0.00
Vulcan	245	1.00	64.00	66.86		66.86	0.000000	0.01	118.42	81.57	0.00
Vulcan	240	1.00	64.00	66.86		66.86	0.000000	0.01	160.35	114.77	0.00
Vulcan	235	1.00	66.00	66.86		66.86	0.000000	0.01	121.00	155.23	0.00
Vulcan	230	1.00	66.00	66.86		66.86	0.000000	0.01	132.43	171.70	0.00
Vulcan	225	1.00	66.00	66.86		66.86	0.000000	0.01	93.65	119.89	0.00
Vulcan	220	1.00	66.00	66.86		66.86	0.000000	0.00	271.66	333.13	0.00
Vulcan	215	1.00	67.90	66.83	66.83	66.86	0.014435		0.68	9.90	0.00
Vulcan	195	3.00	68.00	66.21	66.05	66.21	0.000146		10.58	59.64	0.00
Vulcan	175	3.00	65.50	65.93	65.93	66.04	0.010203	2.68	1.12	5.19	1.01
Vulcan	165	3.00	63.00	63.71	63.37	63.72	0.000307	0.65	4.60	12.86	0.19
Vulcan	150	3.00	63.00	63.31	63.31	63.39	0.011229	2.26	1.33	8.63	1.01
101	230	0.10	60.00	60.03	60.03	60.04	0.028192	0.76	0.13	8.65	1.09
101	225.3	0.10	58.00	59.41	58.01	59.41	0.000000	0.00	70.79	67.30	0.00
101	225.2	0.10	54.64	59.41		59.41	0.000000	0.00	148.91	67.30	0.00
101	225.1	0.10	58.00	59.41		59.41	0.000000	0.00	70.79	67.30	0.00
101	220	0.10	57.75	59.41		59.41	0.000000	0.00	127.41	106.42	0.00
101	215	0.10	56.00	59.41		59.41	0.000000	0.00	380.98	157.42	0.00
101	210	0.10	56.00	59.41		59.41	0.000000	0.00	274.05	91.81	0.00
101	205	0.10	56.00	59.41		59.41	0.000000	0.00	339.34	114.67	0.00
101	195	0.10	56.00	59.41		59.41	0.000000	0.00	174.94	97.38	0.00
101	190	0.10	58.00	59.41		59.41	0.000000	0.00	110.17	90.00	0.00
101	185	0.10	59.00	59.41		59.41	0.000000	0.01	11.82	50.00	0.00
101	180	0.10	59.32	59.40	59.39	59.41	0.013313	0.92	0.11	3.02	0.85

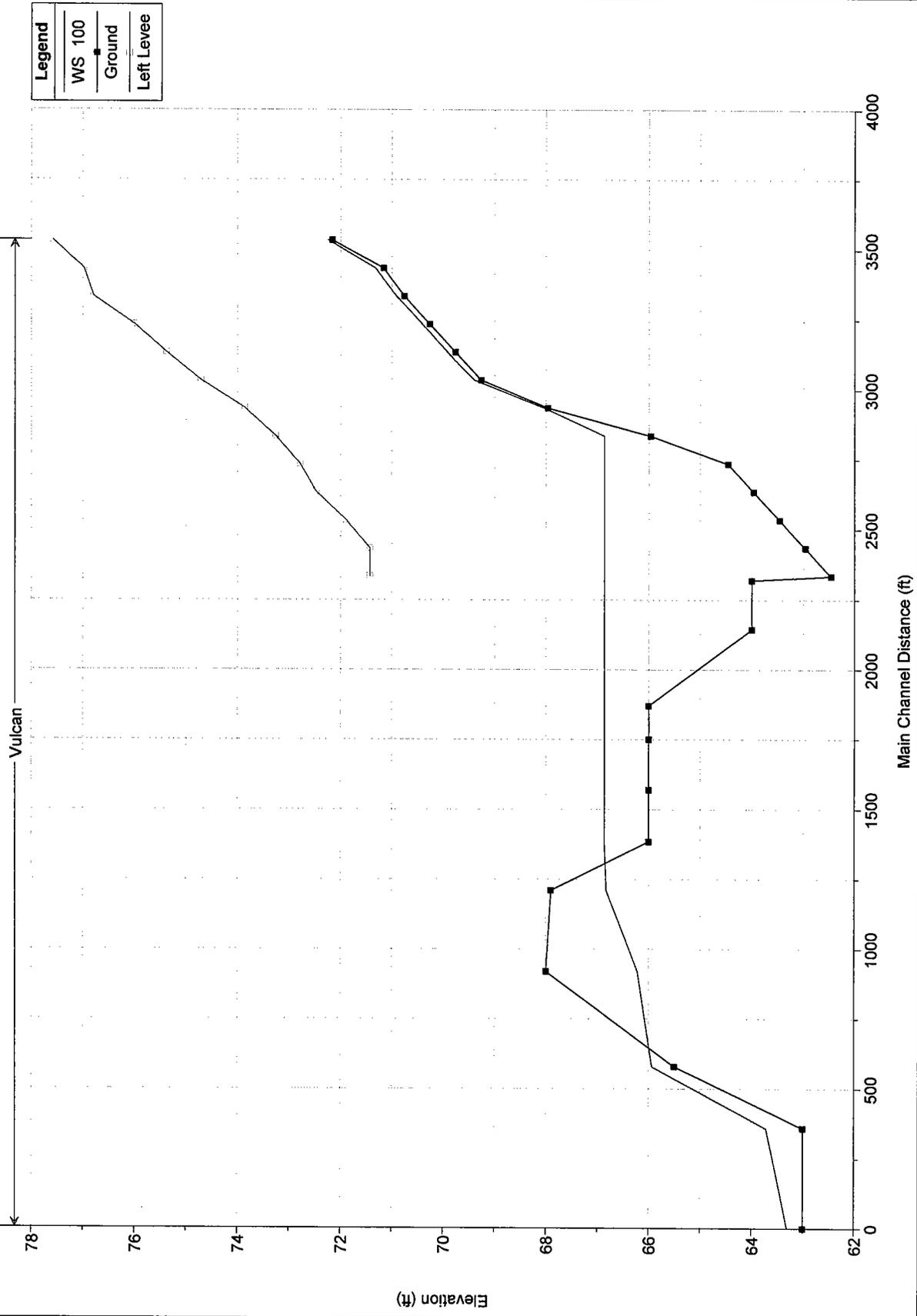
HEC-RAS Plan: 105cut Profile: 100 (Continued)

Reach	River Sta	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit.W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
101	175	0.10	59.00	59.08		59.09	0.001738	0.41	0.25	5.18	0.33
101	170	0.10	58.50	58.56	58.56	58.57	0.019285	0.96	0.10	3.68	1.00
101	165	0.10	55.90	55.94	55.92	55.94	0.002926	0.28	0.36	19.44	0.36
101	160	0.10	54.00	54.06	54.06	54.07	0.018859	0.96	0.10	3.59	1.00
101	150	0.10	52.00	54.03	52.08	54.03	0.000000	0.00	63.65	94.08	0.00
101	145	0.10	52.00	54.03		54.03	0.000000	0.00	56.28	32.31	0.00
Combine	140	1.00	52.00	54.03	52.16	54.03	0.000000	0.02	55.36	38.64	0.00
Combine	135	1.00	54.00	54.02	54.02	54.03	0.009999	0.57	1.76	84.04	0.69

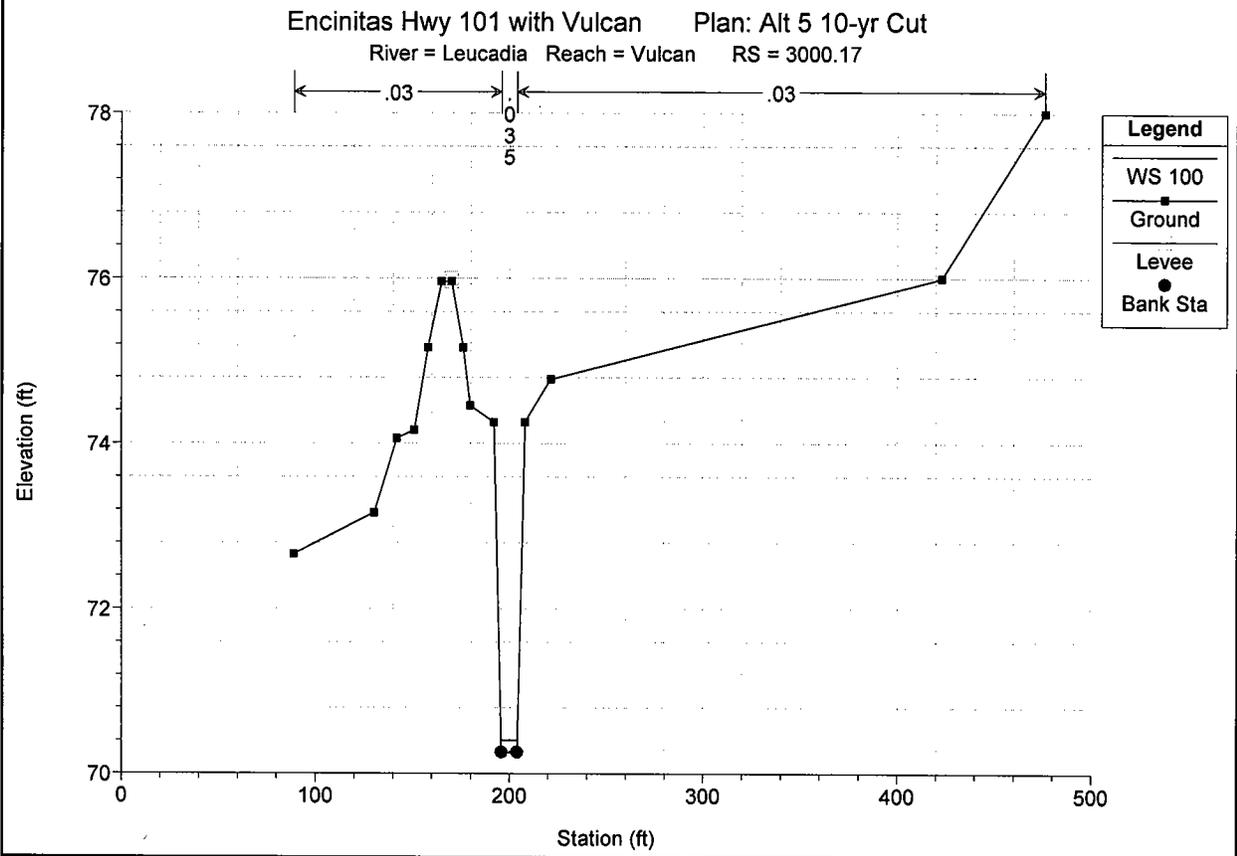
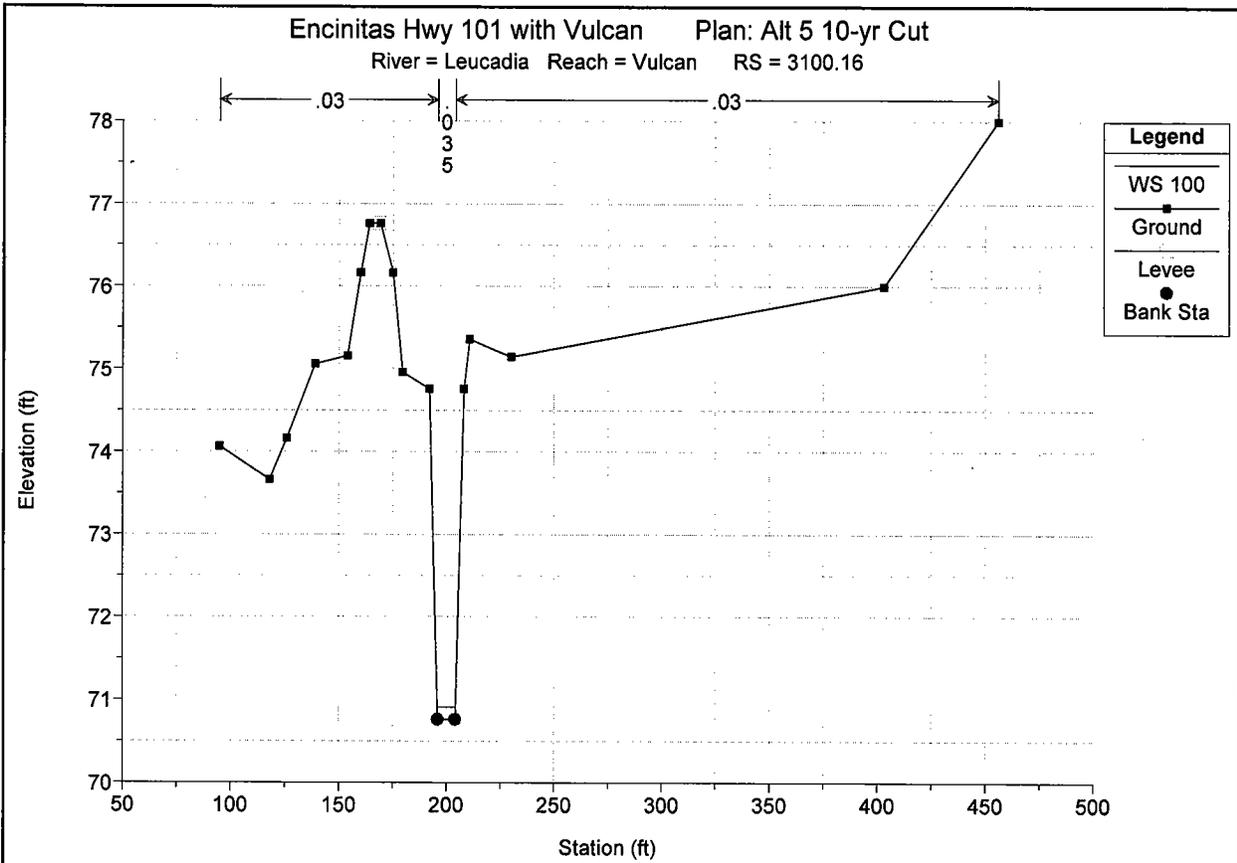
Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut

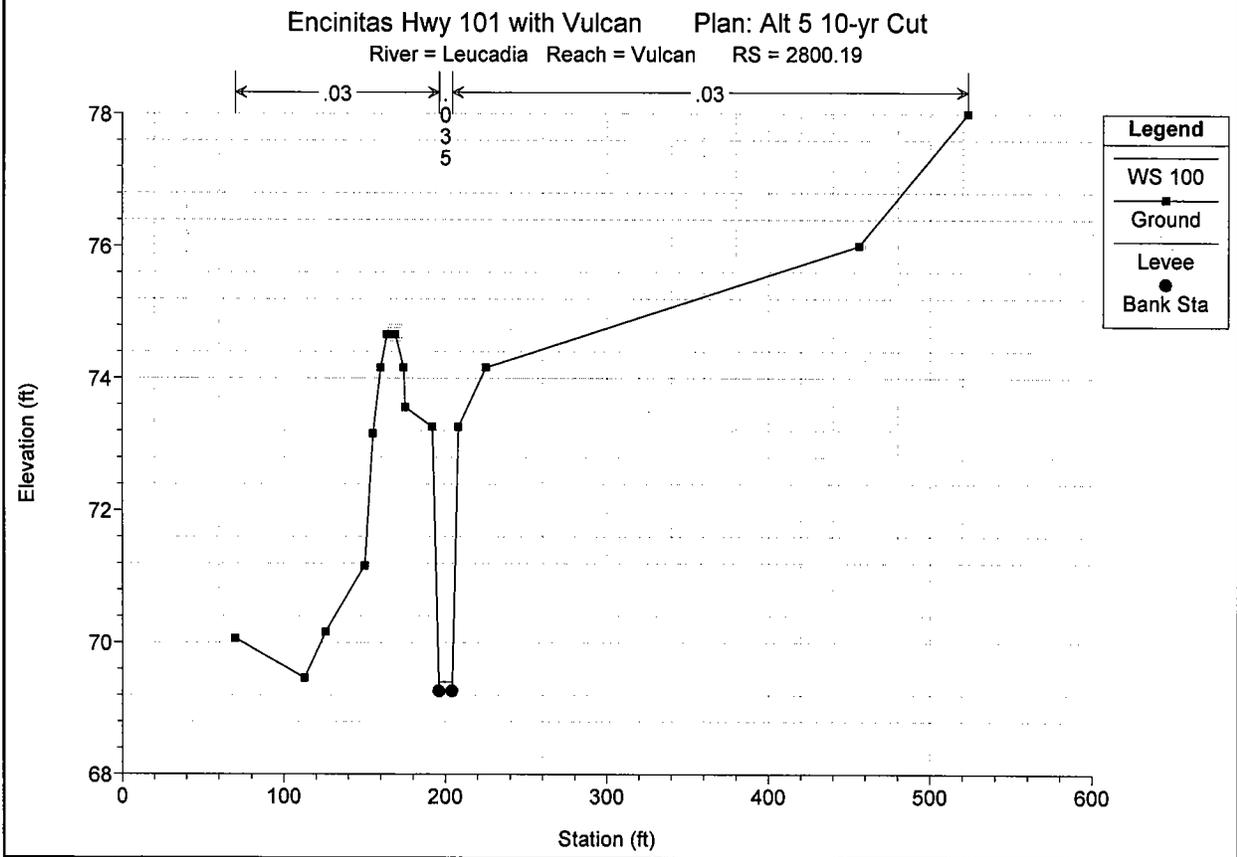
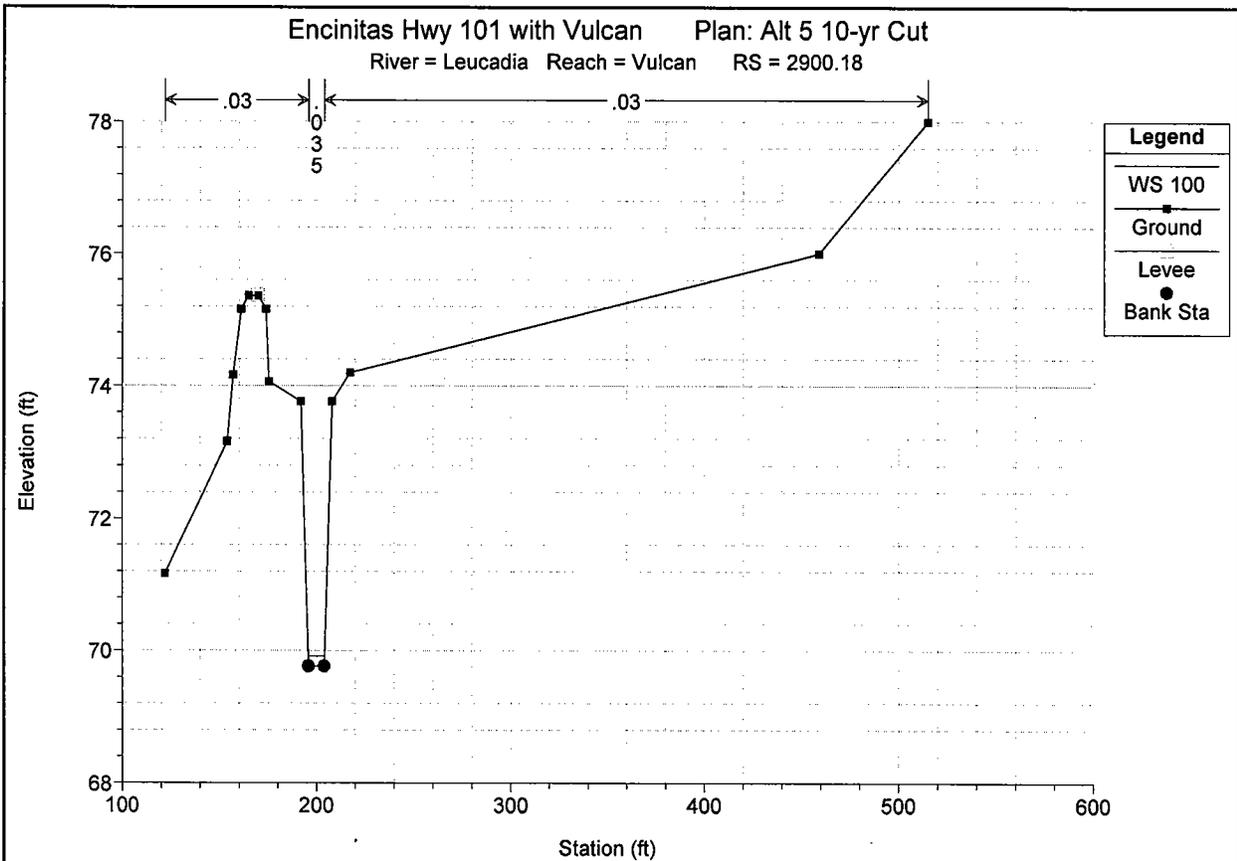


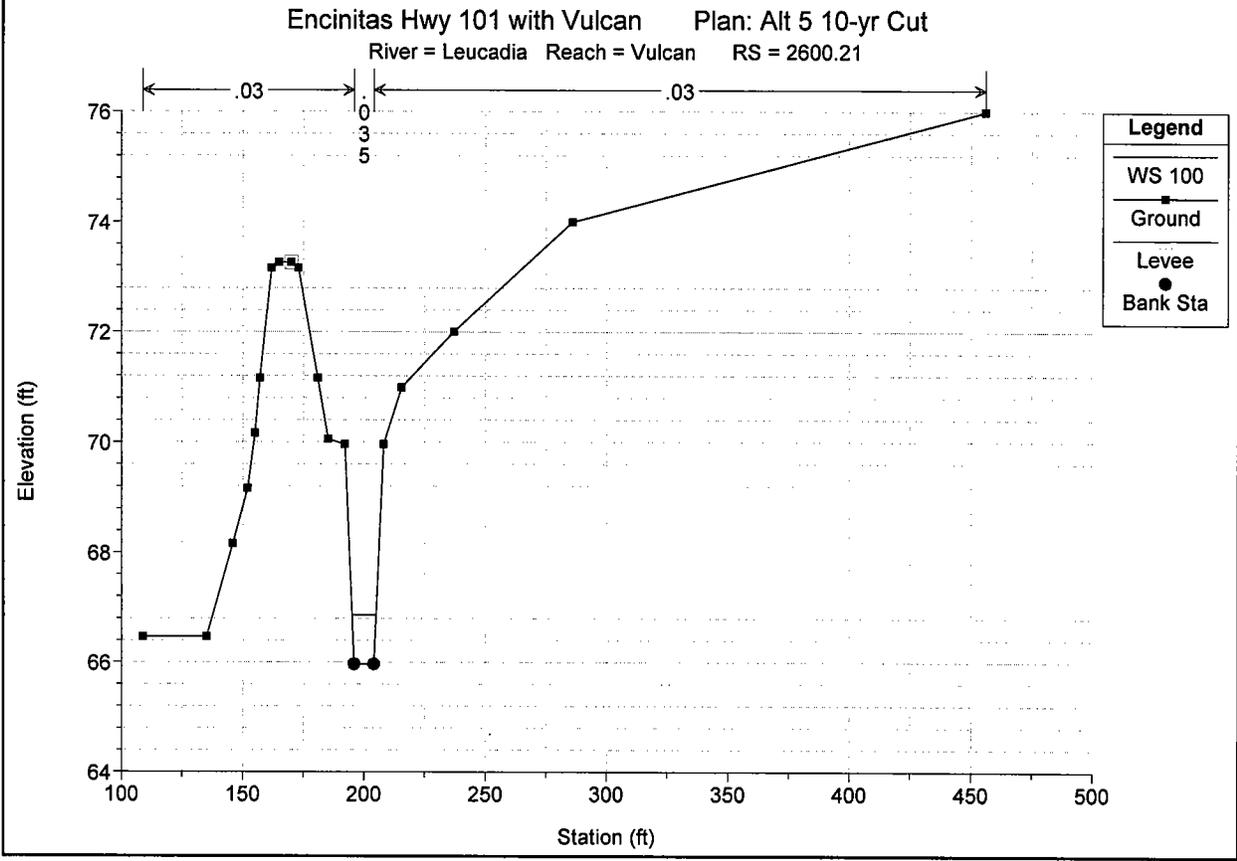
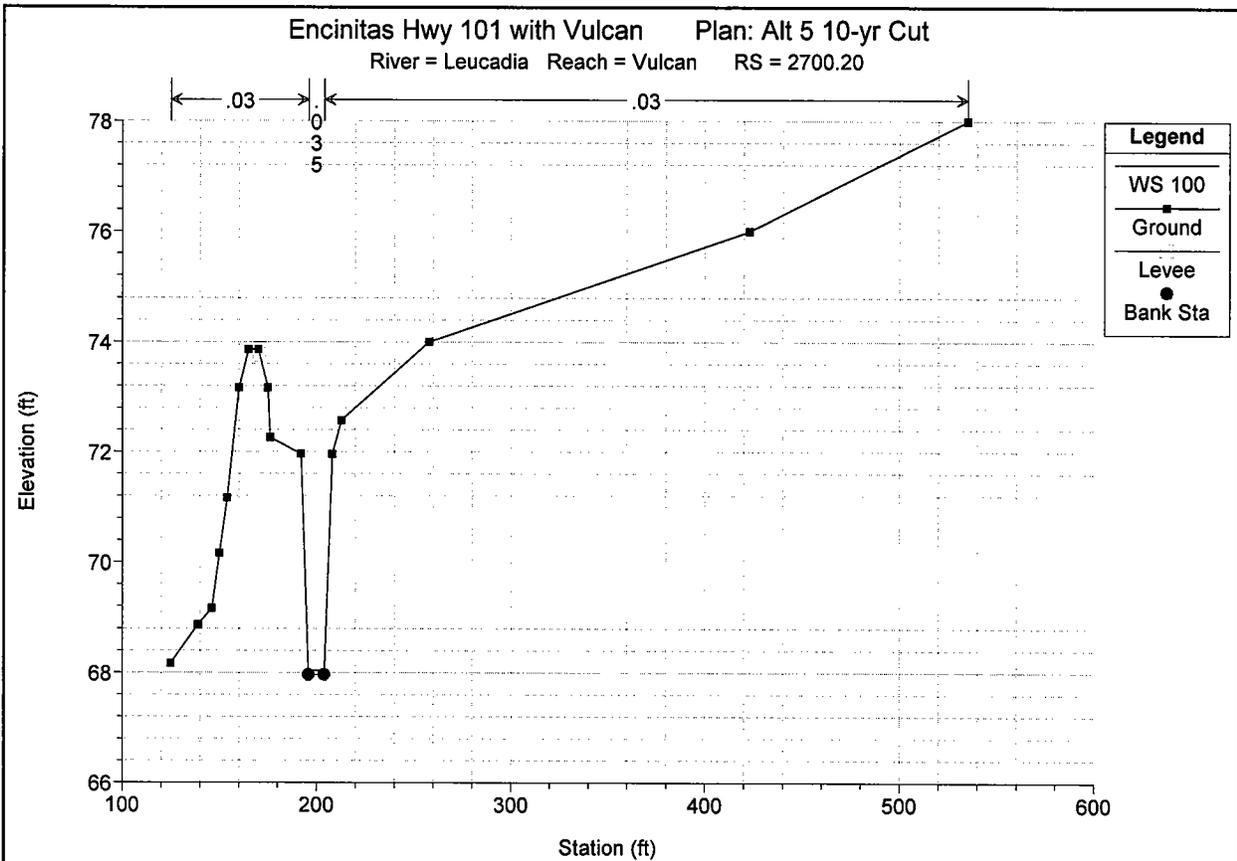
Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut

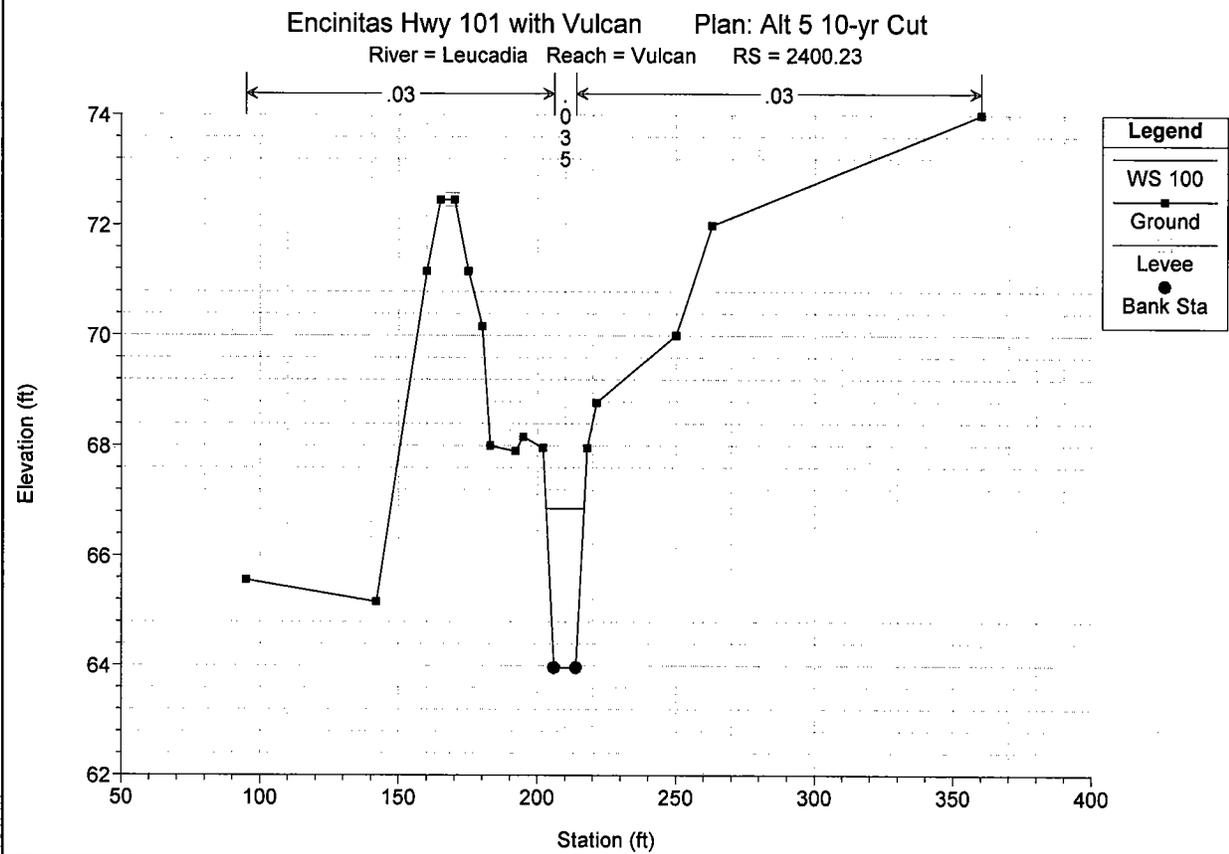
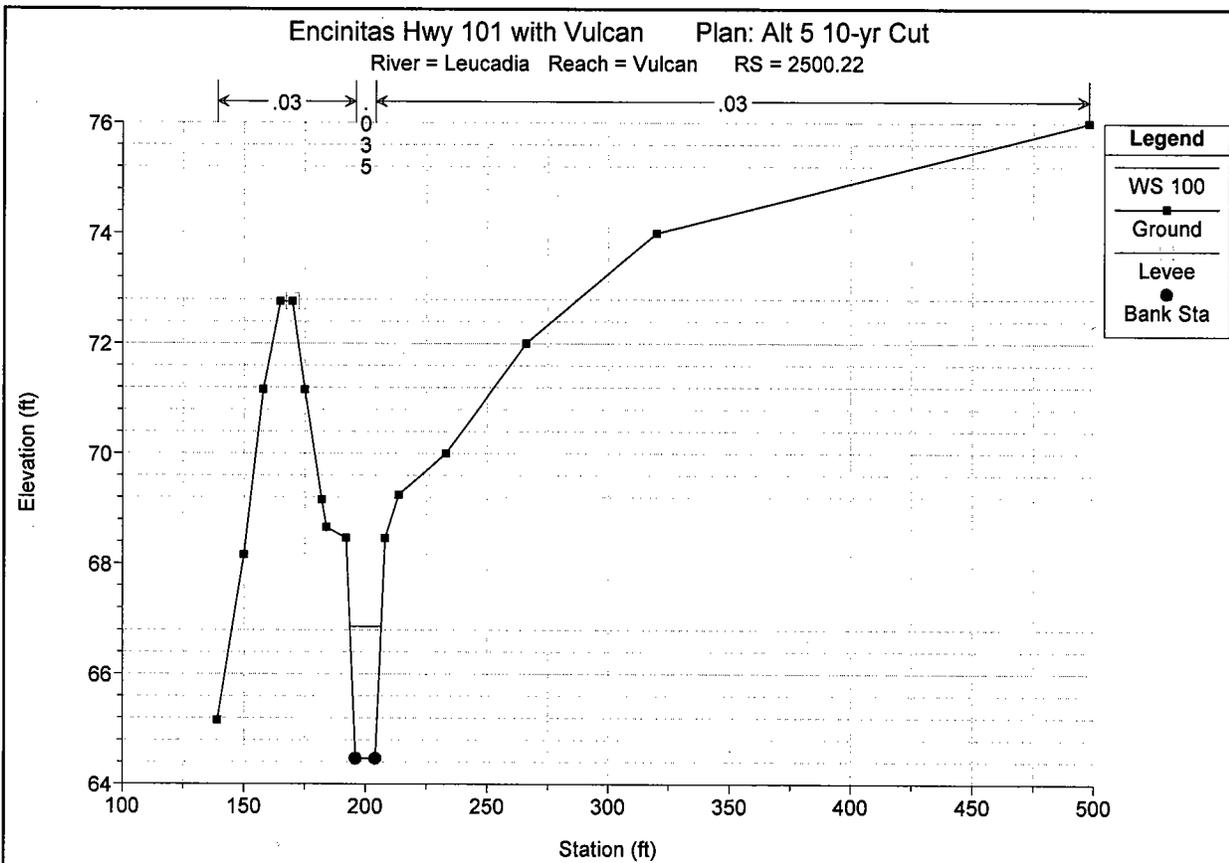


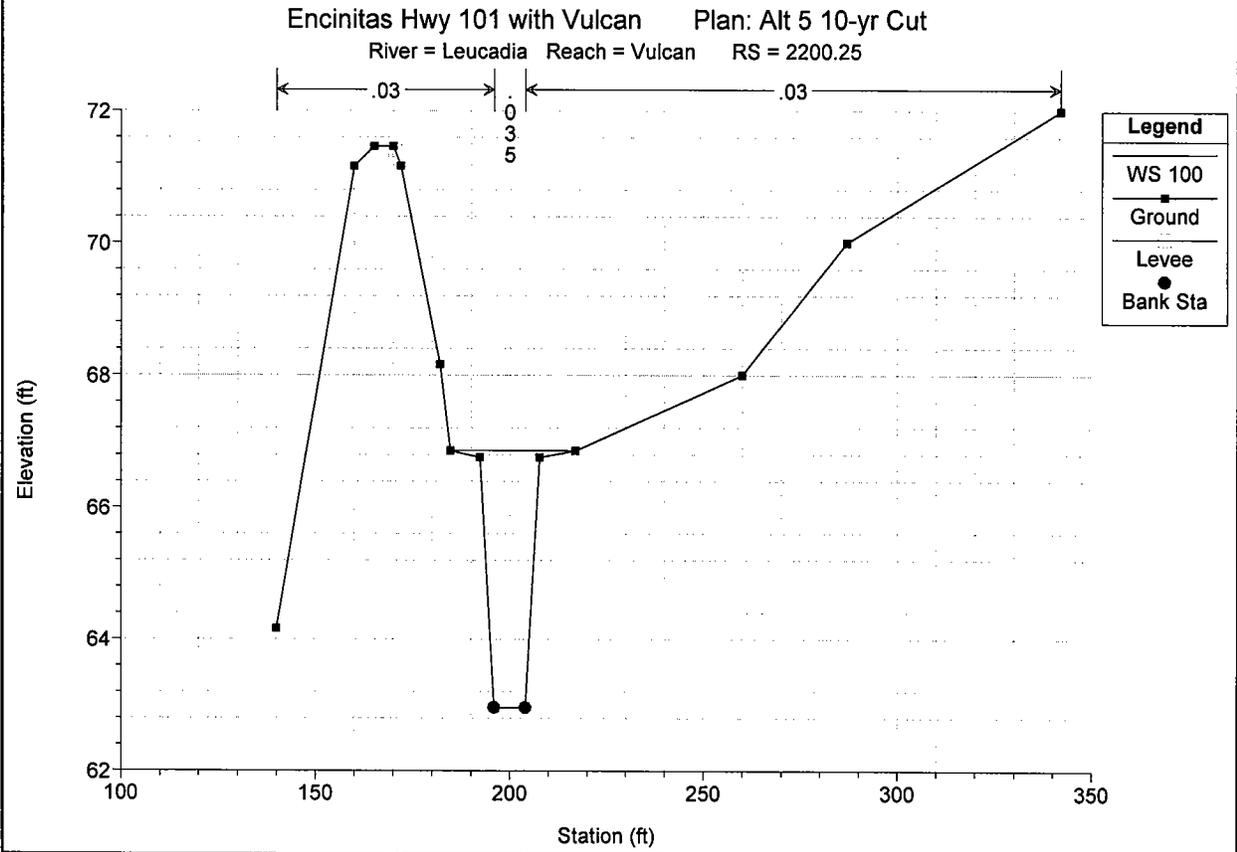
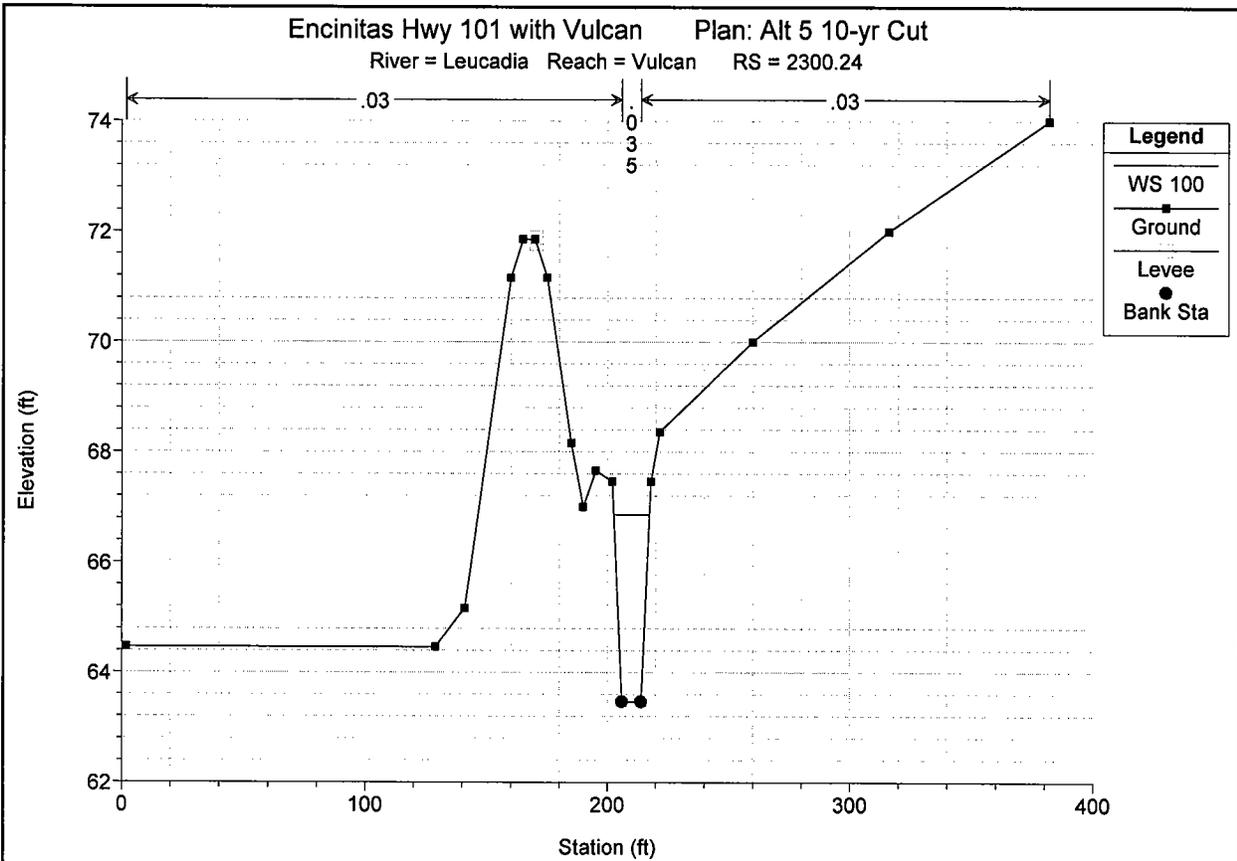






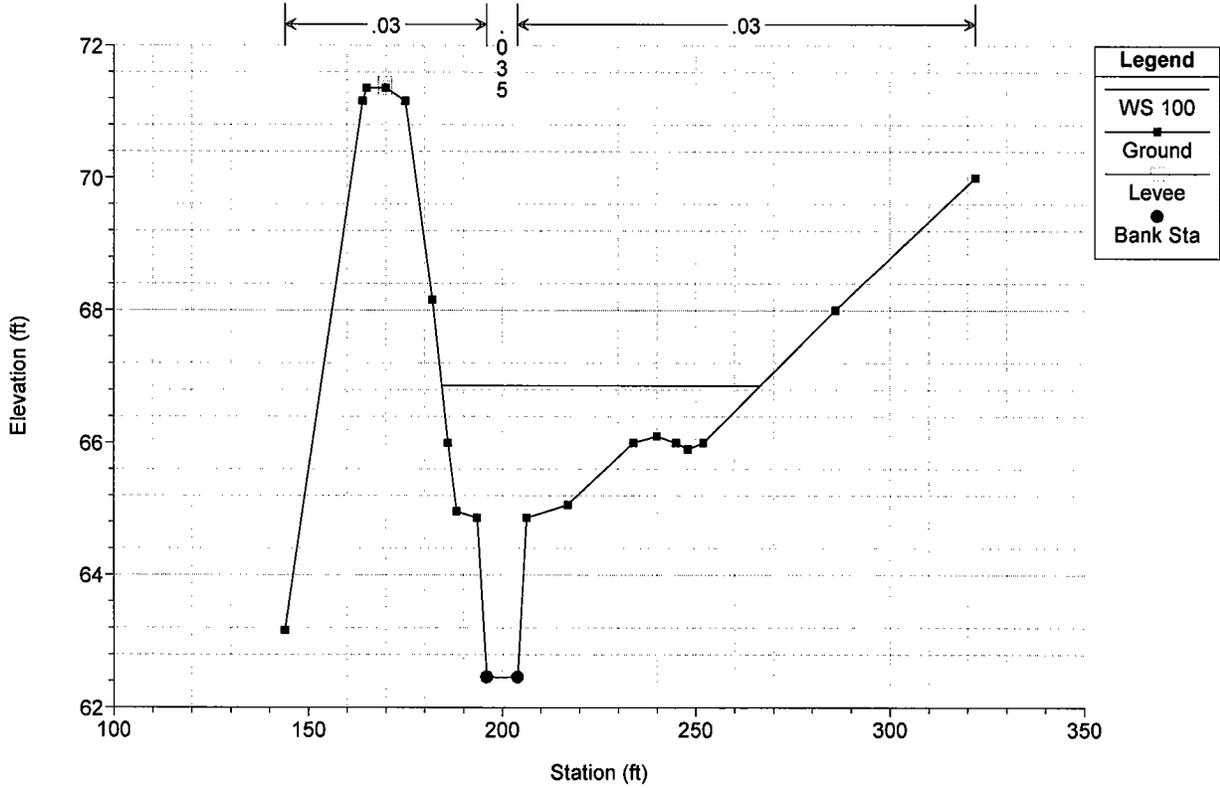






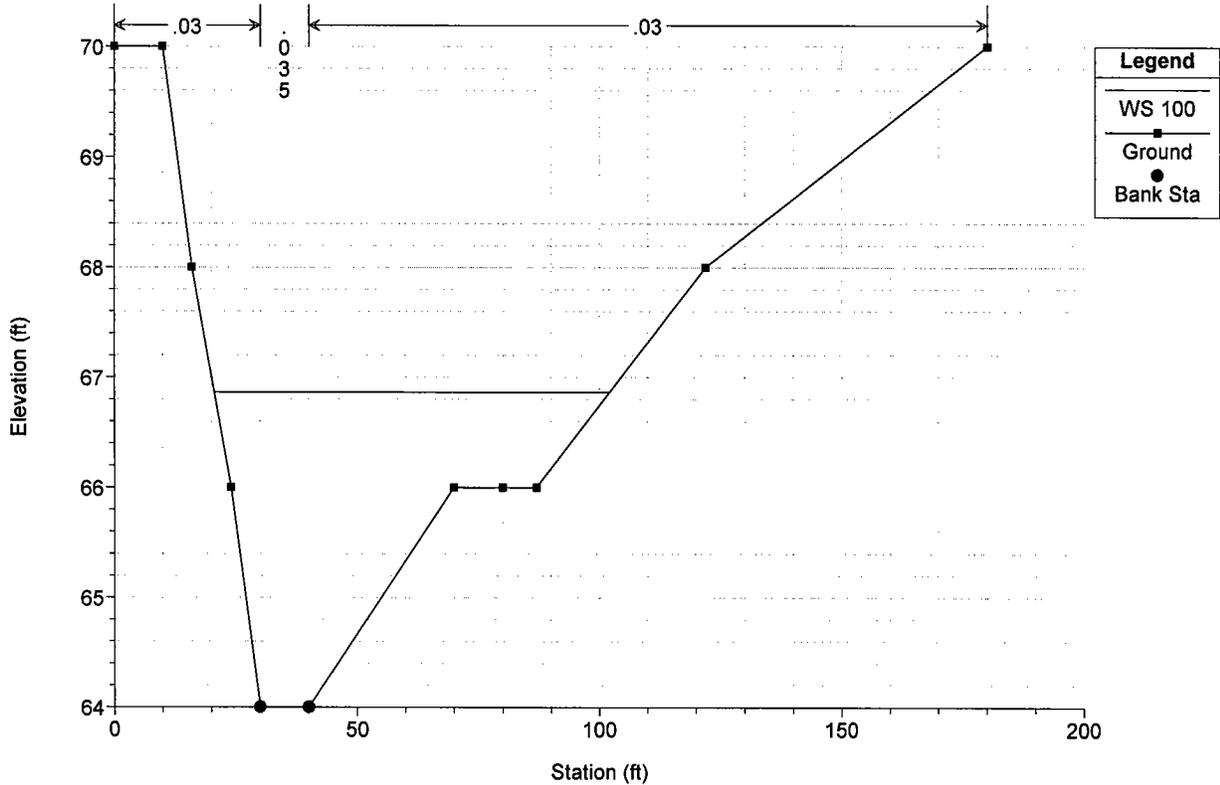
Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut

River = Leucadia Reach = Vulcan RS = 2100.26

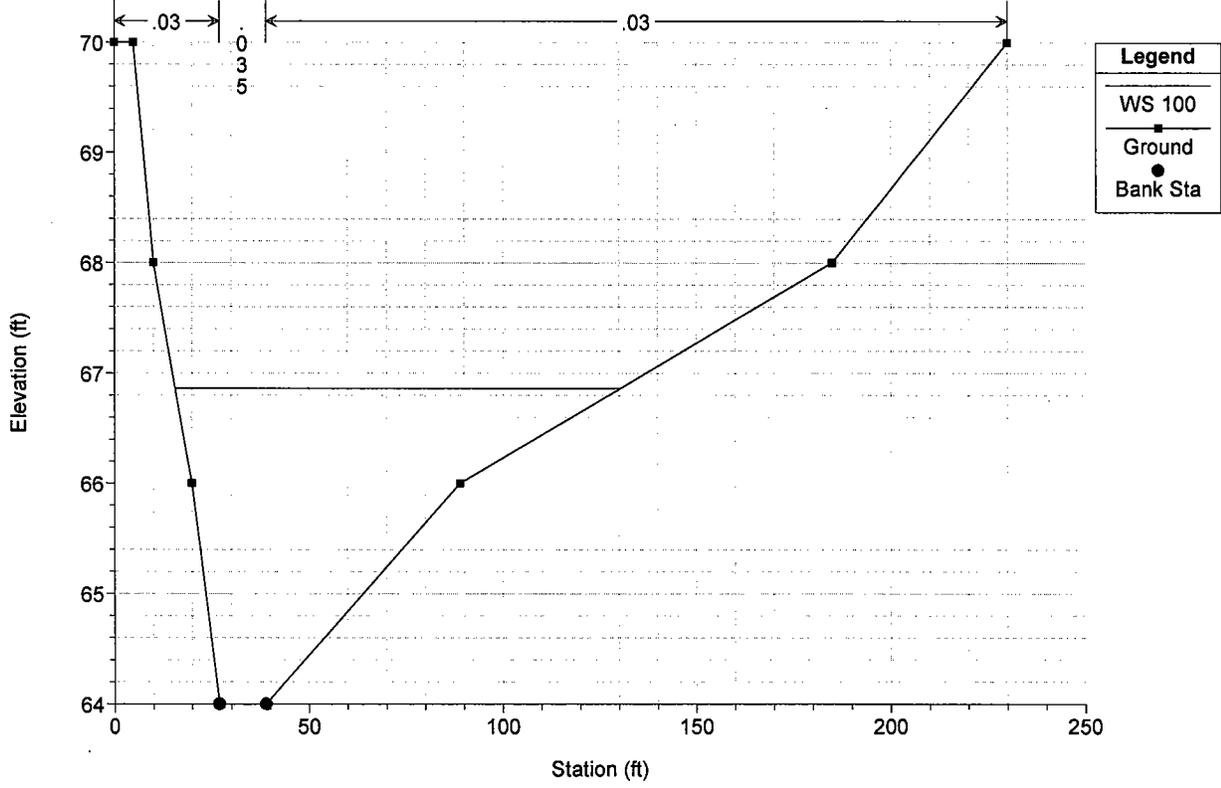


Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut

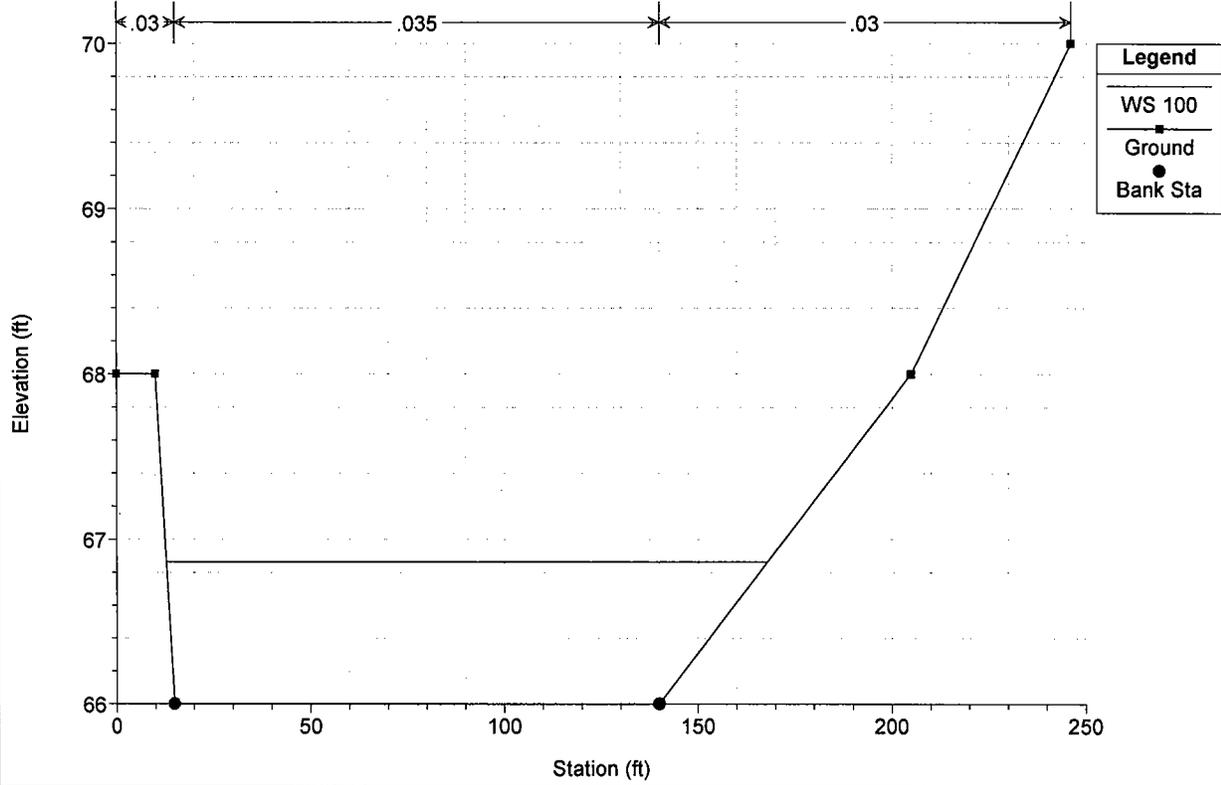
River = Leucadia Reach = Vulcan RS = 245

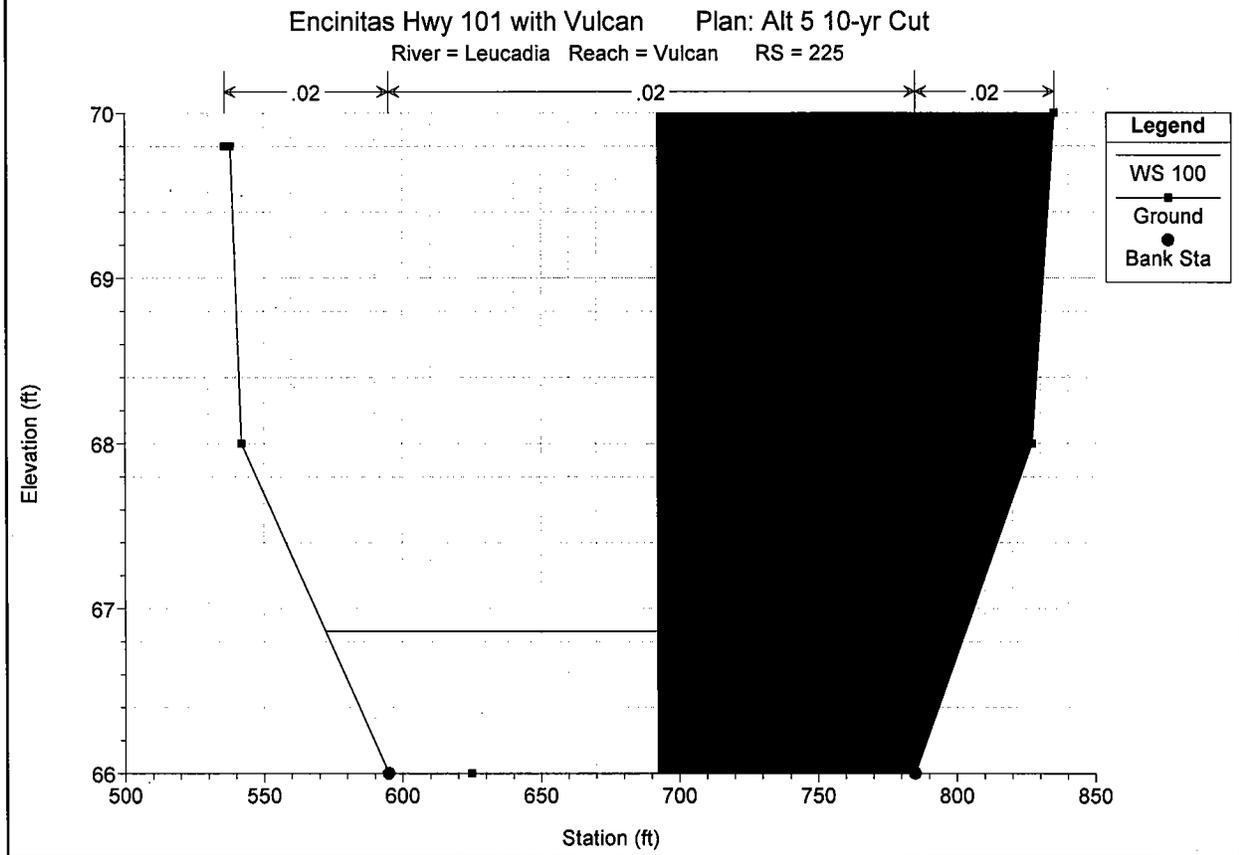
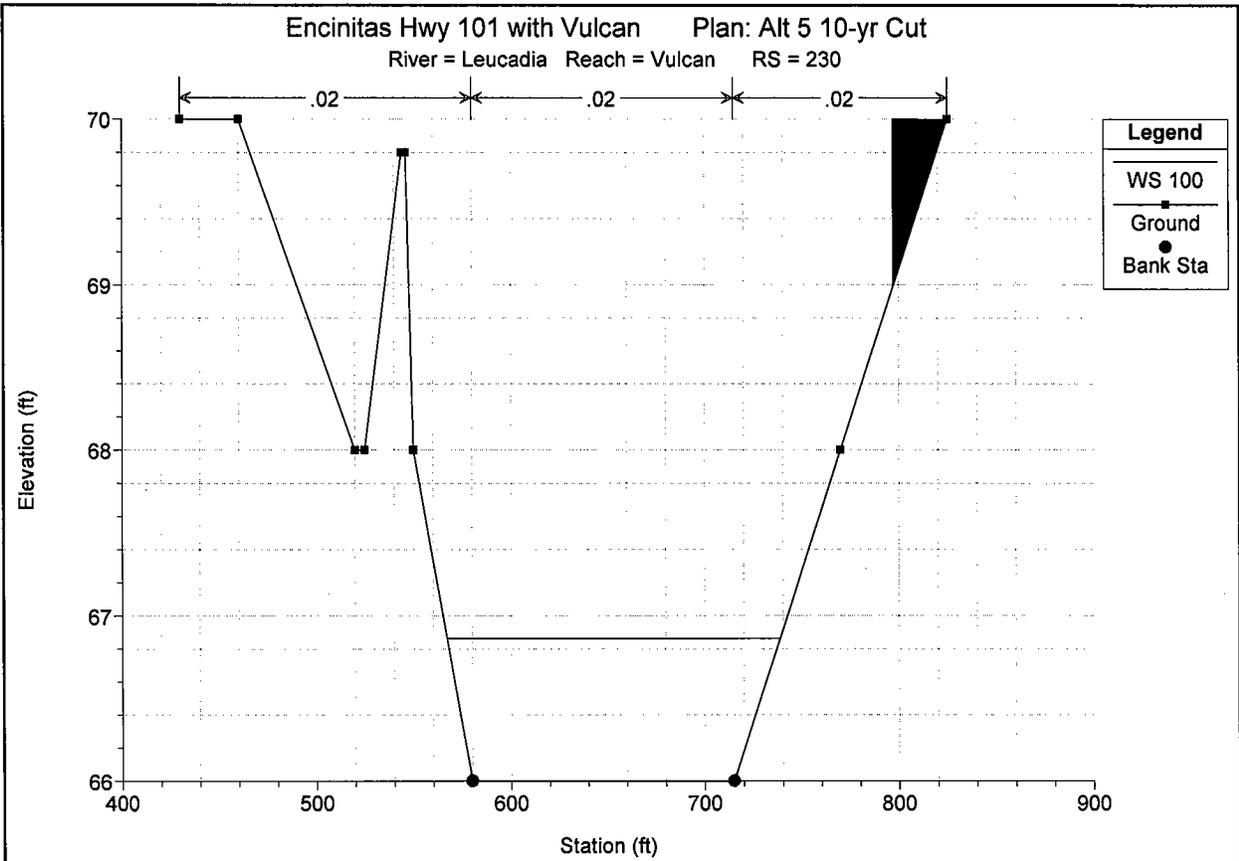


Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut  
 River = Leucadia Reach = Vulcan RS = 240

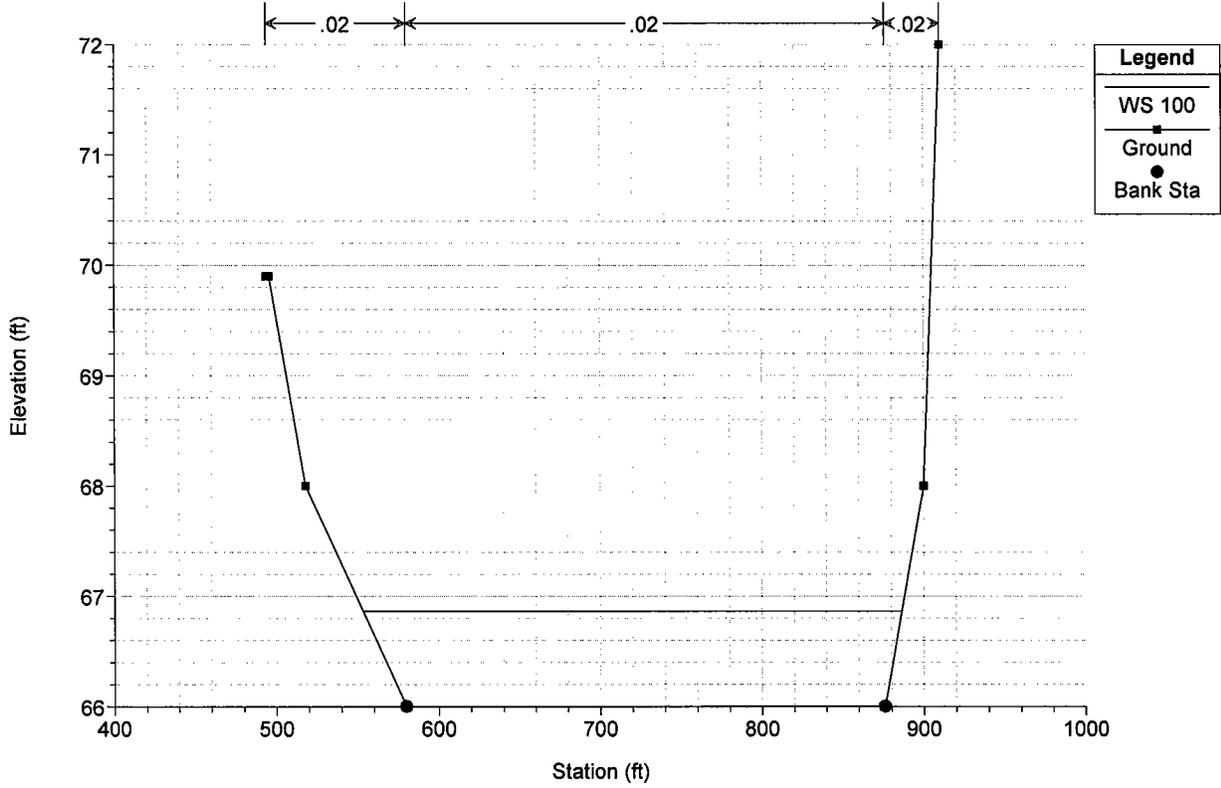


Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut  
 River = Leucadia Reach = Vulcan RS = 235

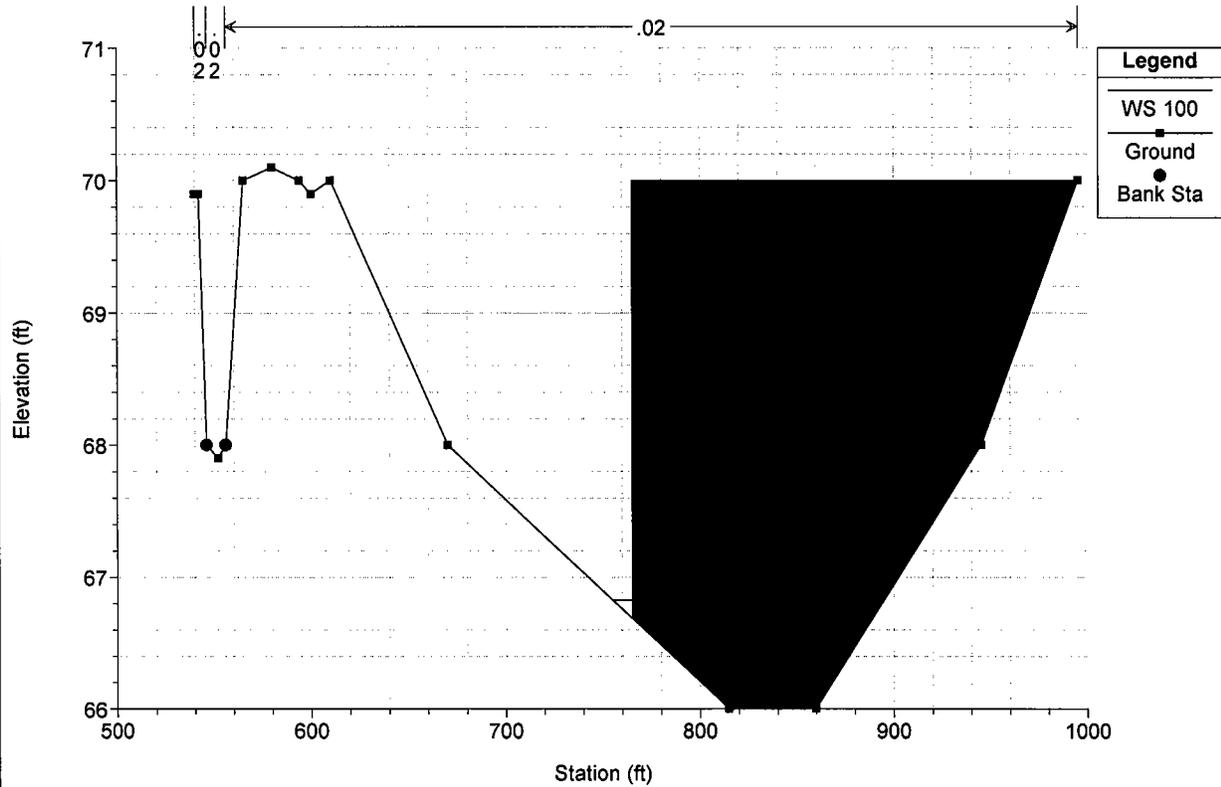


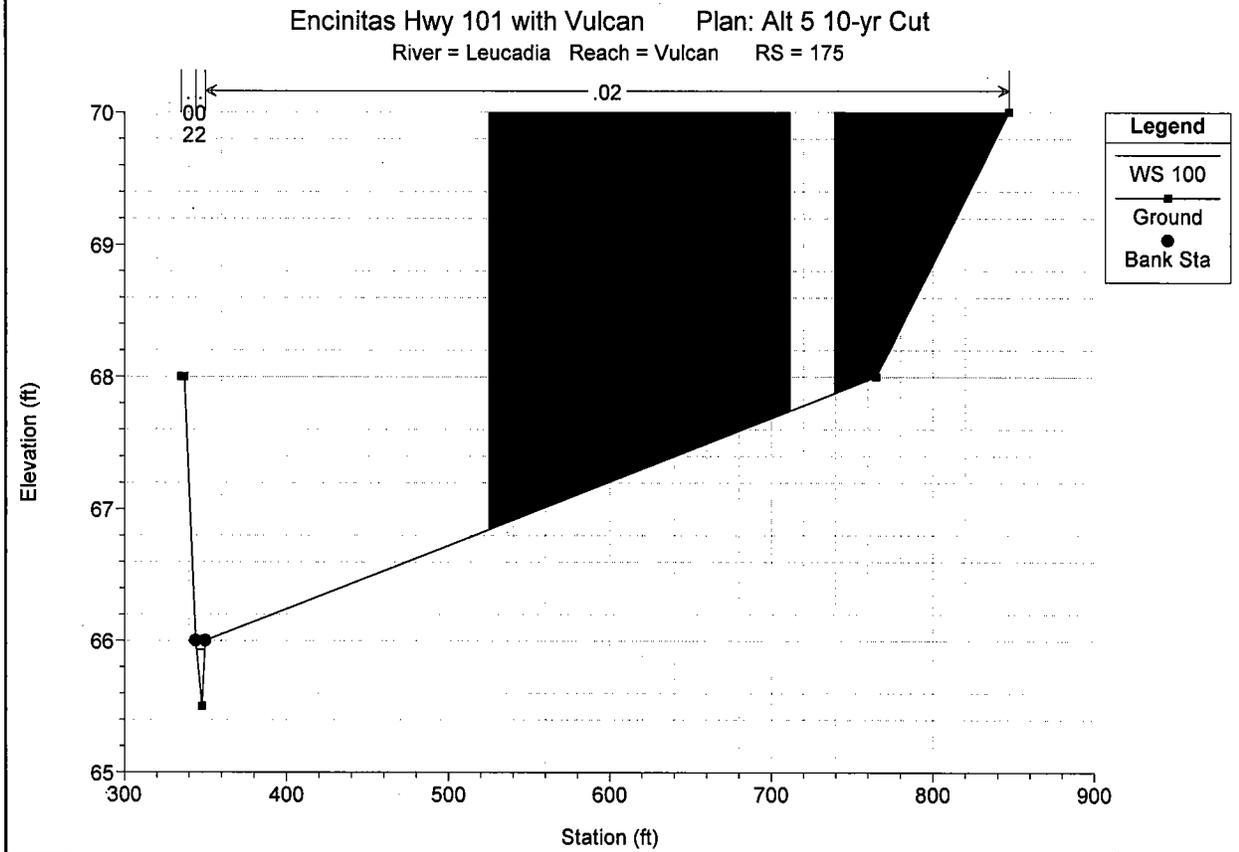
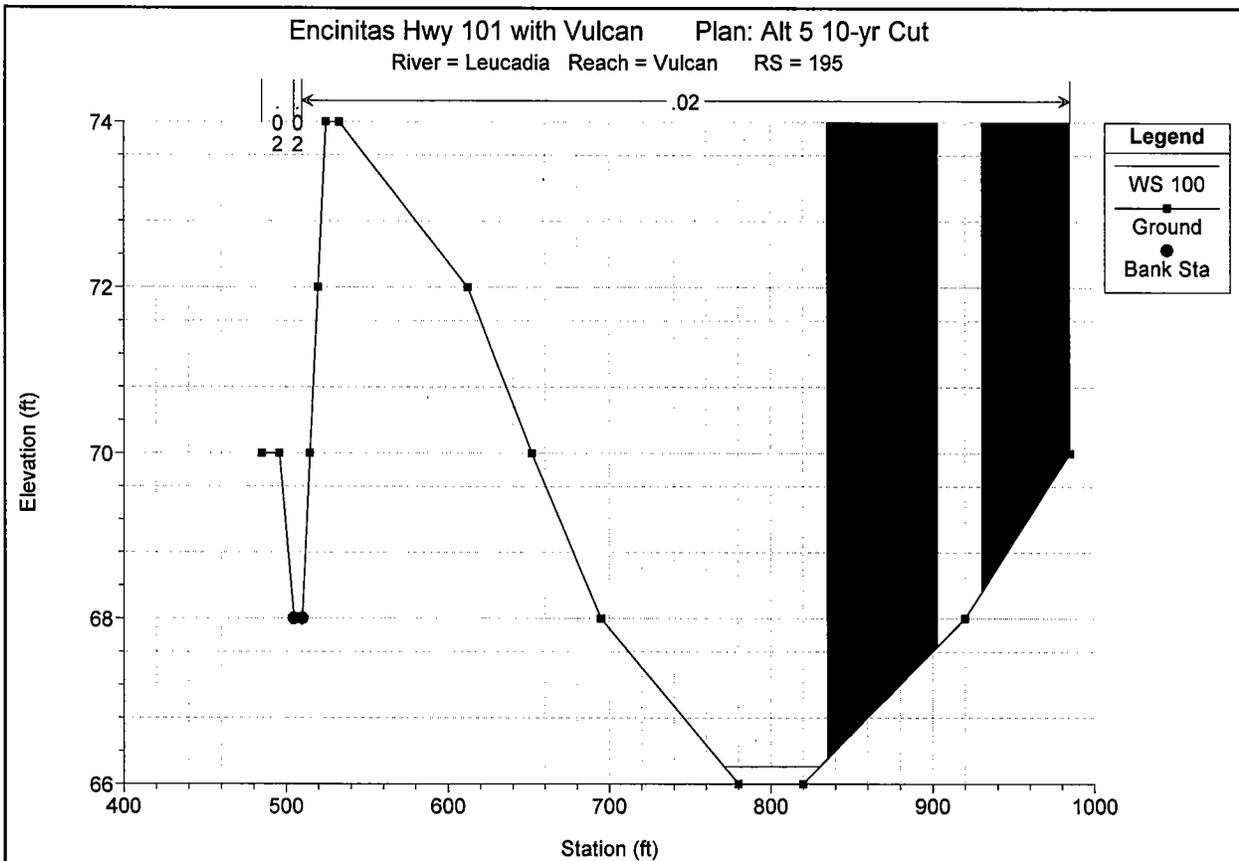


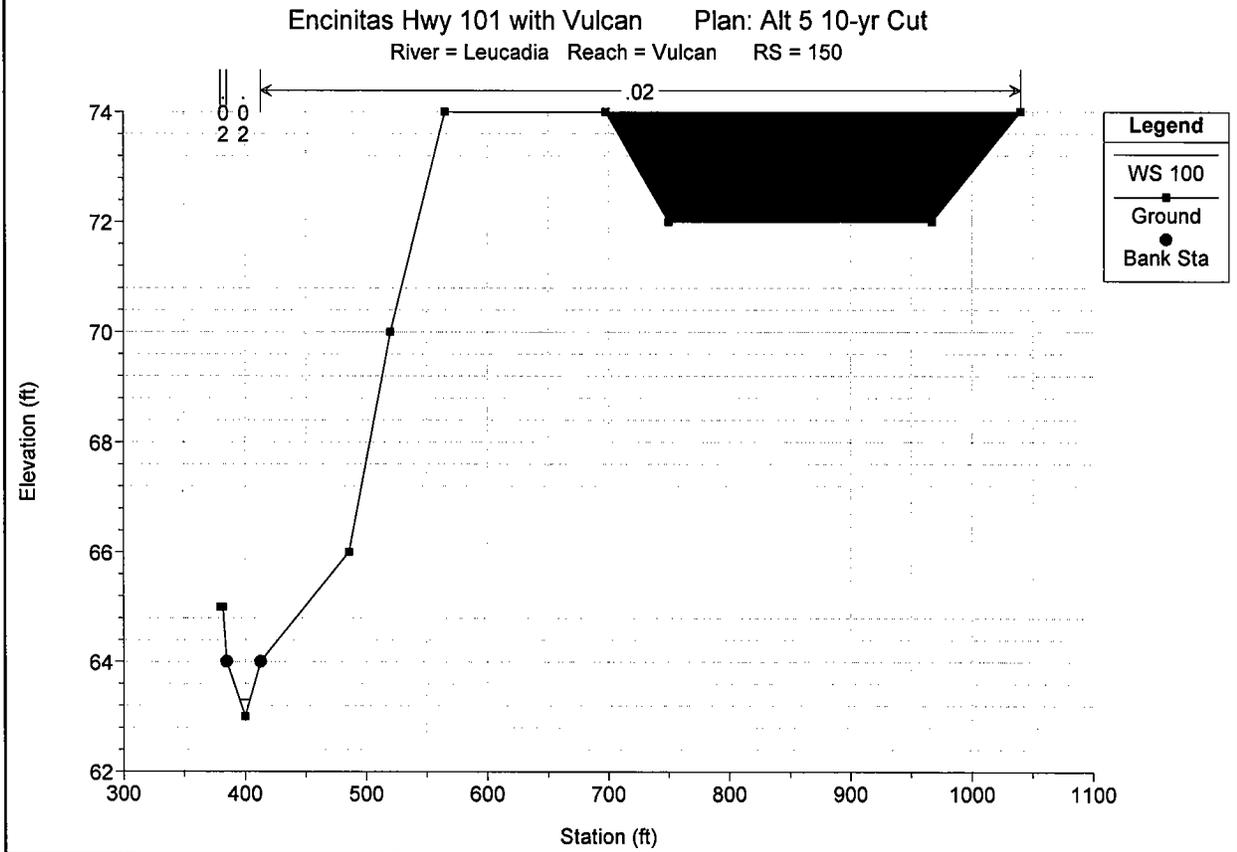
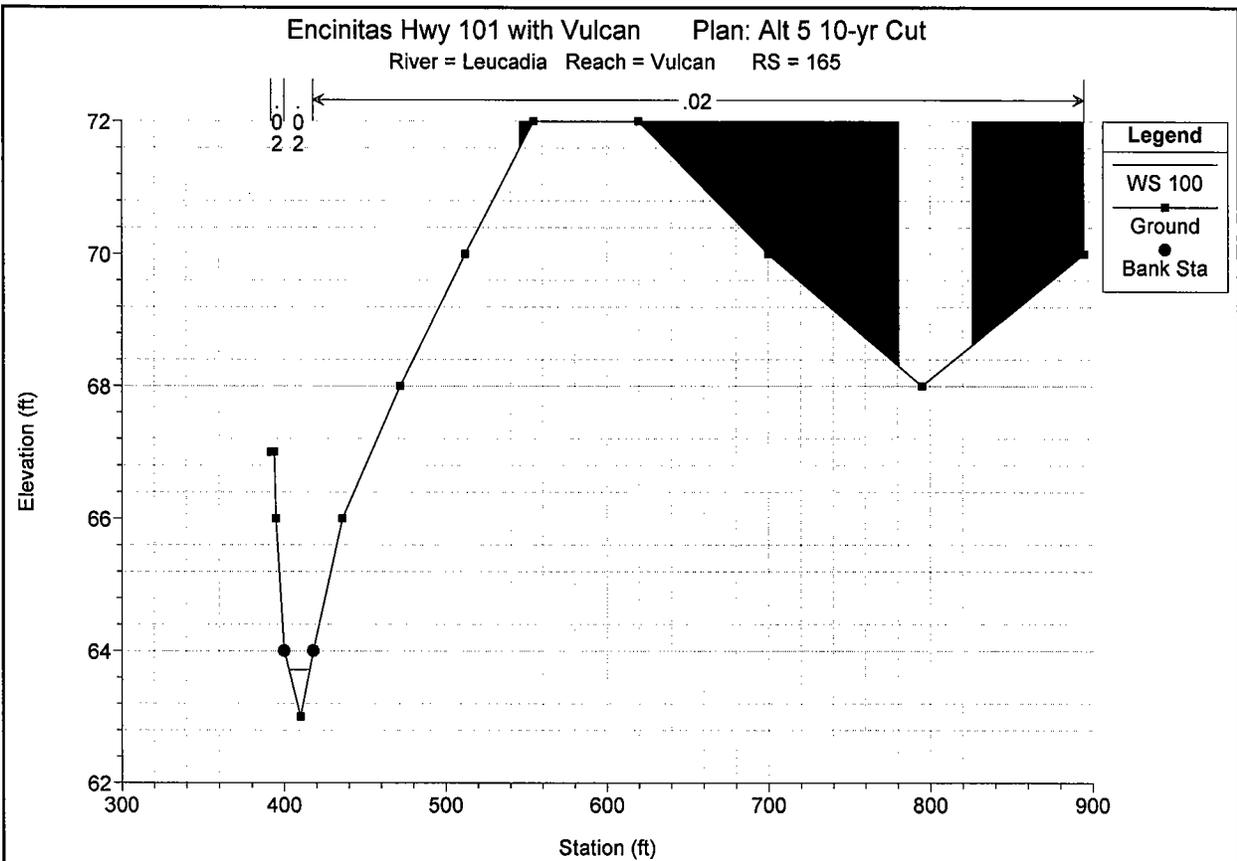
Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut  
 River = Leucadia Reach = Vulcan RS = 220

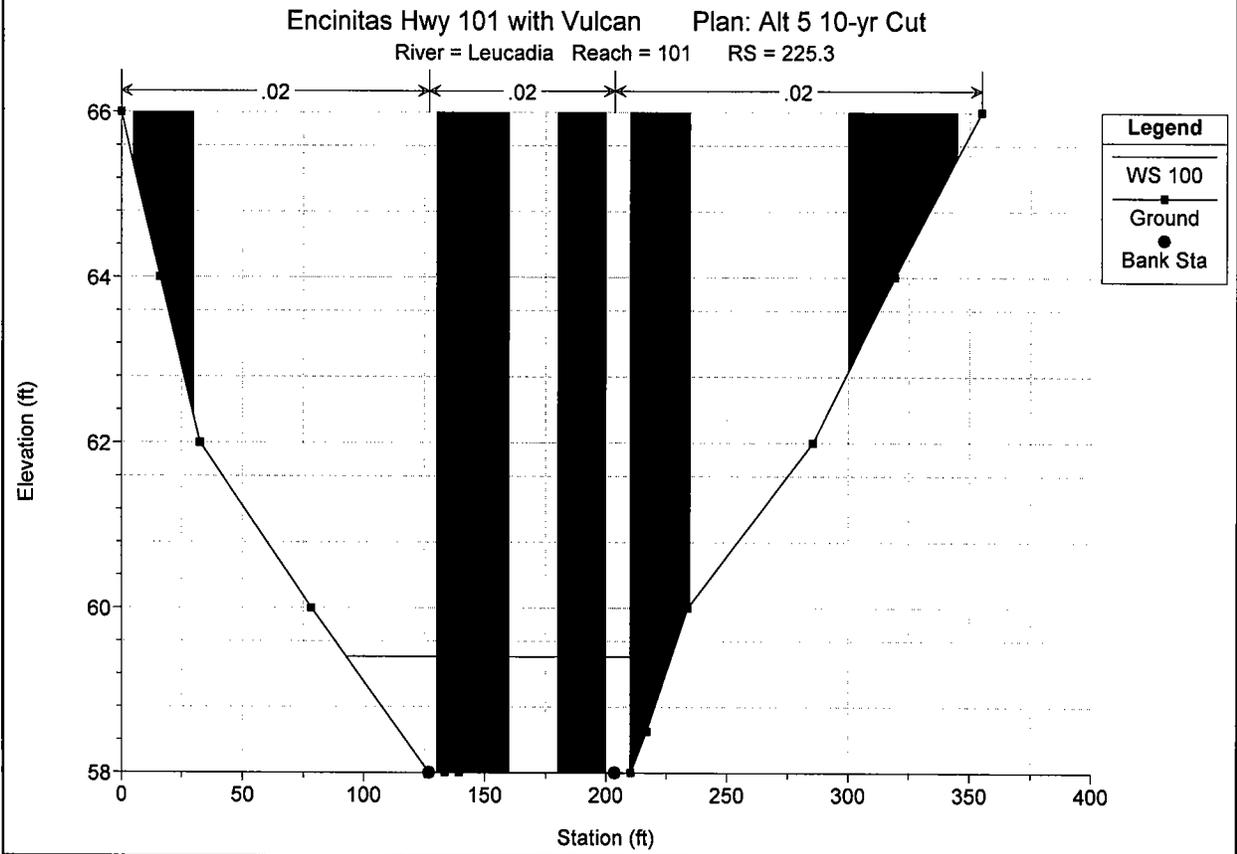
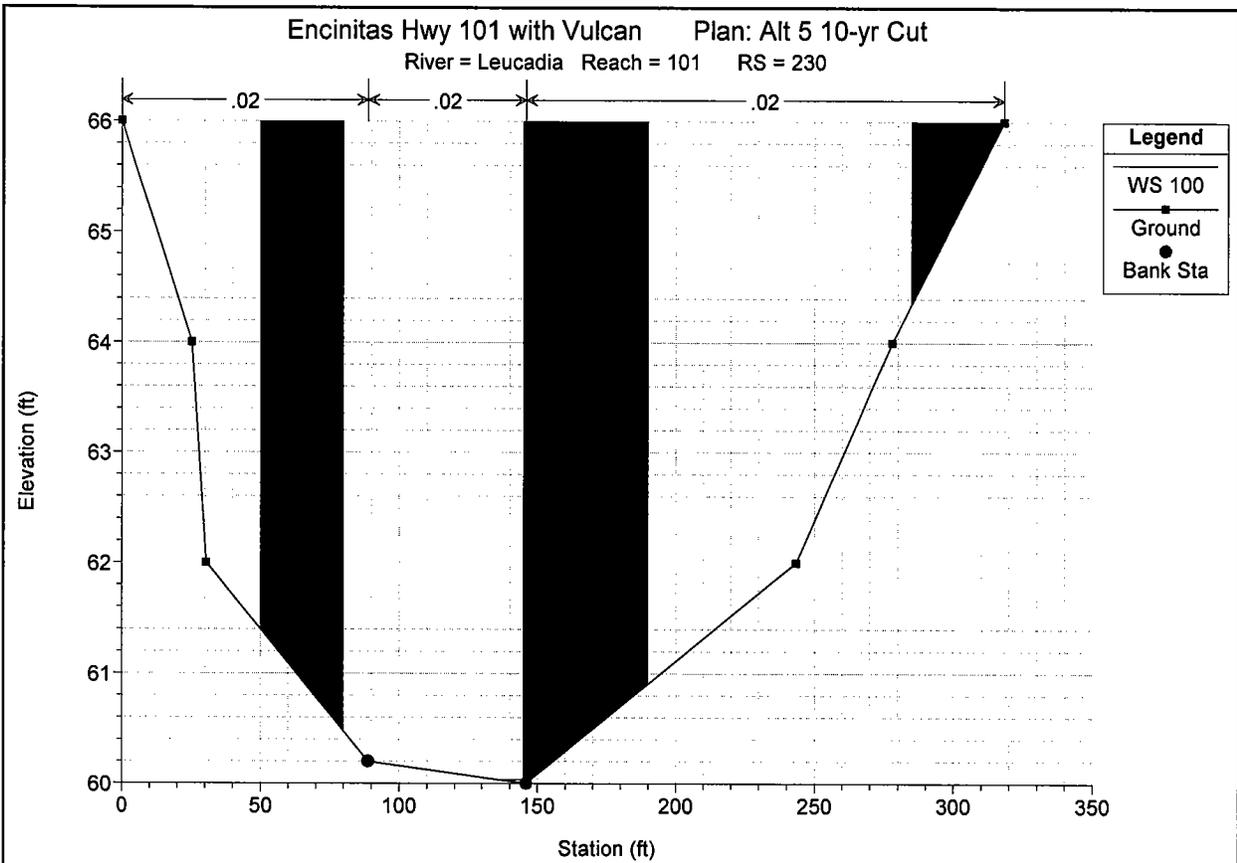


Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut  
 River = Leucadia Reach = Vulcan RS = 215



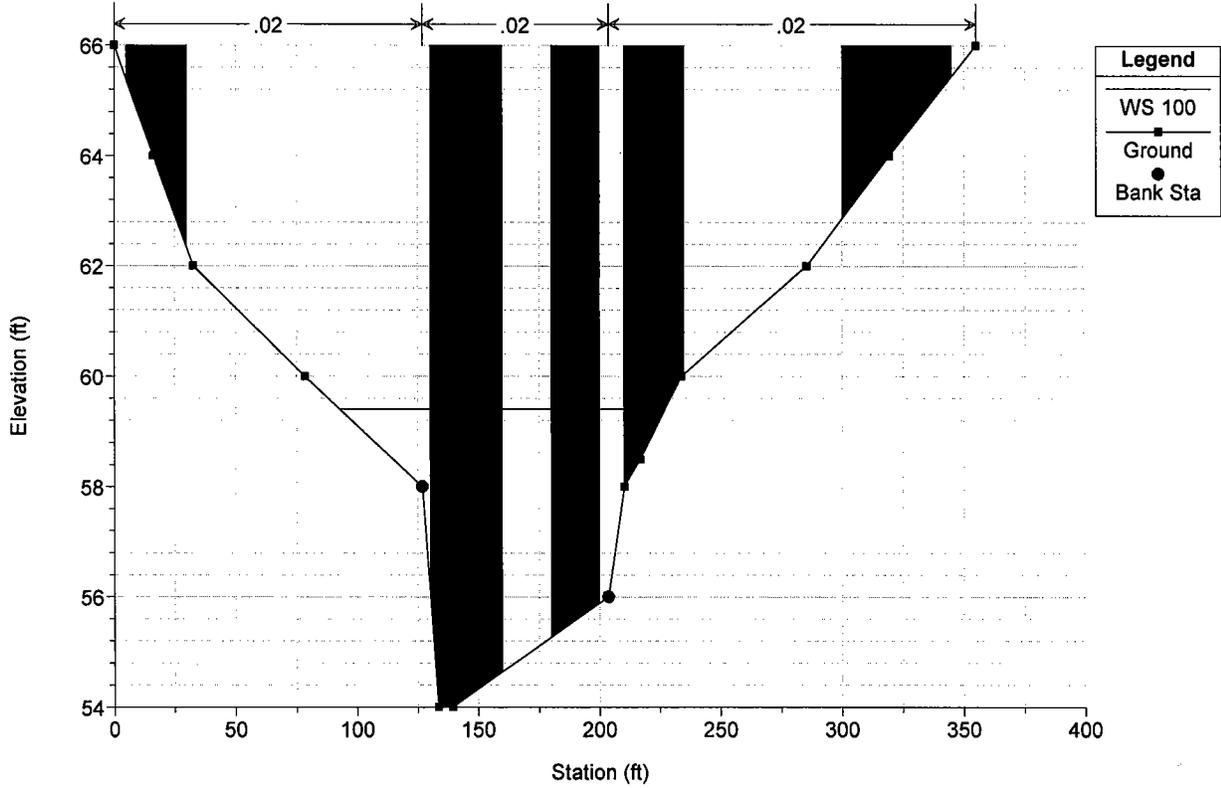






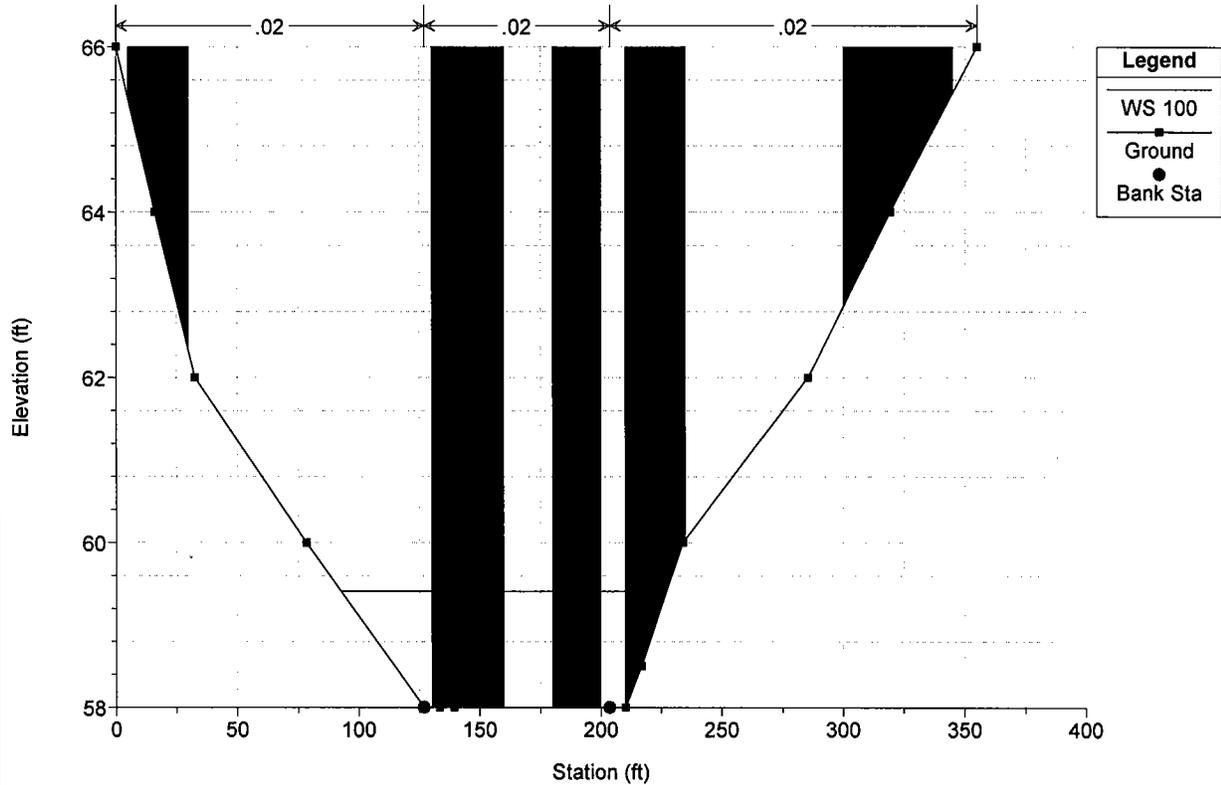
Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut

River = Leucadia Reach = 101 RS = 225.2



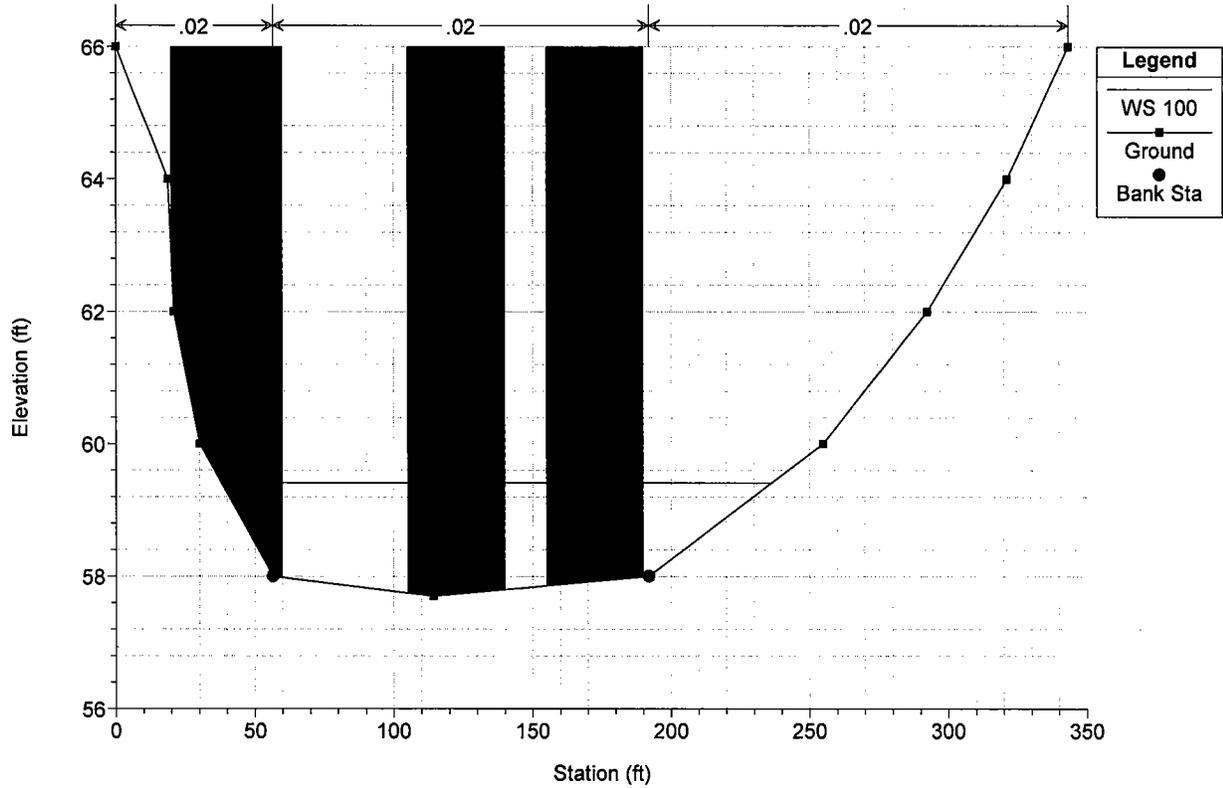
Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut

River = Leucadia Reach = 101 RS = 225.1



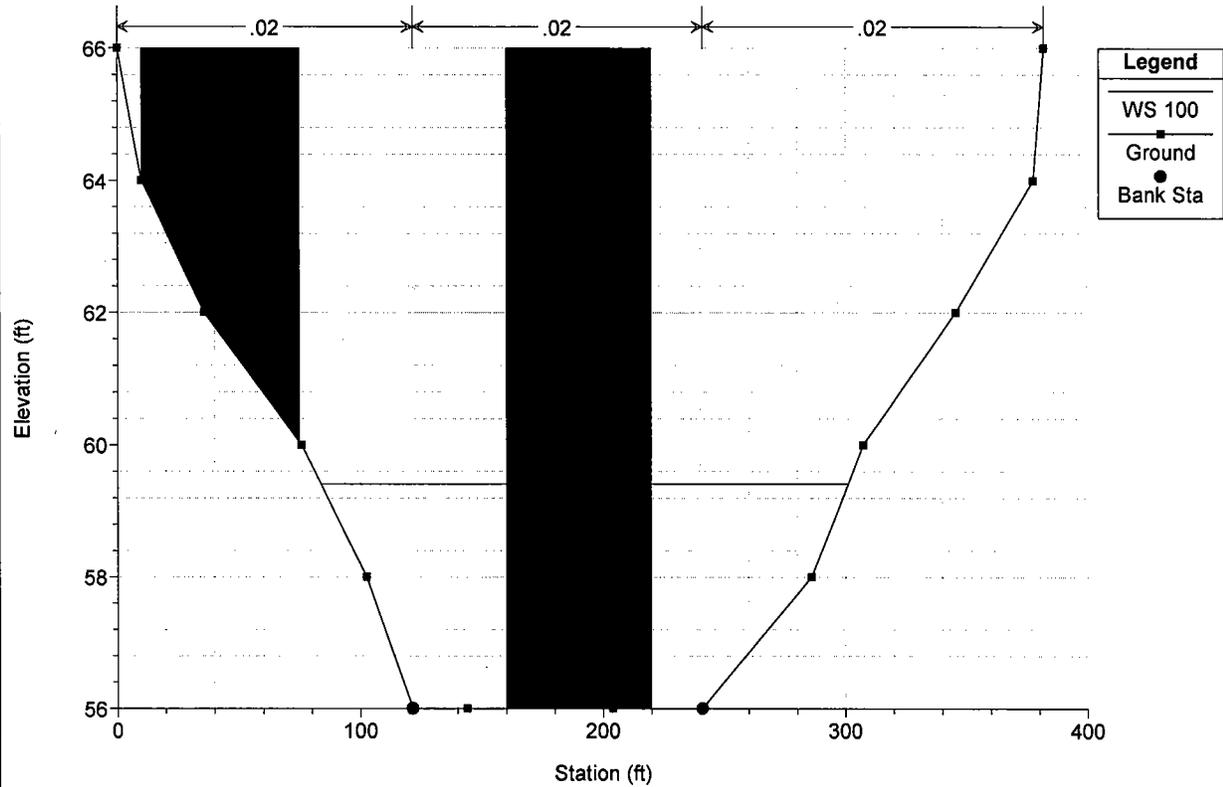
Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut

River = Leucadia Reach = 101 RS = 220

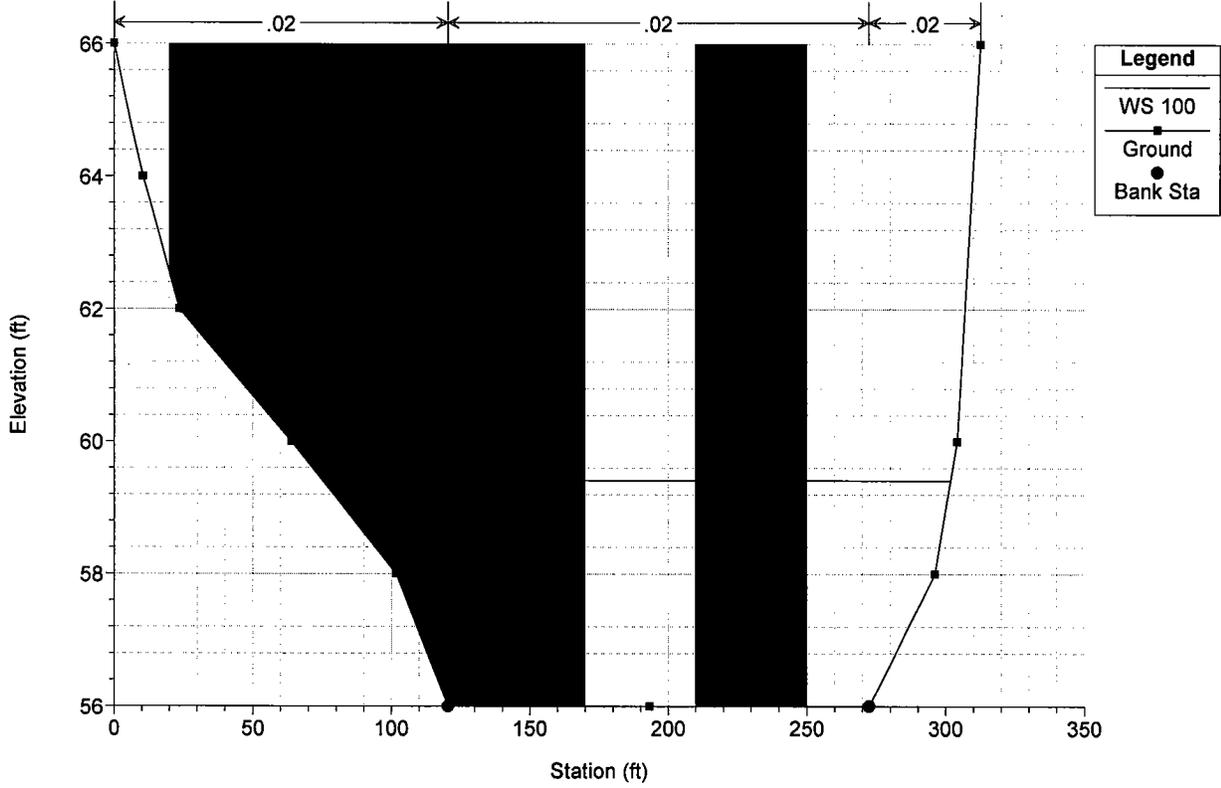


Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut

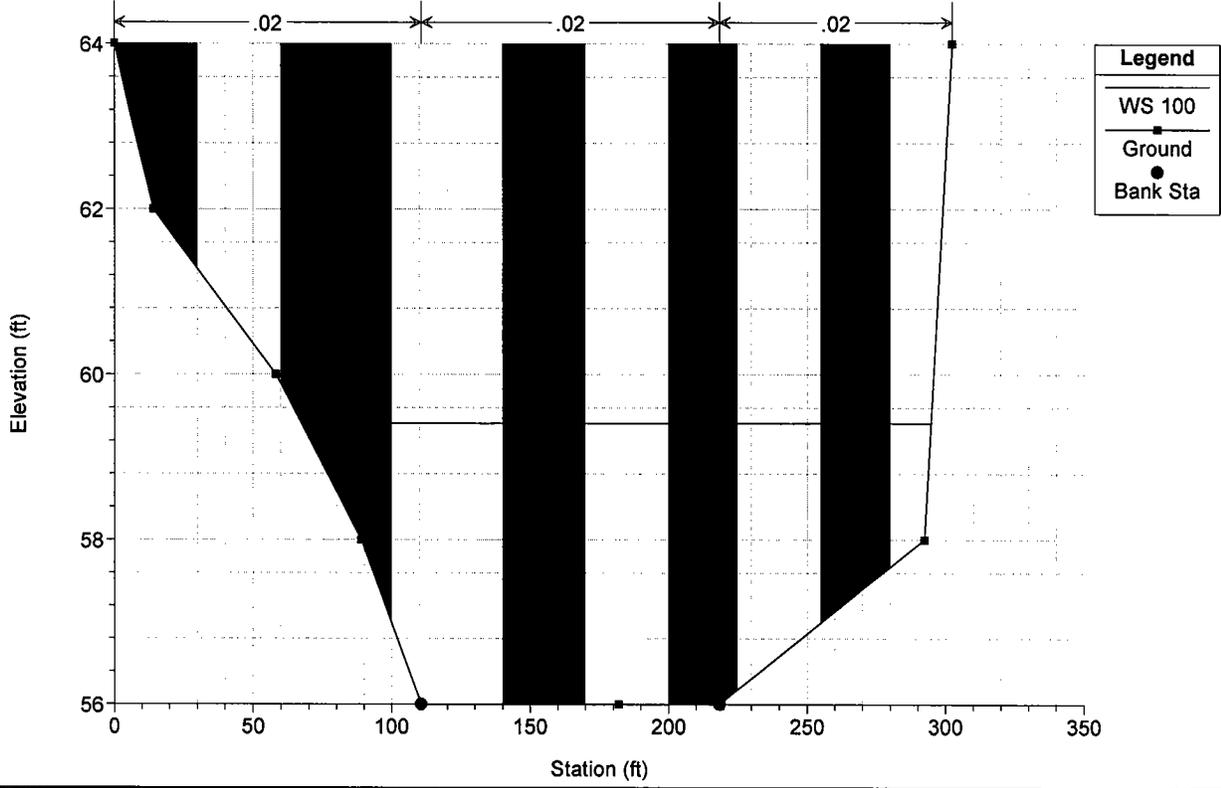
River = Leucadia Reach = 101 RS = 215



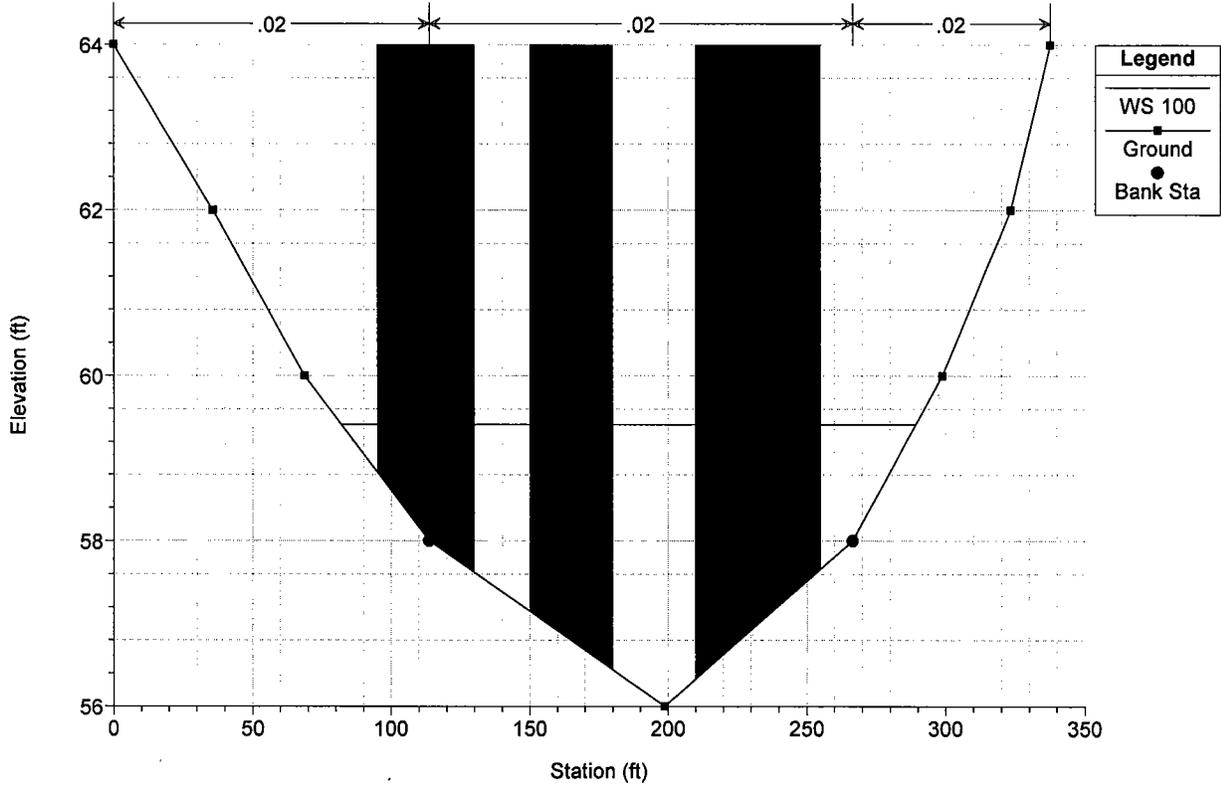
Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut  
 River = Leucadia Reach = 101 RS = 210



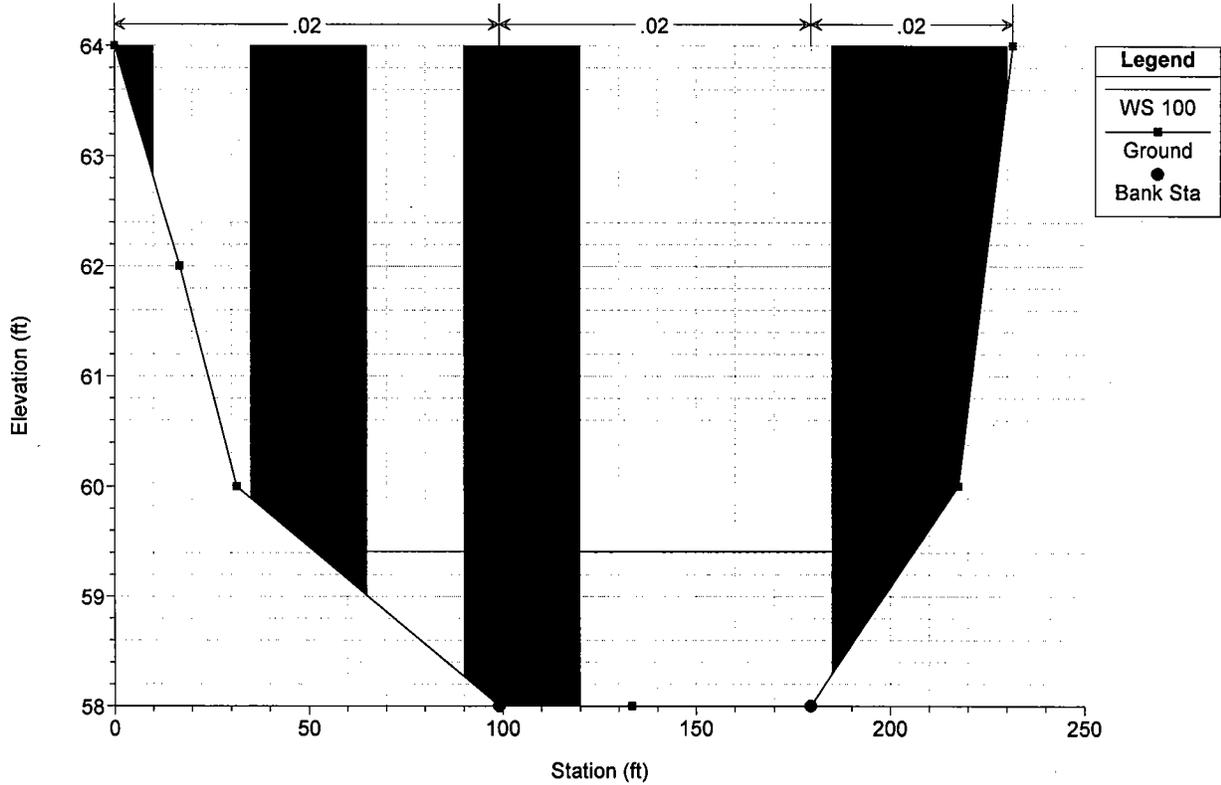
Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut  
 River = Leucadia Reach = 101 RS = 205



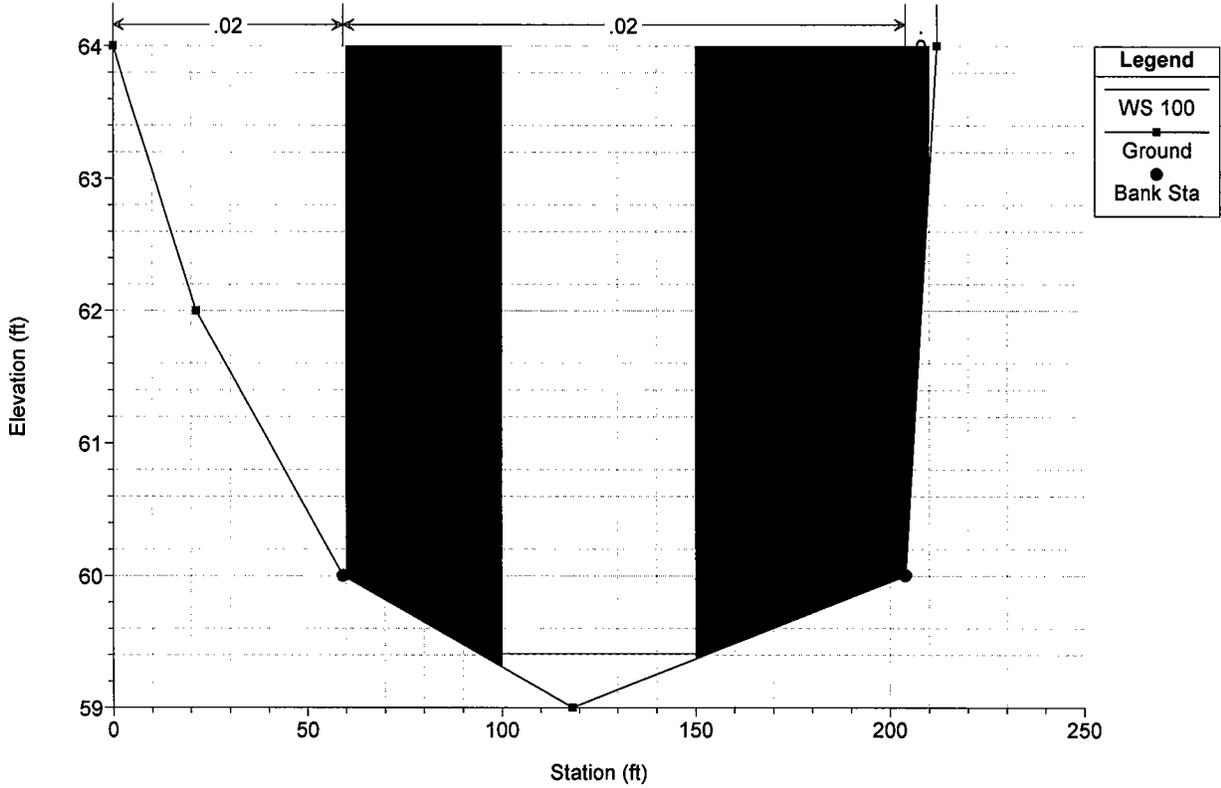
Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut  
 River = Leucadia Reach = 101 RS = 195



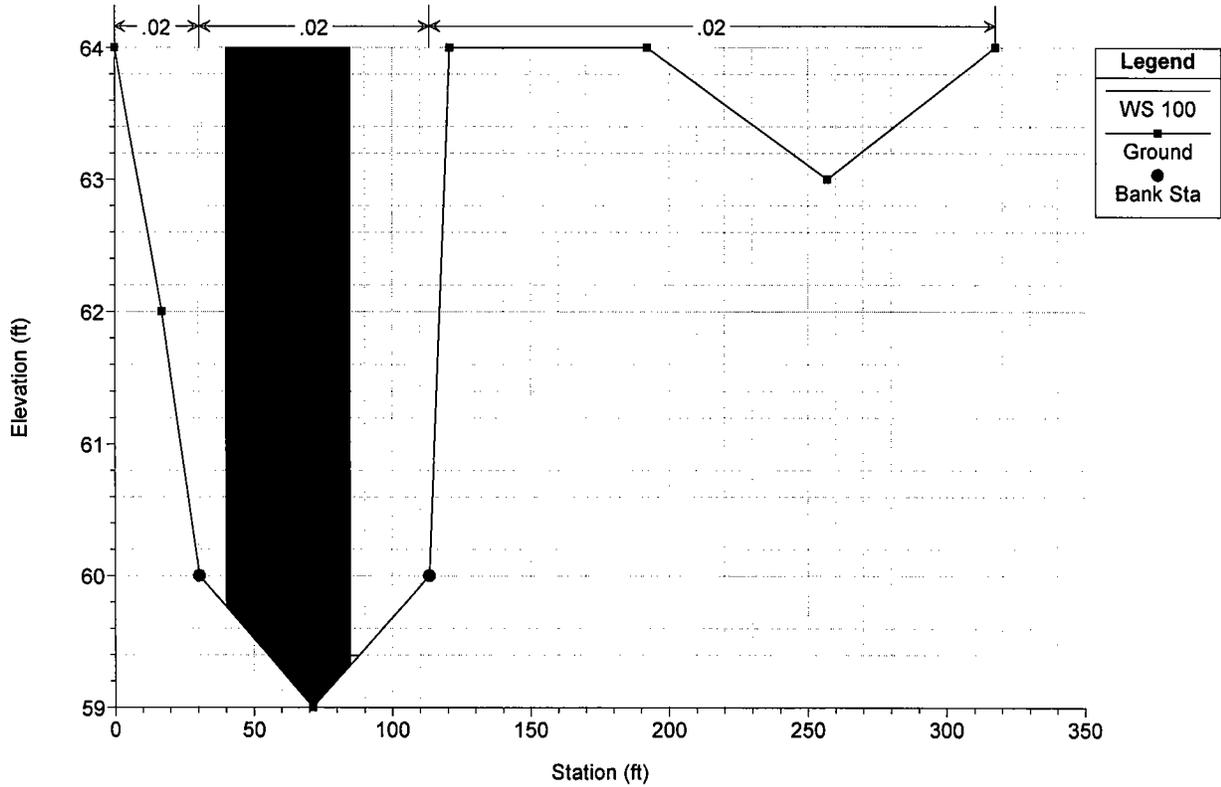
Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut  
 River = Leucadia Reach = 101 RS = 190



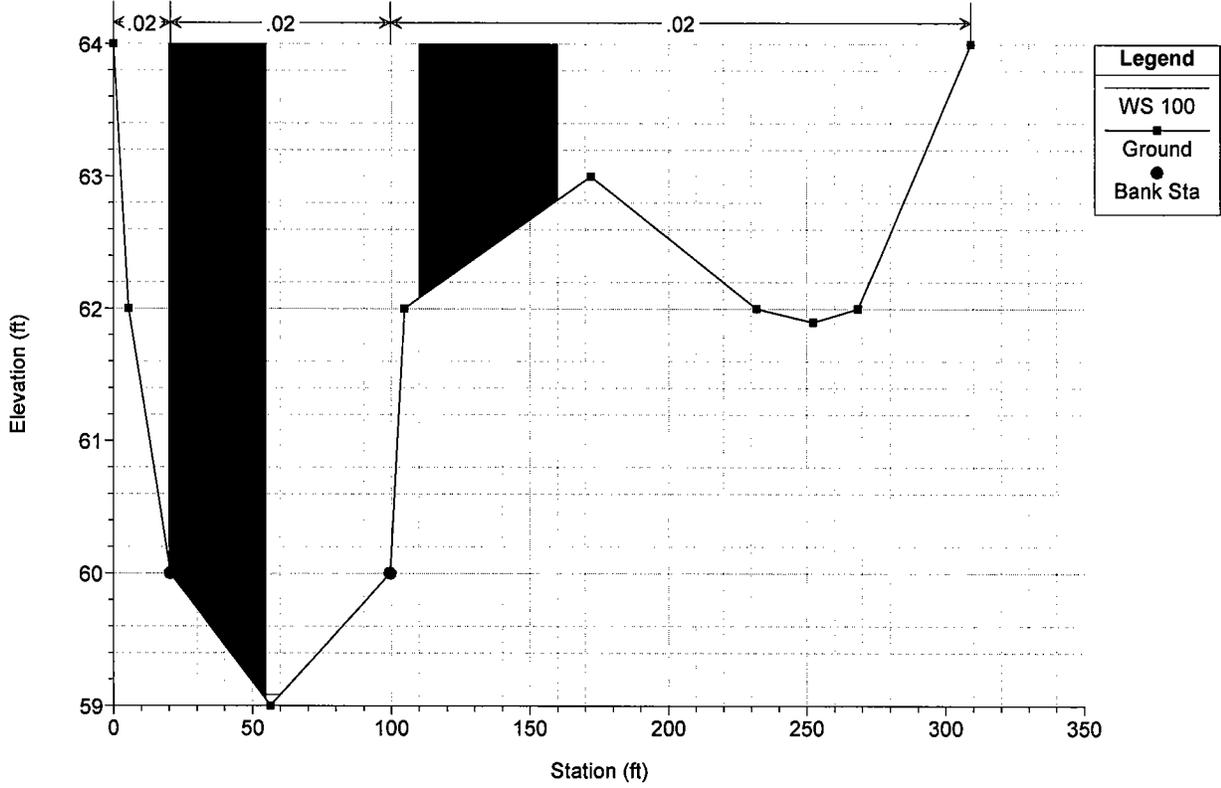
Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut  
 River = Leucadia Reach = 101 RS = 185



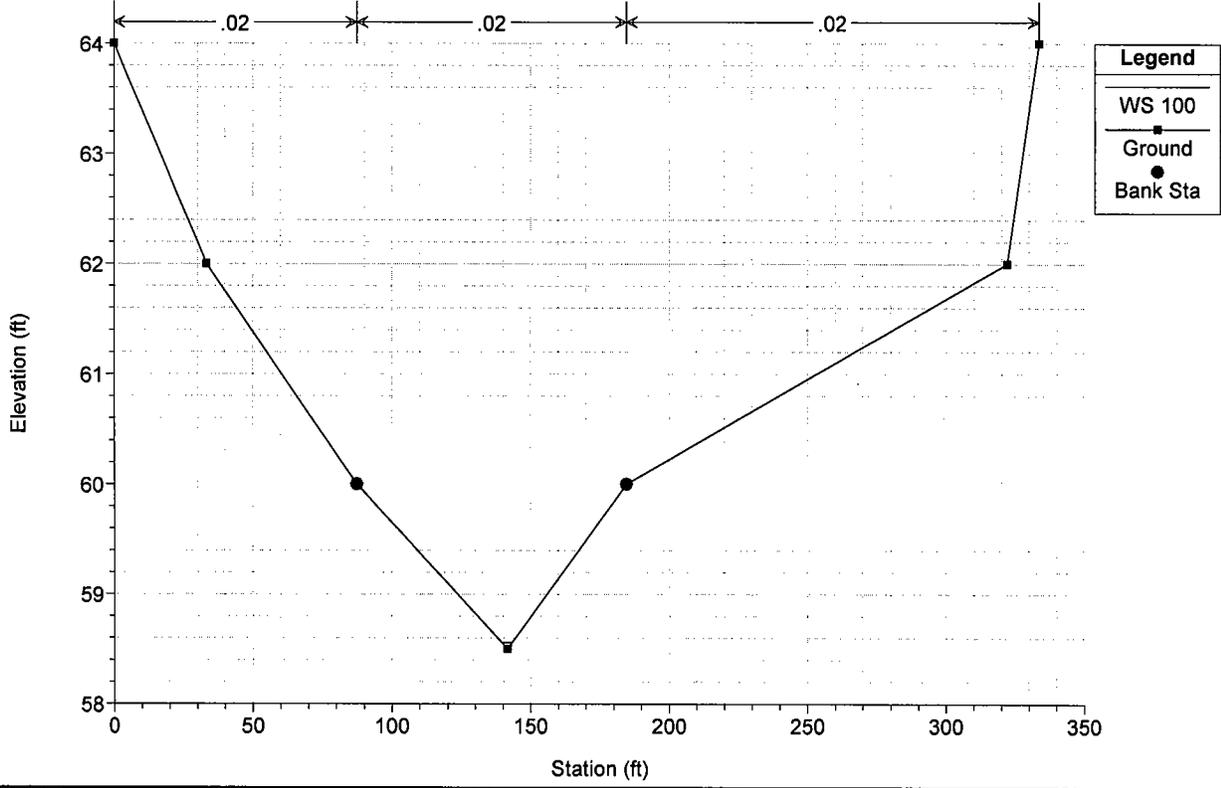
Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut  
 River = Leucadia Reach = 101 RS = 180

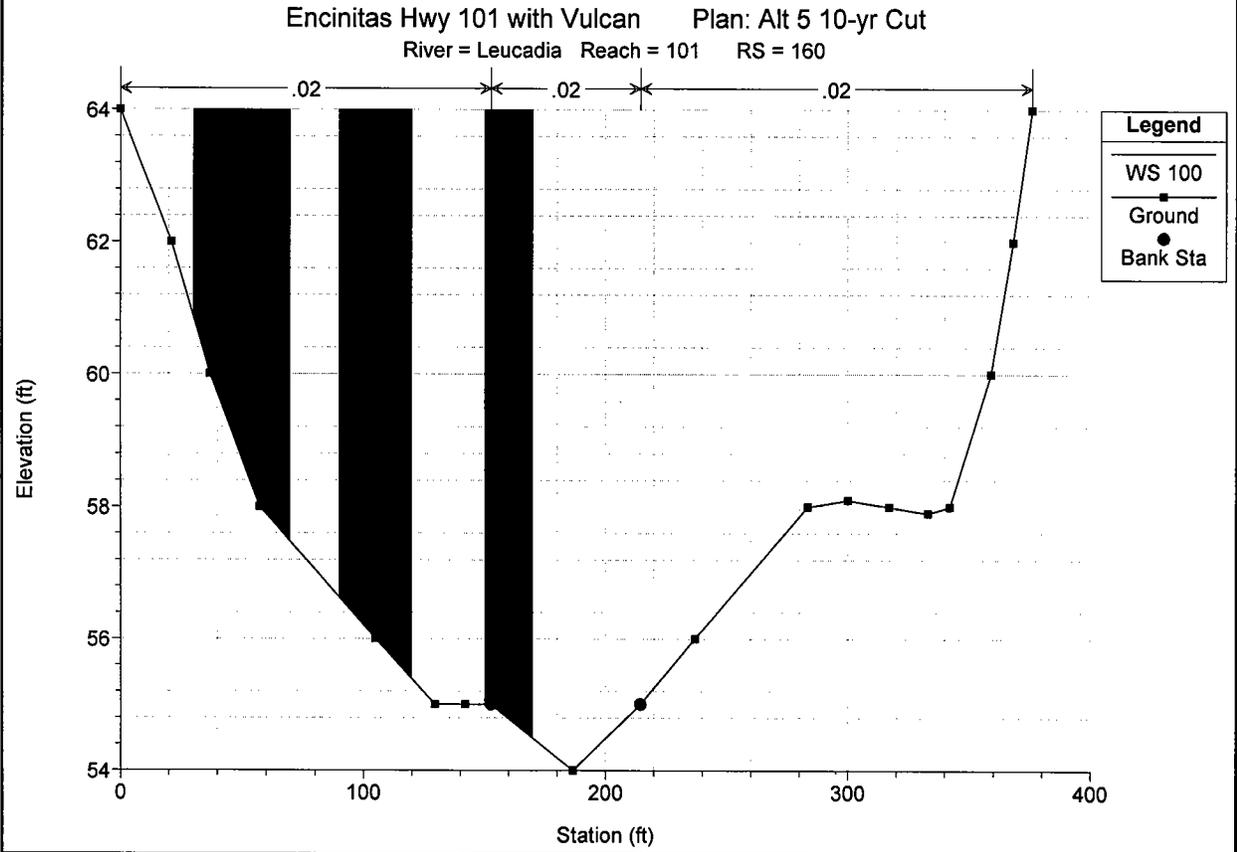
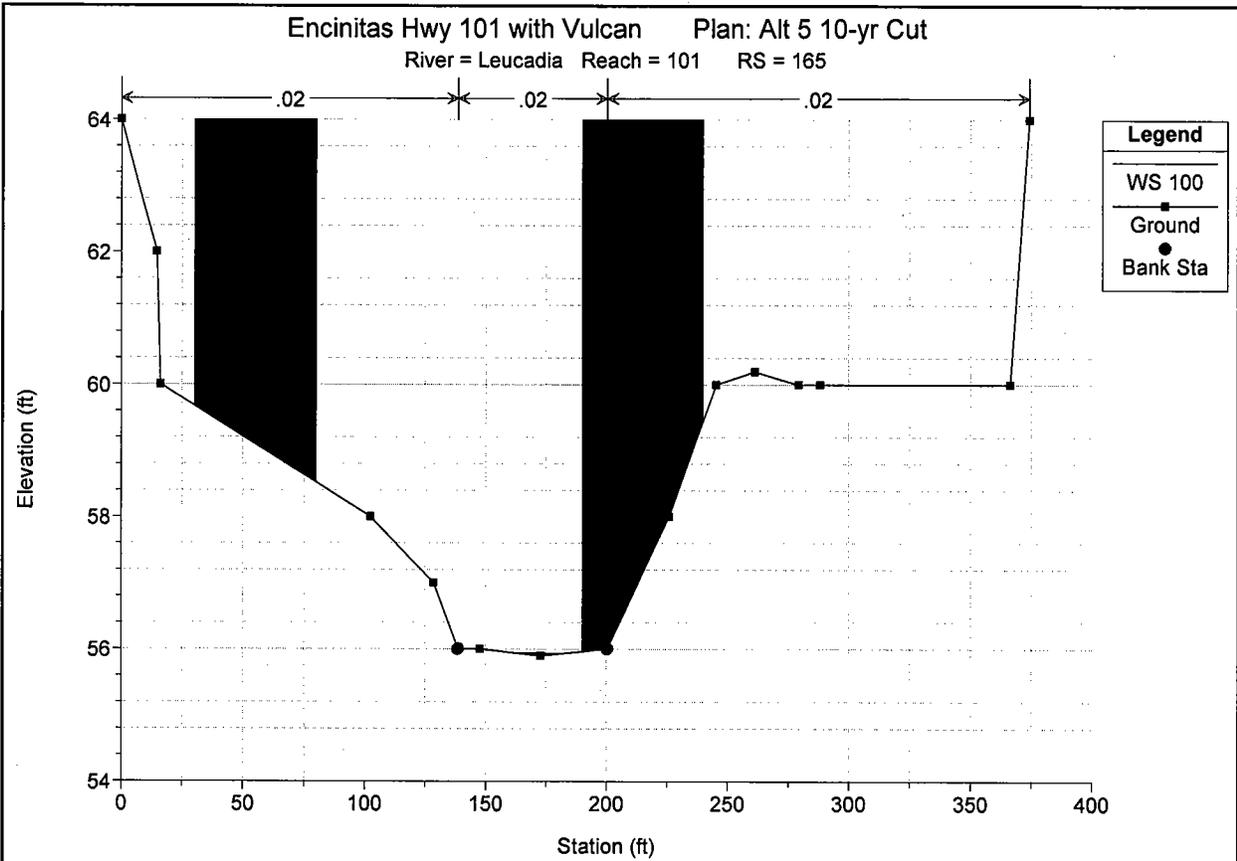


Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut  
 River = Leucadia Reach = 101 RS = 175

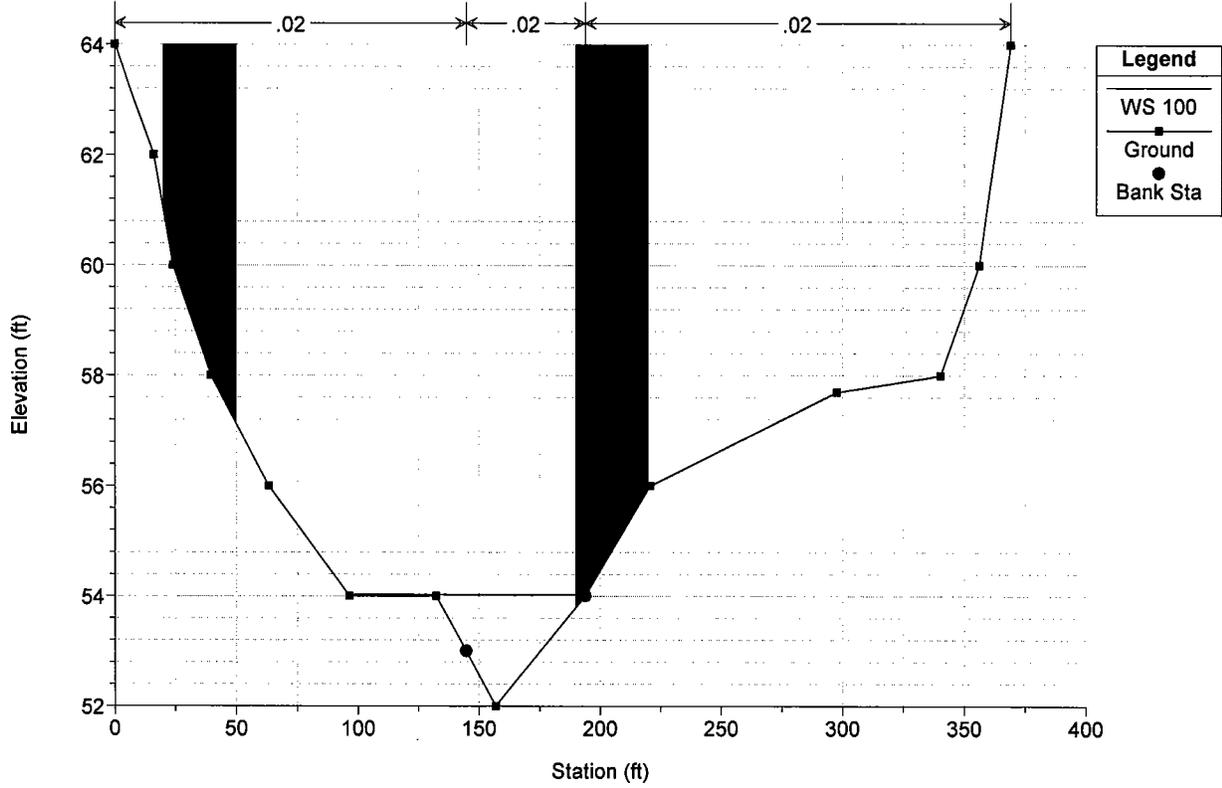


Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut  
 River = Leucadia Reach = 101 RS = 170

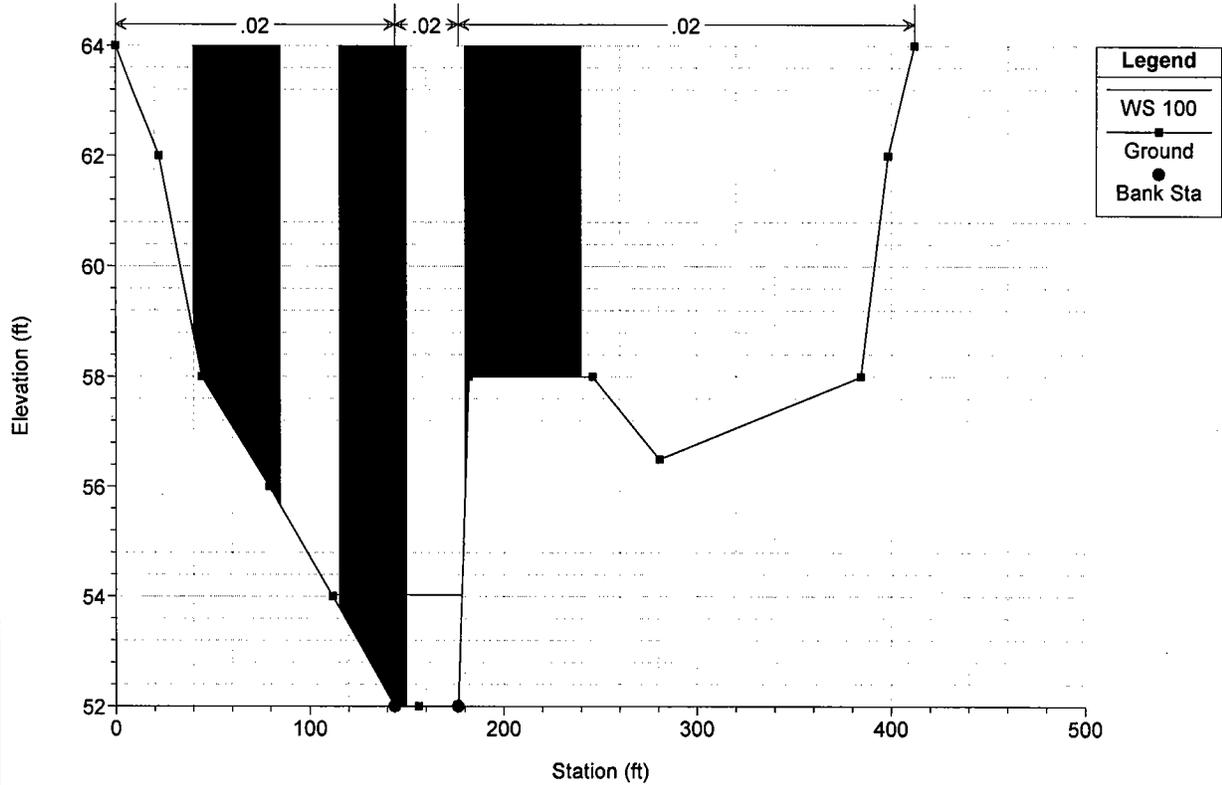




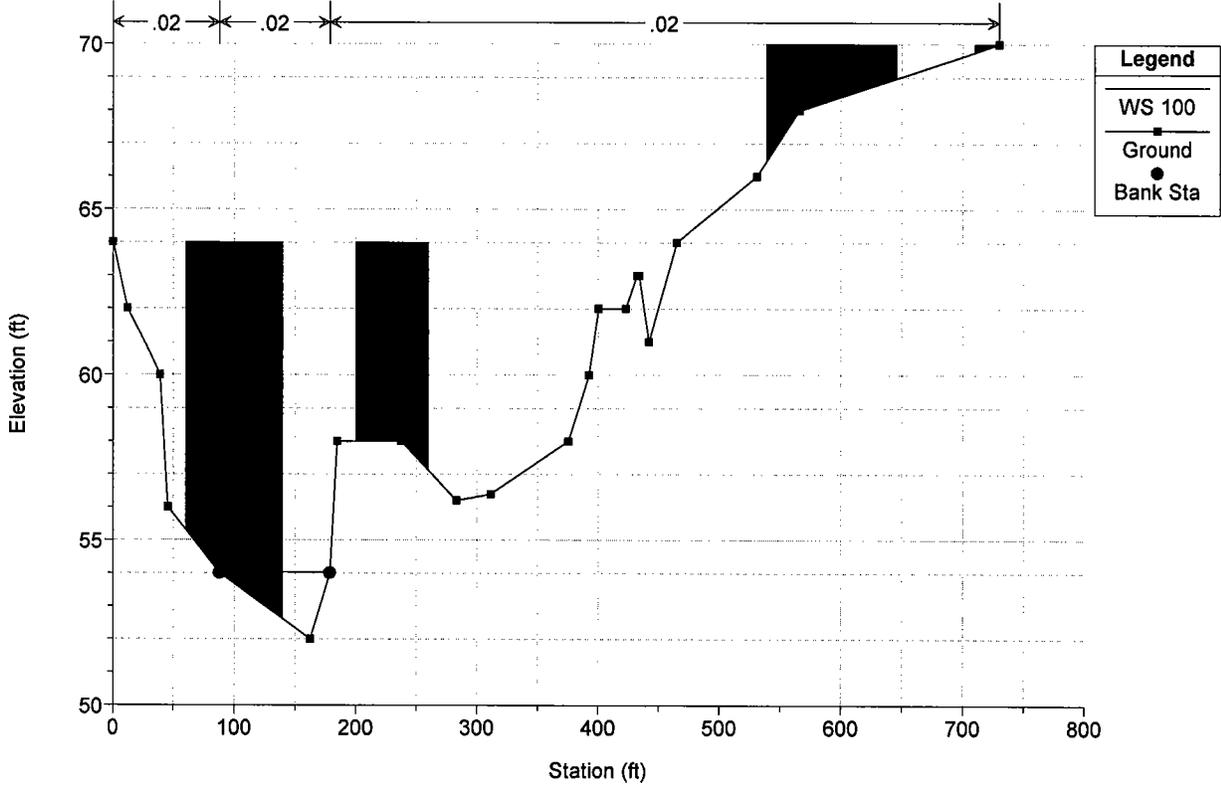
Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut  
 River = Leucadia Reach = 101 RS = 150



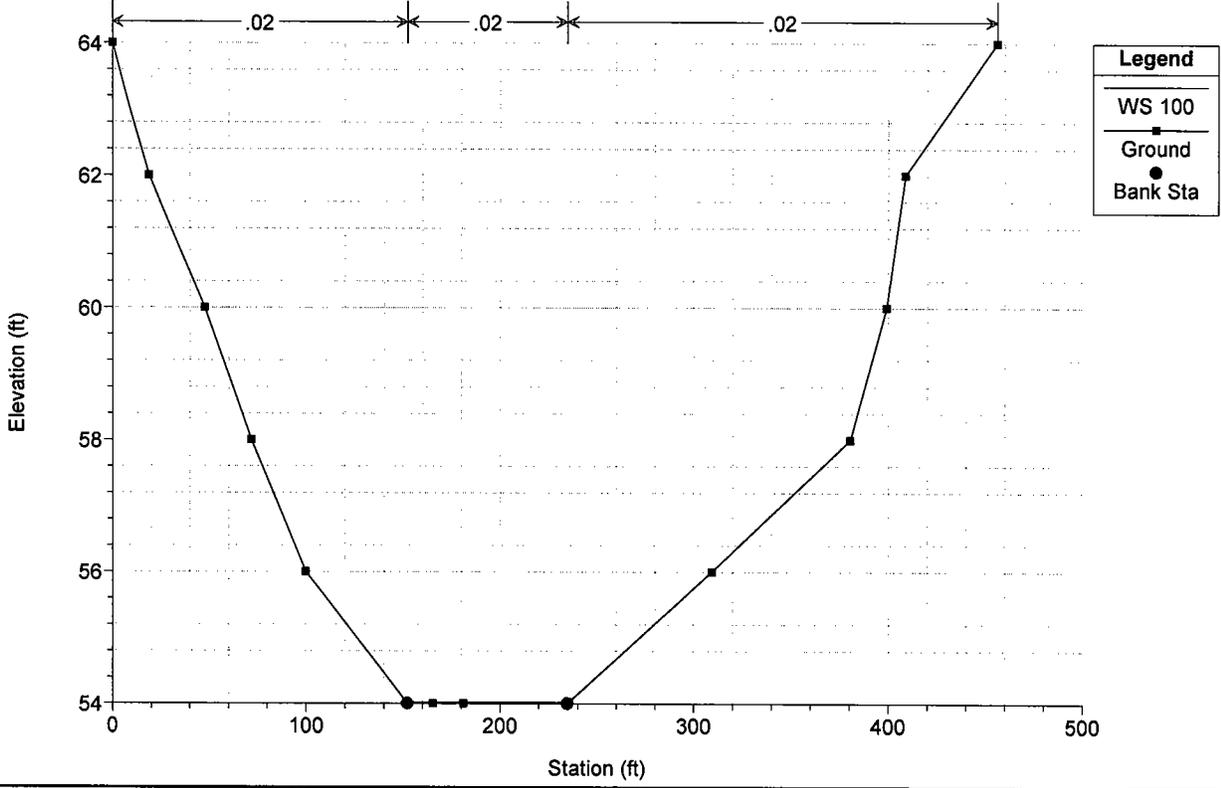
Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut  
 River = Leucadia Reach = 101 RS = 145



Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut  
 River = Leucadia Reach = Combine RS = 140



Encinitas Hwy 101 with Vulcan Plan: Alt 5 10-yr Cut  
 River = Leucadia Reach = Combine RS = 135



HEC-RAS Version 3.0.1 Mar 2001  
 U.S. Army Corp of Engineers  
 Hydrologic Engineering Center  
 609 Second Street, Suite D  
 Davis, California 95616-4687  
 (916) 756-1104

```

X   X  XXXXXX   XXXX       XXXX       XX       XXXX
X   X  X       X   X       X   X       X   X   X
X   X  X       X           X   X       X   X   X
XXXXXXXX XXXX   X           XXX XXXX   XXXXXXX XXXX
X   X  X       X           X   X       X   X       X
X   X  X       X   X       X   X       X   X       X
X   X  XXXXXX   XXXX       X   X       X   X   XXXXX
  
```

PROJECT DATA

Project Title: Encinitas Hwy 101 with Vulcan  
 Project File : 101Vul.prj  
 Run Date and Time: 1/24/2005 9:32:22 AM

Project in English units

Project Description:

ENCINITAS COAST HIGHWAY 101 -100-YR & 10-YR ANALYSIS  
 JN: 14413 DECEMBER 23,  
 2003  
 BASED ON HEC-2 FILENAME: ENC\_1.HC2  
 X-SECTIONS LEFT TO RIGHT LOOKING  
 DOWNSTREAM

PLAN DATA

Plan Title: Alt 5 10-yr Cut  
 Plan File : w:\14413\Hec-Ras 101\101Vul.p08

Geometry Title: Alt 2 Option C Cut @ 135  
 Geometry File : w:\14413\Hec-Ras 101\101Vul.g01

Flow Title : Alt 5 10-yr cut  
 Flow File : w:\14413\Hec-Ras 101\101Vul.f24

Plan Description:

10-YEAR RUN\*\* Includes blocked obstructions in alley  
 Varying Qs based on HEC-1  
 FN: 10A5.hcl  
 Extended XS from 95 down to encompass 100-yr floodplain  
 Vertical  
 Datum NAVD 88

Plan Summary Information:

Number of: Cross Sections =	44	Multiple Openings =	0
Culverts =	0	Inline Weirs =	0
Bridges =	0		

Computational Information

Water surface calculation tolerance =	0.003
Critical depth calculation tolerance =	0.003
Maximum number of iterations =	20
Maximum difference tolerance =	0.1
Flow tolerance factor =	0.001

Computation Options

Critical depth computed only where necessary
Conveyance Calculation Method: At breaks in n values only
Friction Slope Method: Average Conveyance
Computational Flow Regime: Mixed Flow



84	75.16	105	74.56	130	75.16	147	75.46	156	76.16
164	76.96	169	76.96	175	76.16	180.6	74.66	192.8	74.46
196	71.16	204	71.16	207.2	74.46	217	74.66	223	74
230	74	235	74.1	242	74	260	74	273	74
300	74.47	388	76	437	78				

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 84 .03 196 .035 204 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 196 204 100 100 100 .1 .3  
 Left Levee Station= 168.69 Elevation= 76.98

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 3100.16

INPUT

Description:  
 Station Elevation Data num= 18  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 95 74.06 118 73.66 126 74.16 139 75.06 154 75.16  
 160 76.16 164 76.76 169 76.76 175 76.16 179.6 74.96  
 192 74.76 196 70.76 204 70.76 208 74.76 210.7 75.36  
 230 75.15 403 76 456 78

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 95 .03 196 .035 204 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 196 204 100 100 100 .1 .3  
 Left Levee Station= 168.28 Elevation= 76.79

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 3000.17

INPUT

Description:  
 Station Elevation Data num= 16  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 89 72.66 130 73.16 142 74.06 151 74.16 158 75.16  
 165 75.96 170 75.96 176 75.16 179.6 74.46 192 74.26  
 196 70.26 204 70.26 208 74.26 221.38 74.78 423 76  
 476 78

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 89 .03 196 .035 204 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 196 204 100 100 100 .1 .3  
 Left Levee Station= 169.98 Elevation= 76

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 2900.18

INPUT

Description:  
 Station Elevation Data num= 15  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 122 71.16 154 73.16 157 74.16 161 75.16 165 75.36  
 170 75.36 174 75.16 175.4 74.06 192 73.76 196 69.76  
 204 69.76 208 73.76 217.41 74.2 459 76 515 78

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 122 .03 196 .035 204 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 196 204 100 100 100 .1 .3  
 Left Levee Station= 169.51 Elevation= 75.38

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 2800.19

INPUT

Description:

Station Elevation Data		num=		17							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
70	70.06	113	69.46	126	70.16	150	71.16	155	73.16		
160	74.16	164	74.66	169	74.66	174	74.16	175.1	73.56		
192	73.26	196	69.26	204	69.26	208	73.26	225	74.16		
456	76	523	78								

Manning's n Values

num=		3			
Sta	n Val	Sta	n Val	Sta	n Val
70	.03	196	.035	204	.03

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	196	204	168.93	100	100		.1	.3
Left Levee	Station=		Elevation=		74.71			

CROSS SECTION

REACH: Vulcan

RIVER: Leucadia

RS: 2700.20

INPUT

Description:

Station Elevation Data		num=		18							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
125	68.16	139	68.86	146	69.16	150	70.16	154	71.16		
160	73.16	165	73.86	170	73.86	175	73.16	176.2	72.26		
192	71.96	196	67.96	204	67.96	208	71.96	212.73	72.57		
258	74	423	76	535	78						

Manning's n Values

num=		3			
Sta	n Val	Sta	n Val	Sta	n Val
125	.03	196	.035	204	.03

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	196	204	170.68	100	100		.1	.3
Left Levee	Station=		Elevation=		73.86			

CROSS SECTION

REACH: Vulcan

RIVER: Leucadia

RS: 2600.21

INPUT

Description:

Station Elevation Data		num=		20							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
109	66.46	135	66.46	146	68.16	152	69.16	155	70.16		
157	71.16	162	73.16	165	73.26	170	73.26	173	73.16		
181	71.16	185.1	70.06	192	69.96	196	65.96	204	65.96		
208	69.96	215.42	70.99	237	72	286	74	456	76		

Manning's n Values

num=		3			
Sta	n Val	Sta	n Val	Sta	n Val
109	.03	196	.035	204	.03

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	196	204	170.09	100	100		.1	.3
Left Levee	Station=		Elevation=		73.26			

CROSS SECTION

REACH: Vulcan

RIVER: Leucadia

RS: 2500.22

INPUT

Description:

Station Elevation Data		num=		17							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
139	65.16	150	68.16	158	71.16	165	72.76	170	72.76		
175	71.16	182	69.16	184	68.66	192	68.46	196	64.46		
204	64.46	208	68.46	213.55	69.25	233	70	266	72		
320	74	498	76								

Manning's n Values

num=		3			
Sta	n Val	Sta	n Val	Sta	n Val
139	.03	196	.035	204	.03

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	196	204	170.09	100	100		.1	.3
Left Levee	Station=		Elevation=		72.78			

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 2400.23

INPUT

Description:

Station Elevation Data		num= 18									
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
95	65.56	142	65.16	160	71.16	165	72.46	170	72.46		
175	71.16	180	70.16	183	68	192	67.9	194.8	68.16		
202	67.96	206	63.96	214	63.96	218	67.96	221.32	68.78		
250	70	263	72	360	74						

Manning's n Values		num= 3			
Sta	n Val	Sta	n Val	Sta	n Val
95	.03	206	.035	214	.03

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	206	214		100	100		.1	.3
Left Levee	Station=		169.39	Elevation=	72.47			

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 2300.24

INPUT

Description:

Station Elevation Data		num= 18									
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
2	64.46	129	64.46	141	65.16	160	71.16	165	71.86		
170	71.86	175	71.16	185	68.16	190	67	195.2	67.66		
202	67.46	206	63.46	214	63.46	218	67.46	221.7	68.36		
260	70	316	72	382	74						

Manning's n Values		num= 3			
Sta	n Val	Sta	n Val	Sta	n Val
2	.03	206	.035	214	.03

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	206	214		100	100		.1	.3
Left Levee	Station=		170.56	Elevation=	71.89			

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 2200.25

INPUT

Description:

Station Elevation Data		num= 15									
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
140	64.16	160	71.16	165	71.46	170	71.46	172	71.16		
182	68.16	184.7	66.86	192.3	66.76	196	62.96	204	62.96		
207.7	66.76	217	66.86	260	68	287	70	342	72		

Manning's n Values		num= 3			
Sta	n Val	Sta	n Val	Sta	n Val
140	.03	196	.035	204	.03

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	196	204		100	100		.1	.3
Left Levee	Station=		170.39	Elevation=	71.43			

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 2100.26

INPUT

Description:

Station Elevation Data		num= 20									
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
144	63.16	164	71.16	165	71.36	170	71.36	175	71.16		
182	68.16	186	66	188.3	64.96	193.6	64.86	196	62.46		
204	62.46	206.4	64.86	217	65.06	234	66	240	66.1		
245	66	248	65.9	252	66	286	68	322	70		

Manning's n Values		num= 3			
Sta	n Val	Sta	n Val	Sta	n Val
144	.03	196	.035	204	.03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 196 204 15 15 15  
 Left Levee Station= 169.8 Elevation= 71.43

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 245

INPUT

Description:

Station Elevation Data num= 11  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 70 10 70 16 68 24 66 30 64  
 40 64 70 66 80 66 87 66 122 68  
 180 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .03 30 .035 40 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 30 40 175 175 175  
 .1 .3

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 240

INPUT

Description:

Station Elevation Data num= 9  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 70 5 70 10 68 20 66 27 64  
 39 64 89 66 185 68 230 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .03 27 .035 39 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 27 39 275 275 275  
 .1 .3

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 235

INPUT

Description:

Station Elevation Data num= 6  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 68 10 68 15 66 140 66 205 68  
 246 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .03 15 .035 140 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 15 140 120 120 120  
 .1 .3

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 230

INPUT

Description:

Station Elevation Data num= 11  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 430 70 460 70 520 68 525 68 544 69.8  
 546 69.8 550 68 580 66 715 66 770 68  
 825 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 430 .02 580 .02 715 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 580 715 175 180 185  
 .1 .3

Blocked Obstructions num= 1  
 Sta L Sta R Elev  
 797 825 70

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 225

INPUT

Description:

Station Elevation Data		num= 8							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
536	69.8	538	69.8	542	68	595	66	625	66
785	66	827	68	835	70				

Manning's n Values		num= 3			
Sta	n Val	Sta	n Val	Sta	n Val
536	.02	595	.02	785	.02

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	595	785		190	185		.1	.3

Blocked Obstructions		num= 1	
Sta L	Sta R	Elev	
692	835	70	

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 220

INPUT

Description:

Station Elevation Data		num= 7							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
494	69.9	496	69.9	518	68	580	66	876	66
900	68	910	72						

Manning's n Values		num= 3			
Sta	n Val	Sta	n Val	Sta	n Val
494	.02	580	.02	876	.02

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	580	876		175	175		.1	.3

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 215

INPUT

Description:

Station Elevation Data		num= 15							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
540	69.9	542	69.9	546	68	552	67.9	556	68
565	70	580	70.1	594	70	600	69.9	610	70
670	68	815	66	860	66	945	68	995	70

Manning's n Values		num= 3			
Sta	n Val	Sta	n Val	Sta	n Val
540	.02	546	.02	556	.02

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	546	556		290	290		.1	.3

Blocked Obstructions		num= 1	
Sta L	Sta R	Elev	
765	995	70	

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 195

INPUT

Description:

Station Elevation Data		num= 15							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
485	70	496	70	505	68	510	68	515	70
520	72	525	74	533	74	612	72	652	70
695	68	780	66	820	66	920	68	985	70

Manning's n Values		num= 3			
Sta	n Val	Sta	n Val	Sta	n Val
485	.02	505	.02	510	.02

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	505	510		340	340		.1	.3

Blocked Obstructions num= 2  
 Sta L Sta R Elev Sta L Sta R Elev  
 835 903 74 930 985 74

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 175

INPUT

Description:  
 Station Elevation Data num= 7  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 335 68 337 68 344 66 348 65.5 350 66  
 765 68 847 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 335 .02 344 .02 350 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 344 350 225 220 220 .1 .3

Blocked Obstructions num= 2  
 Sta L Sta R Elev Sta L Sta R Elev  
 525 712 70 739 847 70

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 165

INPUT

Description:  
 Station Elevation Data num= 14  
 Sta Elev  
 392 67 394 67 395 66 400 64 410 63  
 418 64 436 66 472 68 512 70 555 72  
 620 72 700 70 795 68 895 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 392 .02 400 .02 418 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 400 418 360 360 360 .1 .3

Blocked Obstructions num= 2  
 Sta L Sta R Elev Sta L Sta R Elev  
 546 781 72 826 895 72

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 150

INPUT

Description:  
 Station Elevation Data num= 12  
 Sta Elev  
 380 65 382 65 385 64 400 63 413 64  
 486 66 520 70 565 74 698 74 750 72  
 967 72 1040 74

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 380 .02 385 .02 413 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 385 413 305 305 305 .1 .3

Blocked Obstructions num= 1  
 Sta L Sta R Elev  
 606 1040 74

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 230

INPUT

Description:  
 Station Elevation Data num= 8  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 66 25.4 64 30.5 62 88.9 60.2 146 60  
 243.4 62 278 64 318.4 66

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 88.9 .02 146 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 88.9 146 104.1 100.2 136.3 .1 .3

Blocked Obstructions num= 3  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 50 80 66 145 190 66 285 350 66

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 225.3

INPUT

Description:  
 Station Elevation Data num= 14  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 66 16 64 32.6 62 78.4 60 126.9 58  
 133.4 58 139.4 58 203.7 58 210.3 58 216.8 58.5  
 233.9 60 285.5 62 319.2 64 355 66

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 126.9 .02 203.7 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 126.9 203.7 5 5 5 .1 .3

Blocked Obstructions num= 5  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 5 30 66 130 160 66 180 200 66  
 210 235 66 300 345 66

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 225.2

INPUT

Description:  
 Station Elevation Data num= 14  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 66 16 64 32.6 62 78.4 60 126.9 58  
 133.4 54 139.4 54 203.7 56 210.3 58 216.8 58.5  
 233.9 60 285.5 62 319.2 64 355 66

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 126.9 .02 203.7 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 126.9 203.7 5 5 5 .1 .3

Blocked Obstructions num= 5  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 5 30 66 130 160 66 180 200 66  
 210 235 66 300 345 66

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 225.1

INPUT

Description:  
 Station Elevation Data num= 14  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 66 16 64 32.6 62 78.4 60 126.9 58  
 133.4 58 139.4 58 203.7 58 210.3 58 216.8 58.5  
 233.9 60 285.5 62 319.2 64 355 66

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 126.9 .02 203.7 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 126.9 203.7 134.2 131.9 133.3 .1 .3

Blocked Obstructions num= 5  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 5 30 66 130 160 66 180 200 66  
 210 235 66 300 345 66

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 220

INPUT

Description:

Station Elevation Data		num= 11		Sta Elev		Sta Elev		Sta Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	66	18.9	64	21	62	30.1	60	56.5	58
114.4	57.7	192	58	255	60	292.4	62	321.2	64
343.3	66								

Manning's n Values		num= 3		Sta n Val		Sta n Val	
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.02	56.5	.02	192	.02		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	56.5	192		222.7	215.1		.1	.3

Blocked Obstructions		num= 3		Sta L Sta R Elev		Sta L Sta R Elev		
Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta L	Sta R	Elev
20	60	66	105	140	66	155	190	66

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 215

INPUT

Description:

Station Elevation Data		num= 14		Sta Elev		Sta Elev		Sta Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	66	10	64	35.7	62	75.9	60	102.5	58
121.6	56	143.9	56	204.1	56	241	56	286	58
307.5	60	345.4	62	377.3	64	381.6	66		

Manning's n Values		num= 3		Sta n Val		Sta n Val	
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.02	121.6	.02	241	.02		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	121.6	241		78.2	80.6		.1	.3

Blocked Obstructions		num= 2		Sta L Sta R Elev		Sta L Sta R Elev		
Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta L	Sta R	Elev
10	75	66	160	220	66			

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 210

INPUT

Description:

Station Elevation Data		num= 11		Sta Elev		Sta Elev		Sta Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	66	10.4	64	23.6	62	63.8	60	101.7	58
120.4	56	193.3	56	272.5	56	296.1	58	304.2	60
312.7	66								

Manning's n Values		num= 3		Sta n Val		Sta n Val	
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.02	120.4	.02	272.5	.02		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	120.4	272.5		47.1	45.4		.1	.3

Blocked Obstructions		num= 2		Sta L Sta R Elev		Sta L Sta R Elev		
Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta L	Sta R	Elev
20	170	66	210	250	66			

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 205

INPUT

Description:

Station Elevation Data		num= 9		Sta Elev		Sta Elev		Sta Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	64	14	62	58.3	60	89	58	110.7	56
182	56	218.5	56	292.3	58	302.4	64		

Manning's n Values		num= 3		Sta n Val		Sta n Val	
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.02	110.7	.02	218.5	.02		

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 110.7 218.5 141.2 142.6 152.6 .1 .3  
 Blocked Obstructions num= 5  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 0 30 64 60 100 64 140 170 64  
 200 225 64 255 280 64

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 195

INPUT

Description:  
 Station Elevation Data num= 9  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 64 35.6 62 68.6 60 113.8 58 198.9 56  
 266.6 58 298.8 60 323.4 62 337.5 64

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 113.8 .02 266.6 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 113.8 266.6 143.6 102.4 81.7 .1 .3  
 Blocked Obstructions num= 3  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 95 130 64 150 180 64 210 255 64

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 190

INPUT

Description:  
 Station Elevation Data num= 8  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 64 16.8 62 31.4 60 99.1 58 133.4 58  
 179.5 58 217.5 60 231.5 64

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 99.1 .02 179.5 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 99.1 179.5 109.2 93.8 106 .1 .3  
 Blocked Obstructions num= 4  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 0 10 64 35 65 64 90 120 64  
 185 230 64

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 185

INPUT

Description:  
 Station Elevation Data num= 6  
 Sta Elev Sta Elev Sta Elev Sta Elev  
 0 64 21.3 62 59.2 60 118.2 59 204.1 60  
 212.1 64

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 59.2 .02 204.1 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 59.2 204.1 56.4 82.7 111.4 .1 .3  
 Blocked Obstructions num= 2  
 Sta L Sta R Elev Sta L Sta R Elev  
 60 100 64 150 210 64

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 180

INPUT

Description:  
 Station Elevation Data num= 9  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 64 21.3 62 59.2 60 118.2 59 204.1 60  
 212.1 64

0	64	17	62	30.5	60	71.4	59	113.4	60
120.7	64	192.2	64	257.1	63	317.6	64		

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 30.5 .02 113.4 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 30.5 113.4 83.8 85.3 85.6 .1 .3  
 Blocked Obstructions num= 2  
 Sta L Sta R Elev Sta L Sta R Elev  
 40 85 64 130 190 64

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 175

INPUT

Description:  
 Station Elevation Data num= 11  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 64 5.6 62 20.6 60 56.6 59 99.6 60  
 104.6 62 172 63 232 62 252.5 61.9 268.5 62  
 309.1 64

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 20.6 .02 99.6 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 20.6 99.6 120.2 124.8 122.1 .1 .3  
 Blocked Obstructions num= 2  
 Sta L Sta R Elev Sta L Sta R Elev  
 20 55 64 110 160 64

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 170

INPUT

Description:  
 Station Elevation Data num= 7  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 64 33.4 62 87.4 60 141.8 58.5 184.7 60  
 322 62 333.5 64

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 87.4 .02 184.7 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 87.4 184.7 137.5 137.6 138.7 .1 .3

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 165

INPUT

Description:  
 Station Elevation Data num= 16  
 Sta Elev  
 0 64 14.5 62 16 60 102.4 58 128.4 57  
 138.5 56 147.5 56 172.9 55.9 200.4 56 225.9 58  
 245.3 60 261.4 60.2 279.4 60 288.3 60 366.3 60  
 374.3 64

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 138.5 .02 200.4 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 138.5 200.4 309.6 309.5 308.6 .1 .3  
 Blocked Obstructions num= 2  
 Sta L Sta R Elev Sta L Sta R Elev  
 30 80 64 190 240 64

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 160

INPUT

Description:

Station Elevation Data											
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	64	21	62	37	60	57.5	58	105	56		
129.5	55	142.1	55	152.6	55	186.5	54	214.5	55		
237	56	283.6	58	300.1	58.1	317	58	333	57.9		
342	58	359	60	368	62	376	64				

Manning's n Values					
Sta	n Val	Sta	n Val	Sta	n Val
0	.02	152.6	.02	214.5	.02

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	152.6	214.5		48.6	52.6		.1	.3

Blocked Obstructions										
Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta R	Elev
30	70	64	90	120	64	150	170	64		

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 150

INPUT

Description:

Station Elevation Data											
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	64	16	62	24	60	39.5	58	63.4	56		
96.4	54	132.3	54	144.8	53	156.9	52	193.8	54		
220.8	56	297.7	57.7	340.3	58	356.3	60	369.2	64		

Manning's n Values					
Sta	n Val	Sta	n Val	Sta	n Val
0	.02	144.8	.02	193.8	.02

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	144.8	193.8		151.2	154.7		.1	.3

Blocked Obstructions										
Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta R	Elev
20	50	64	190	220	64					

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 145

INPUT

Description:

Station Elevation Data											
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	64	22.3	62	44.3	58	79.3	56	111.6	54		
143.9	52	156.1	52	176.6	52	182.1	58	246	58		
280.5	56.5	384.4	58	398.4	62	411.9	64				

Manning's n Values					
Sta	n Val	Sta	n Val	Sta	n Val
0	.02	143.9	.02	176.6	.02

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	143.9	176.6		175.6	160.5		.1	.3

Blocked Obstructions										
Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta R	Elev
40	85	64	115	150	64	180	240	64		

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 140

INPUT

Description:

Station Elevation Data											
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	64	12.5	62	39	60	45.5	56	88	54		
162.6	52	178.6	54	184.6	58	237.6	58	283.1	56.2		
311.6	56.4	375.5	58	392.5	60	400.6	62	422.6	62		
432	63	434	63	442	61	465	64	531	66		
566	68	730	70								

Manning's n Values					
Sta	n Val	Sta	n Val	Sta	n Val

0 .02 88 .02 178.6 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 88 178.6 141.5 123.2 117.1 .1 .3  
 Blocked Obstructions num= 4  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 60 140 64 200 260 64 539 646 70  
 710 730 70

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 135

INPUT

Description:

Station Elevation Data num= 14  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 64 18.7 62 47.7 60 71.8 58 99.9 56  
 152.2 54 165.3 54 181.2 54 234.9 54 309.4 56  
 380.6 58 399.2 60 408.7 62 456.1 64

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 152.2 .02 234.9 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 152.2 234.9 6244 6224.6 6385.5 .1 .3

SUMMARY OF MANNING'S N VALUES

River:Leucadia

Reach	River Sta.	n1	n2	n3
Vulcan	3300.14	.03	.035	.03
Vulcan	3200.15	.03	.035	.03
Vulcan	3100.16	.03	.035	.03
Vulcan	3000.17	.03	.035	.03
Vulcan	2900.18	.03	.035	.03
Vulcan	2800.19	.03	.035	.03
Vulcan	2700.20	.03	.035	.03
Vulcan	2600.21	.03	.035	.03
Vulcan	2500.22	.03	.035	.03
Vulcan	2400.23	.03	.035	.03
Vulcan	2300.24	.03	.035	.03
Vulcan	2200.25	.03	.035	.03
Vulcan	2100.26	.03	.035	.03
Vulcan	245	.03	.035	.03
Vulcan	240	.03	.035	.03
Vulcan	235	.03	.035	.03
Vulcan	230	.02	.02	.02
Vulcan	225	.02	.02	.02
Vulcan	220	.02	.02	.02
Vulcan	215	.02	.02	.02
Vulcan	195	.02	.02	.02
Vulcan	175	.02	.02	.02
Vulcan	165	.02	.02	.02
Vulcan	150	.02	.02	.02
101	230	.02	.02	.02
101	225.3	.02	.02	.02
101	225.2	.02	.02	.02
101	225.1	.02	.02	.02
101	220	.02	.02	.02
101	215	.02	.02	.02
101	210	.02	.02	.02
101	205	.02	.02	.02
101	195	.02	.02	.02
101	190	.02	.02	.02
101	185	.02	.02	.02
101	180	.02	.02	.02
101	175	.02	.02	.02
101	170	.02	.02	.02
101	165	.02	.02	.02
101	160	.02	.02	.02
101	150	.02	.02	.02

101	145	.02	.02	.02
Combine	140	.02	.02	.02
Combine	135	.02	.02	.02

SUMMARY OF REACH LENGTHS

River: Leucadia

Reach	River Sta.	Left	Channel	Right
Vulcan	3300.14	100	100	100
Vulcan	3200.15	100	100	100
Vulcan	3100.16	100	100	100
Vulcan	3000.17	100	100	100
Vulcan	2900.18	100	100	100
Vulcan	2800.19	100	100	100
Vulcan	2700.20	100	100	100
Vulcan	2600.21	100	100	100
Vulcan	2500.22	100	100	100
Vulcan	2400.23	100	100	100
Vulcan	2300.24	100	100	100
Vulcan	2200.25	100	100	100
Vulcan	2100.26	15	15	15
Vulcan	245	175	175	175
Vulcan	240	275	275	275
Vulcan	235	120	120	120
Vulcan	230	175	180	185
Vulcan	225	190	185	185
Vulcan	220	175	175	175
Vulcan	215	290	290	290
Vulcan	195	340	340	340
Vulcan	175	225	220	220
Vulcan	165	360	360	360
Vulcan	150	305	305	305
101	230	104.1	100.2	136.3
101	225.3	5	5	5
101	225.2	5	5	5
101	225.1	134.2	131.9	133.3
101	220	222.7	215.1	206.1
101	215	78.2	80.6	89.6
101	210	47.1	45.4	64.5
101	205	141.2	142.6	152.6
101	195	143.6	102.4	81.7
101	190	109.2	93.8	106
101	185	56.4	82.7	111.4
101	180	83.8	85.3	85.6
101	175	120.2	124.8	122.1
101	170	137.5	137.6	138.7
101	165	309.6	309.5	308.6
101	160	48.6	52.6	51.9
101	150	151.2	154.7	157.7
101	145	175.6	160.5	160.3
Combine	140	141.5	123.2	117.1
Combine	135	6244	6224.6	6385.5

SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS

River: Leucadia

Reach	River Sta.	Contr.	Expan.
Vulcan	3300.14	.1	.3
Vulcan	3200.15	.1	.3
Vulcan	3100.16	.1	.3
Vulcan	3000.17	.1	.3
Vulcan	2900.18	.1	.3
Vulcan	2800.19	.1	.3
Vulcan	2700.20	.1	.3
Vulcan	2600.21	.1	.3
Vulcan	2500.22	.1	.3

Vulcan	2400.23	.1	.3
Vulcan	2300.24	.1	.3
Vulcan	2200.25	.1	.3
Vulcan	2100.26	.1	.3
Vulcan	245	.1	.3
Vulcan	240	.1	.3
Vulcan	235	.1	.3
Vulcan	230	.1	.3
Vulcan	225	.1	.3
Vulcan	220	.1	.3
Vulcan	215	.1	.3
Vulcan	195	.1	.3
Vulcan	175	.1	.3
Vulcan	165	.1	.3
Vulcan	150	.1	.3
101	230	.1	.3
101	225.3	.1	.3
101	225.2	.1	.3
101	225.1	.1	.3
101	220	.1	.3
101	215	.1	.3
101	210	.1	.3
101	205	.1	.3
101	195	.1	.3
101	190	.1	.3
101	185	.1	.3
101	180	.1	.3
101	175	.1	.3
101	170	.1	.3
101	165	.1	.3
101	160	.1	.3
101	150	.1	.3
101	145	.1	.3
Combine	140	.1	.3
Combine	135	.1	.3

**ALTERNATIVE 5**  
**100-YEAR HEC-RAS ANALYSIS**

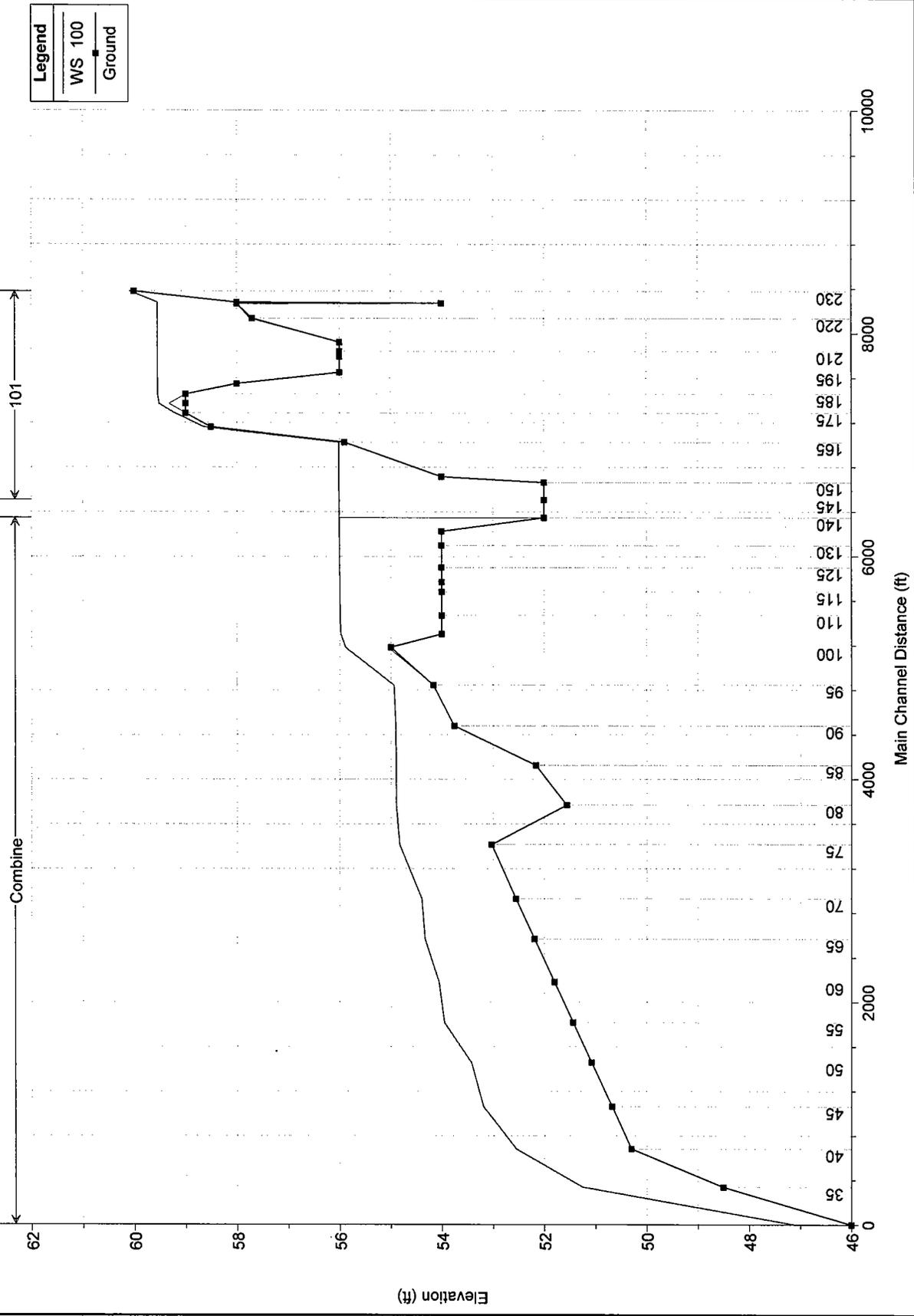
HEC-RAS Plan: 100A5 Profile: 100

Reach	River Sta	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Vulcan	3300.14	13.00	72.16	72.59	72.59	72.79	0.023812	3.71	3.58	8.85	1.00
Vulcan	3200.15	13.00	71.16	71.88	71.58	71.95	0.003891	2.14	6.30	9.40	0.44
Vulcan	3100.16	13.00	70.76	71.44	71.19	71.51	0.004919	2.29	5.86	9.35	0.49
Vulcan	3000.17	13.00	70.26	70.93	70.69	71.01	0.005168	2.33	5.77	9.33	0.50
Vulcan	2900.18	13.00	69.76	70.47	70.19	70.54	0.004234	2.19	6.14	9.41	0.46
Vulcan	2800.19	13.00	69.26	69.83	69.69	69.94	0.008797	2.74	4.88	9.14	0.64
Vulcan	2700.20	13.00	67.96	68.39	68.39	68.59	0.022845	3.66	3.63	8.86	0.98
Vulcan	2600.21	13.00	65.96	66.85	66.39	66.90	0.001875	1.71	7.95	9.79	0.32
Vulcan	2500.22	13.00	64.46	66.86	64.89	66.87	0.000057	0.58	25.01	12.81	0.07
Vulcan	2400.23	13.00	63.96	66.86	64.39	66.87	0.000029	0.46	31.66	13.81	0.05
Vulcan	2300.24	13.00	63.46	66.86	63.89	66.87	0.000016	0.38	38.81	14.81	0.04
Vulcan	2200.25	13.00	62.96	66.86	63.39	66.87	0.000012	0.36	46.96	32.44	0.03
Vulcan	2100.26	13.00	62.46	66.86	62.89	66.86	0.000002	0.16	129.37	82.28	0.01
Vulcan	245	13.00	64.00	66.86		66.86	0.000003	0.15	118.42	81.57	0.02
Vulcan	240	1.00	64.00	66.86		66.86	0.000000	0.01	160.35	114.77	0.00
Vulcan	235	1.00	66.00	66.86		66.86	0.000000	0.01	121.00	155.23	0.00
Vulcan	230	1.00	66.00	66.86		66.86	0.000000	0.01	132.43	171.70	0.00
Vulcan	225	1.00	66.00	66.86		66.86	0.000000	0.01	93.65	119.89	0.00
Vulcan	220	1.00	66.00	66.86		66.86	0.000000	0.00	271.66	333.13	0.00
Vulcan	215	1.00	67.90	66.83	66.83	66.86	0.014435		0.68	9.90	0.00
Vulcan	195	38.00	68.00	66.71	66.27	66.72	0.000260		47.12	84.98	0.00
Vulcan	175	38.00	65.50	66.37	66.37	66.48	0.004576	3.64	18.56	85.07	0.81
Vulcan	165	38.00	63.00	64.57	64.02	64.62	0.000608	1.90	21.04	24.51	0.33
Vulcan	150	38.00	63.00	63.86	63.86	64.07	0.007780	3.71	10.24	23.94	1.00
101	230	1.00	60.00	60.08	60.08	60.10	0.017075	1.12	0.89	22.55	1.00
101	225.3	1.00	58.00	59.54	58.03	59.54	0.000000	0.01	79.95	70.52	0.00
101	225.2	1.00	54.64	59.54		59.54	0.000000	0.01	158.06	70.52	0.00
101	225.1	1.00	58.00	59.54		59.54	0.000000	0.01	79.94	70.52	0.00
101	220	1.00	57.75	59.54		59.54	0.000000	0.01	141.80	110.60	0.00
101	215	1.00	56.00	59.54		59.54	0.000000	0.00	402.07	160.61	0.00
101	210	1.00	56.00	59.54		59.54	0.000000	0.00	286.25	92.35	0.00
101	205	1.00	56.00	59.54		59.54	0.000000	0.00	354.55	114.90	0.00
101	195	1.00	56.00	59.54		59.54	0.000000	0.01	188.18	102.50	0.00
101	190	1.00	58.00	59.54		59.54	0.000000	0.01	122.09	90.00	0.00
101	185	1.00	59.00	59.54		59.54	0.000002	0.05	18.44	50.00	0.02
101	180	1.00	59.32	59.51	59.49	59.54	0.008400	1.38	0.73	7.81	0.80

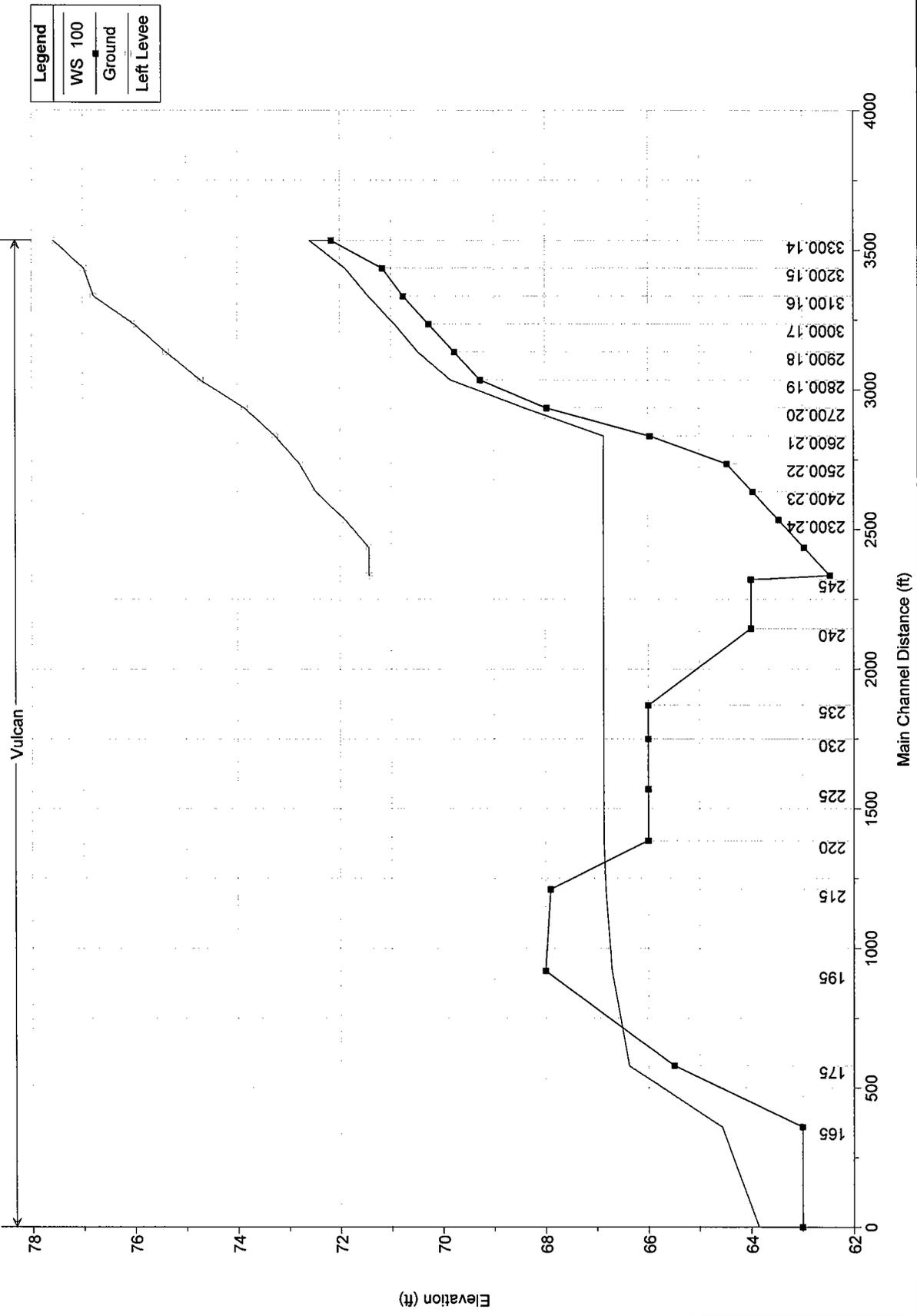
HEC-RAS Plan: 100A5 Profile: 100 (Continued)

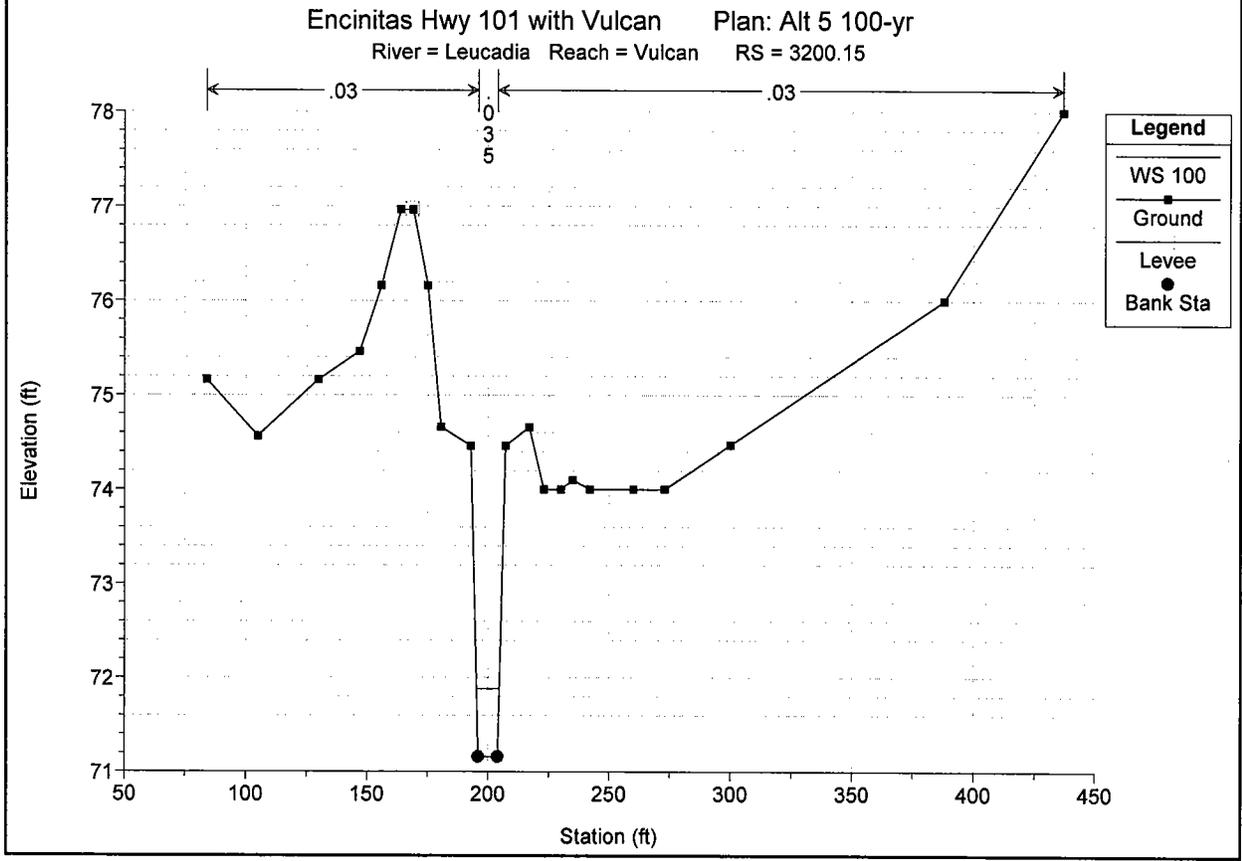
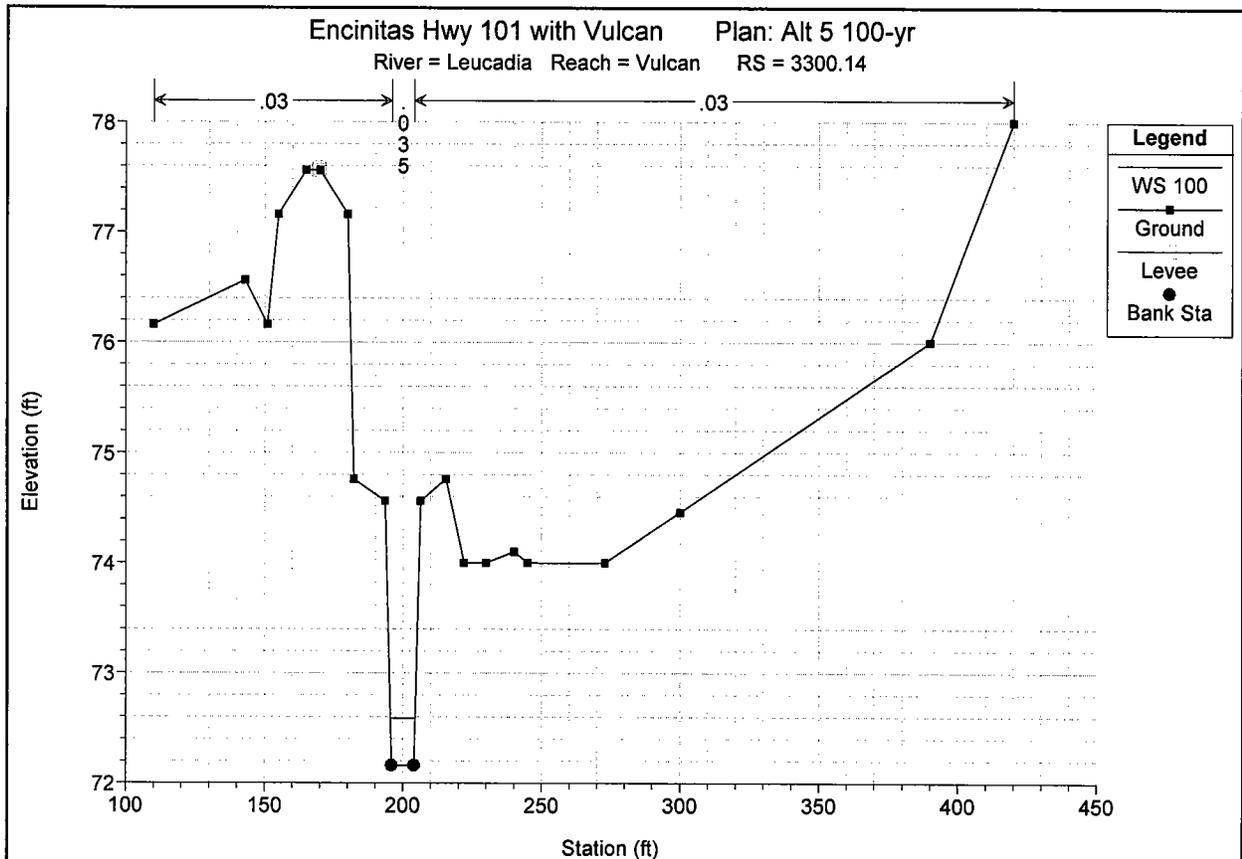
Reach	River Sta	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude #	Chl
101	175	1.00	59.00	59.21	59.14	59.22	0.002048	0.80	1.25	10.64	0.41	
101	170	1.00	58.50	58.64	58.64	58.68	0.014397	1.53	0.65	9.21	1.01	
101	165	1.00	55.90	56.01	55.96	56.02	0.000721	0.31	3.20	51.65	0.22	
101	160	1.00	54.00	56.01		56.01	0.000000	0.01	111.82	97.34	0.00	
101	150	1.00	52.00	56.01		56.01	0.000000	0.00	282.74	128.12	0.00	
101	145	1.00	52.00	56.01		56.01	0.000000	0.01	152.78	60.00	0.00	
Combine	140	47.00	52.00	56.01	52.75	56.01	0.000005	0.35	139.98	56.13	0.03	
Combine	135	47.00	54.00	56.01		56.01	0.000003	0.19	293.67	209.85	0.02	
Combine	130	47.00	54.00	56.00		56.01	0.000036	0.70	82.16	79.33	0.09	
Combine	125	47.00	54.00	56.00		56.00	0.000004	0.23	245.07	159.21	0.03	
Combine	120	57.00	54.00	55.99		56.00	0.000038	0.68	103.14	107.20	0.09	
Combine	115	57.00	54.00	55.99		56.00	0.000037	0.66	105.24	116.10	0.08	
Combine	110	57.00	54.00	55.99		55.99	0.000009	0.33	212.00	167.22	0.04	
Combine	105	90.00	54.00	55.98		55.99	0.000081	0.99	136.00	161.14	0.12	
Combine	100	90.00	55.06	55.88	55.75	55.95	0.003147	2.06	43.74	124.73	0.61	
Combine	95	90.00	54.16	54.94		55.03	0.002337	2.47	39.95	89.47	0.58	
Combine	90	106.00	53.76	54.91		54.91	0.000096	0.79	153.98	171.87	0.13	
Combine	85	106.00	52.16	54.90		54.90	0.000013	0.44	262.92	152.87	0.06	
Combine	80	106.00	51.56	54.89		54.90	0.000018	0.58	238.19	170.79	0.07	
Combine	75	152.00	53.03	54.83		54.87	0.000442	1.66	93.03	129.66	0.34	
Combine	70	152.00	52.55	54.40		54.55	0.000979	3.17	48.00	51.04	0.58	
Combine	65	152.00	52.19	54.33		54.35	0.00243	1.21	142.49	263.50	0.26	
Combine	60	186.00	51.80	54.06		54.18	0.000702	2.84	65.50	81.57	0.56	
Combine	55	186.00	51.44	53.95		54.00	0.000293	1.78	104.40	81.71	0.28	
Combine	50	276.00	51.08	53.42		53.75	0.001421	4.55	60.65	31.73	0.58	
Combine	45	276.00	50.68	53.19		53.31	0.000677	2.80	99.29	71.57	0.41	
Combine	40	276.00	50.30	52.55		52.90	0.001653	4.79	57.56	31.49	0.62	
Combine	35	276.00	48.50	51.25	51.25	51.91	0.005729	6.50	42.48	33.34	1.01	
Combine	30	276.00	46.00	47.11	47.60	48.74	0.017137	10.41	27.36	26.46	1.74	

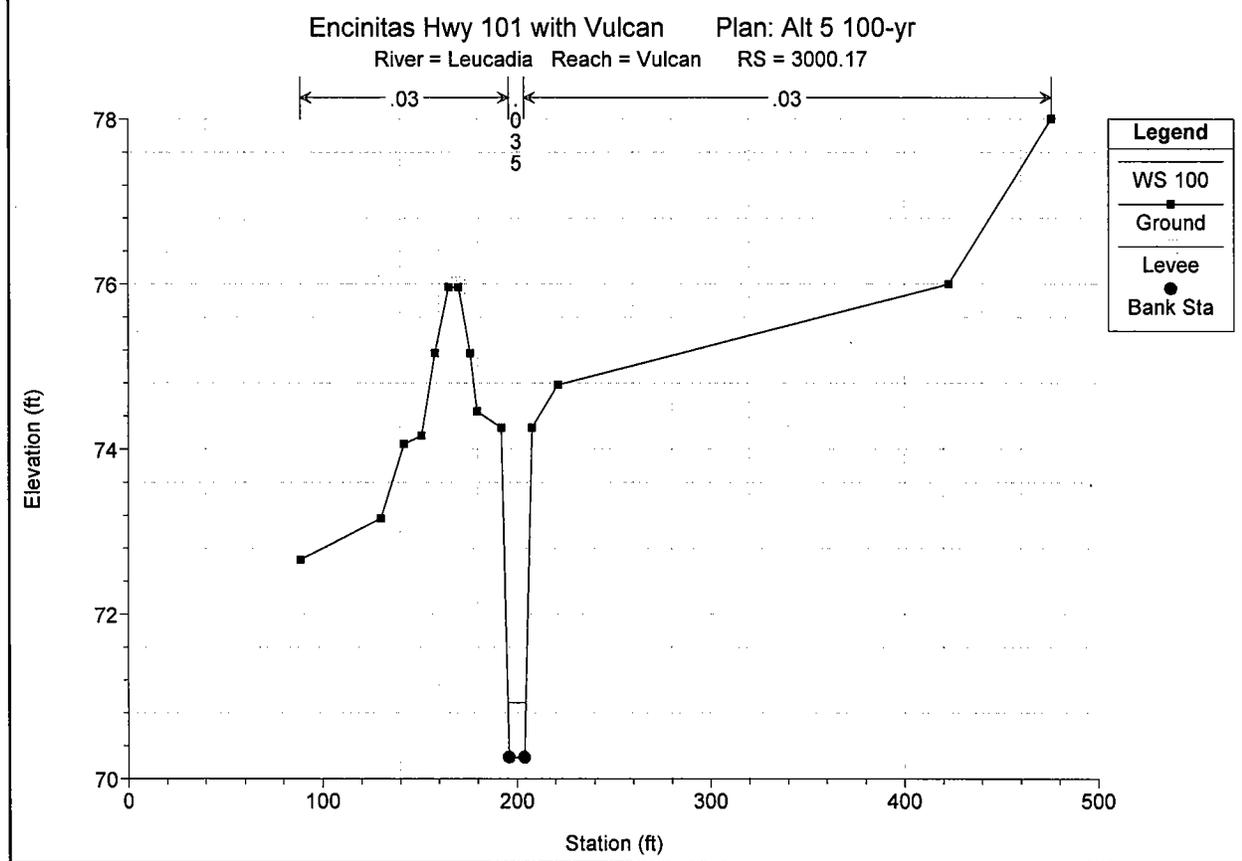
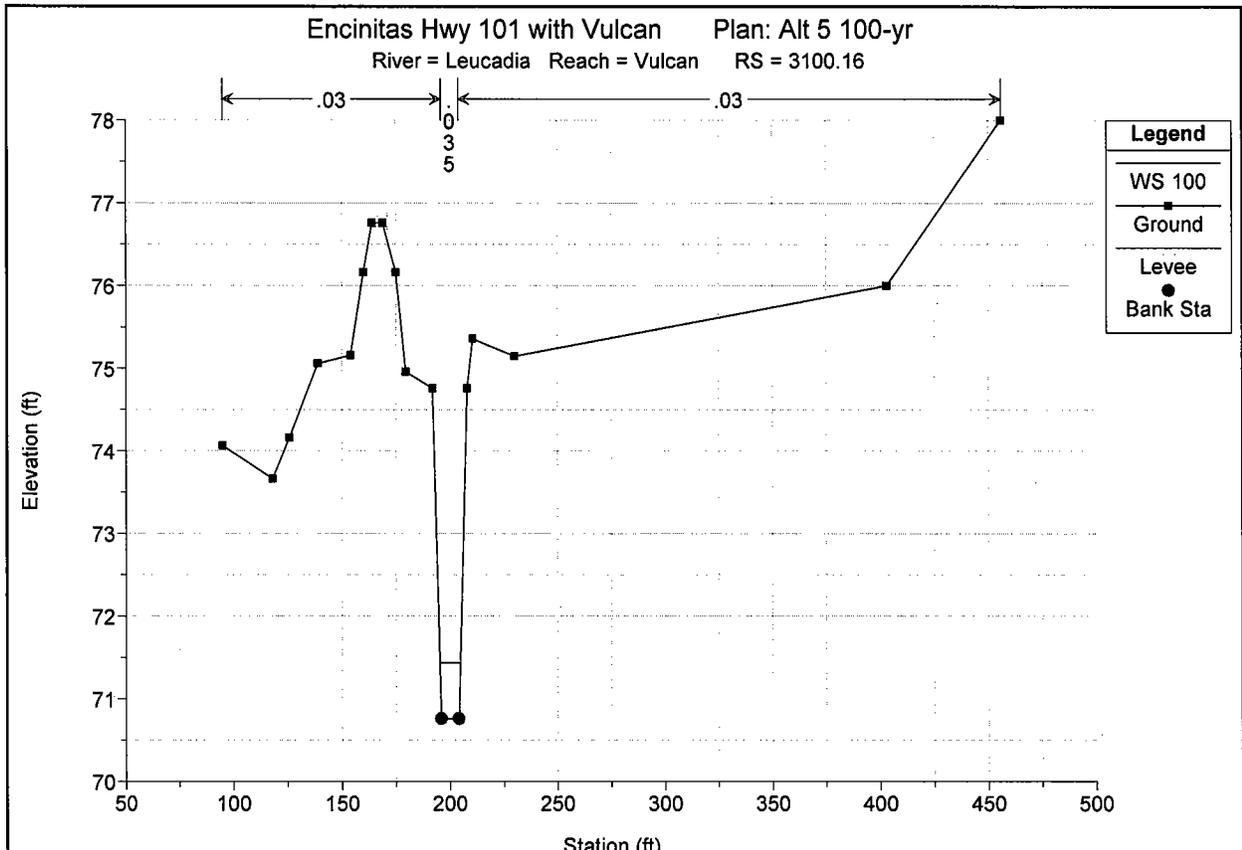
Encinitas Hwy 101 with Vulcan Plan: Alt 5 100-yr

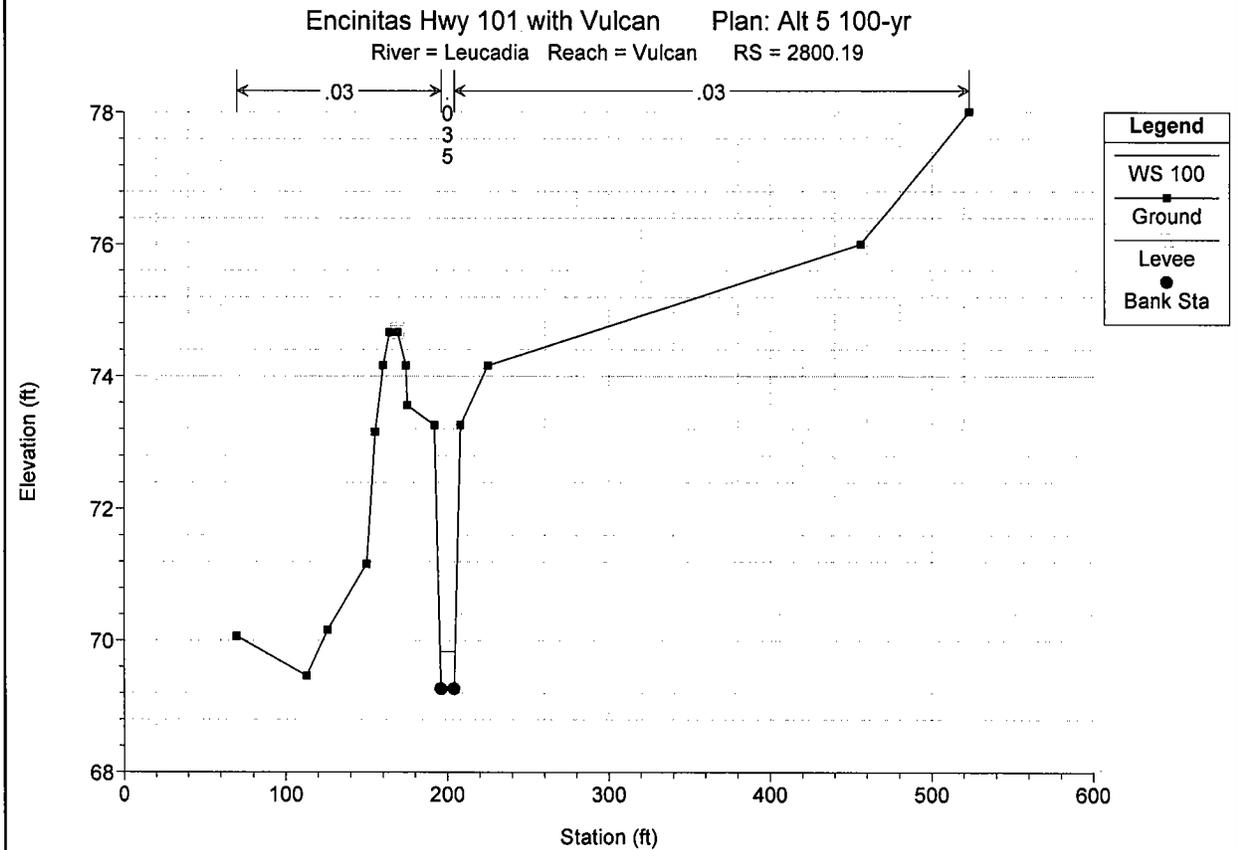
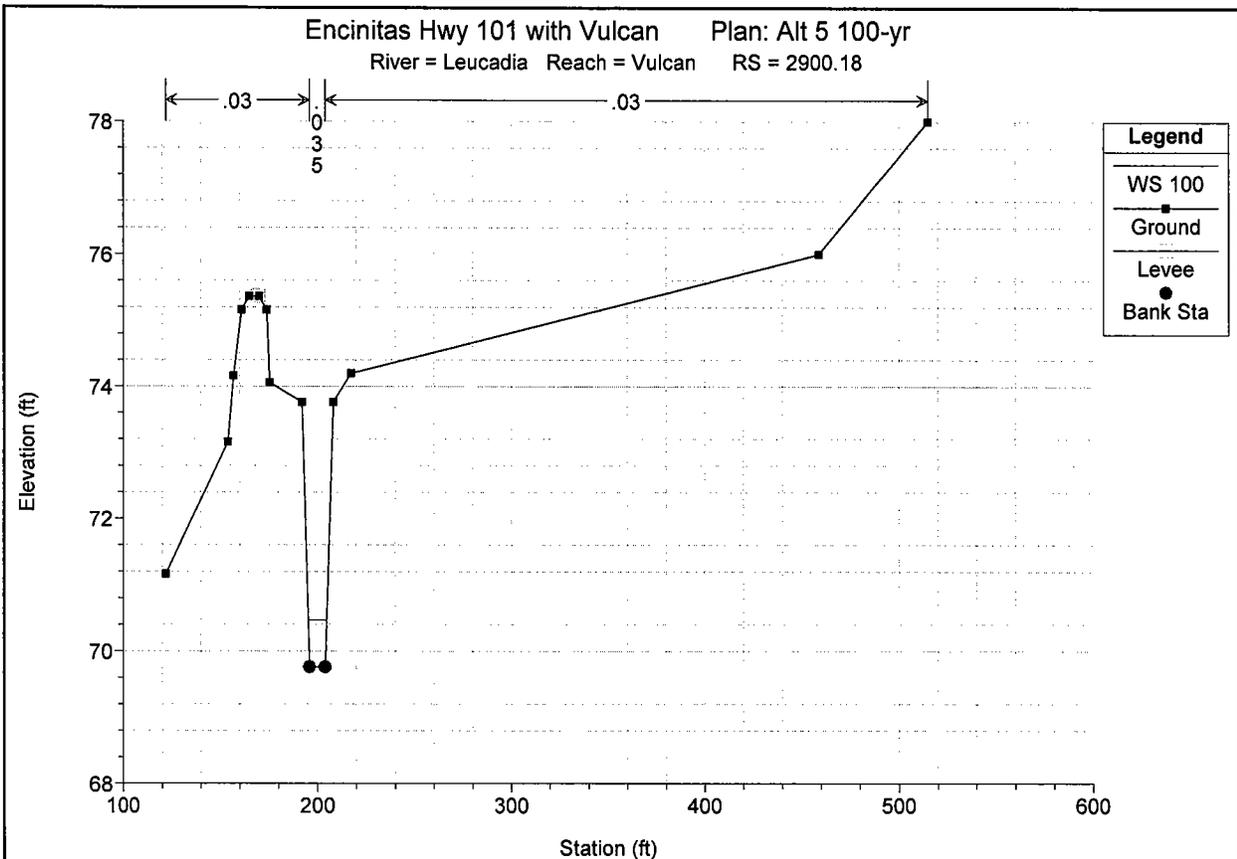


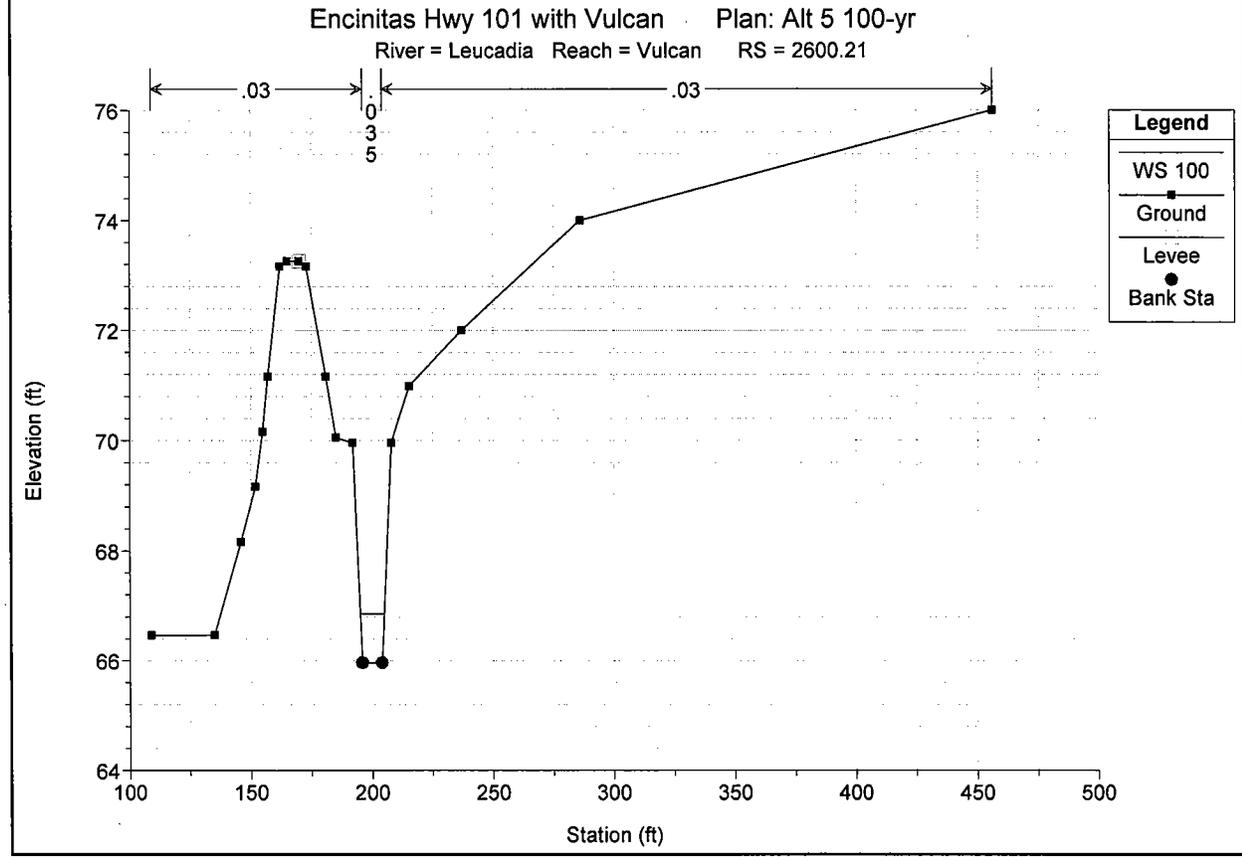
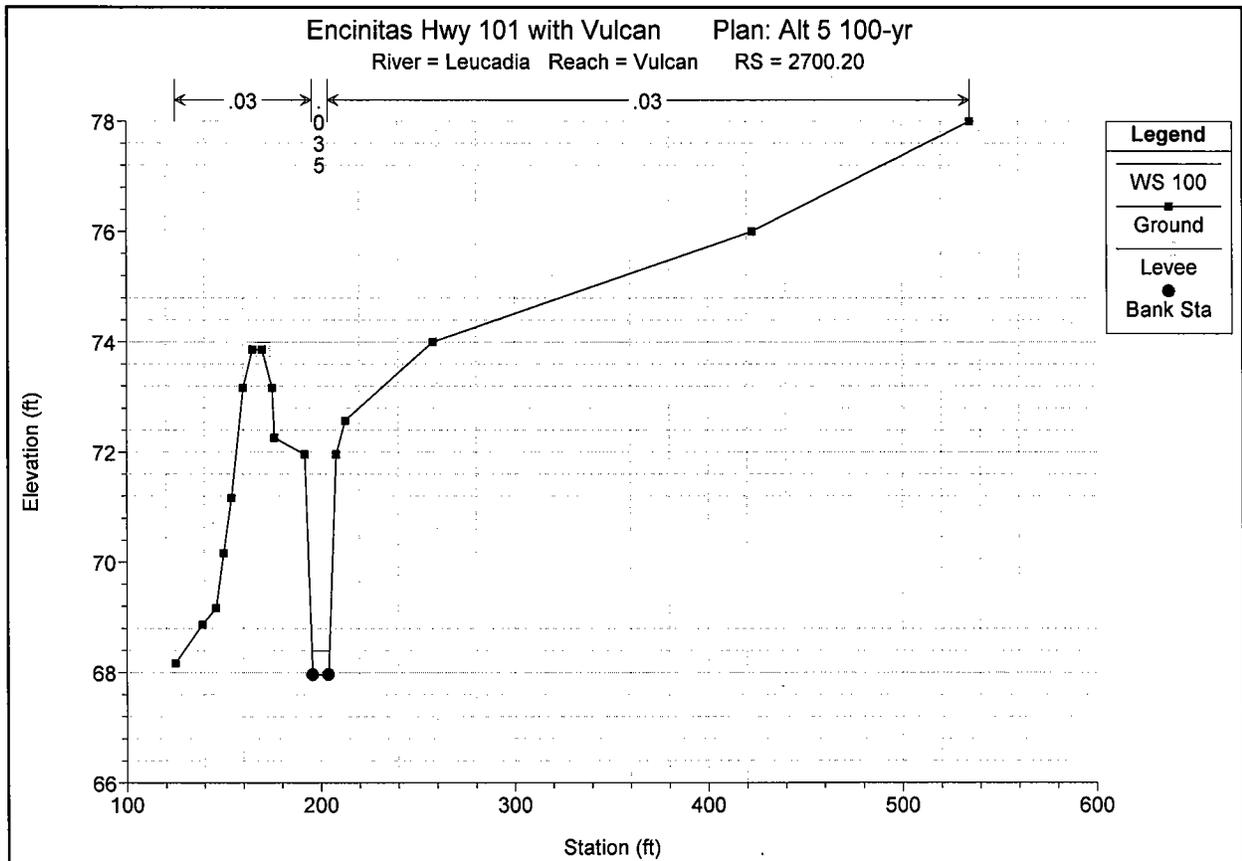
Encinitas Hwy 101 with Vulcan Plan: Alt 5 100-yr

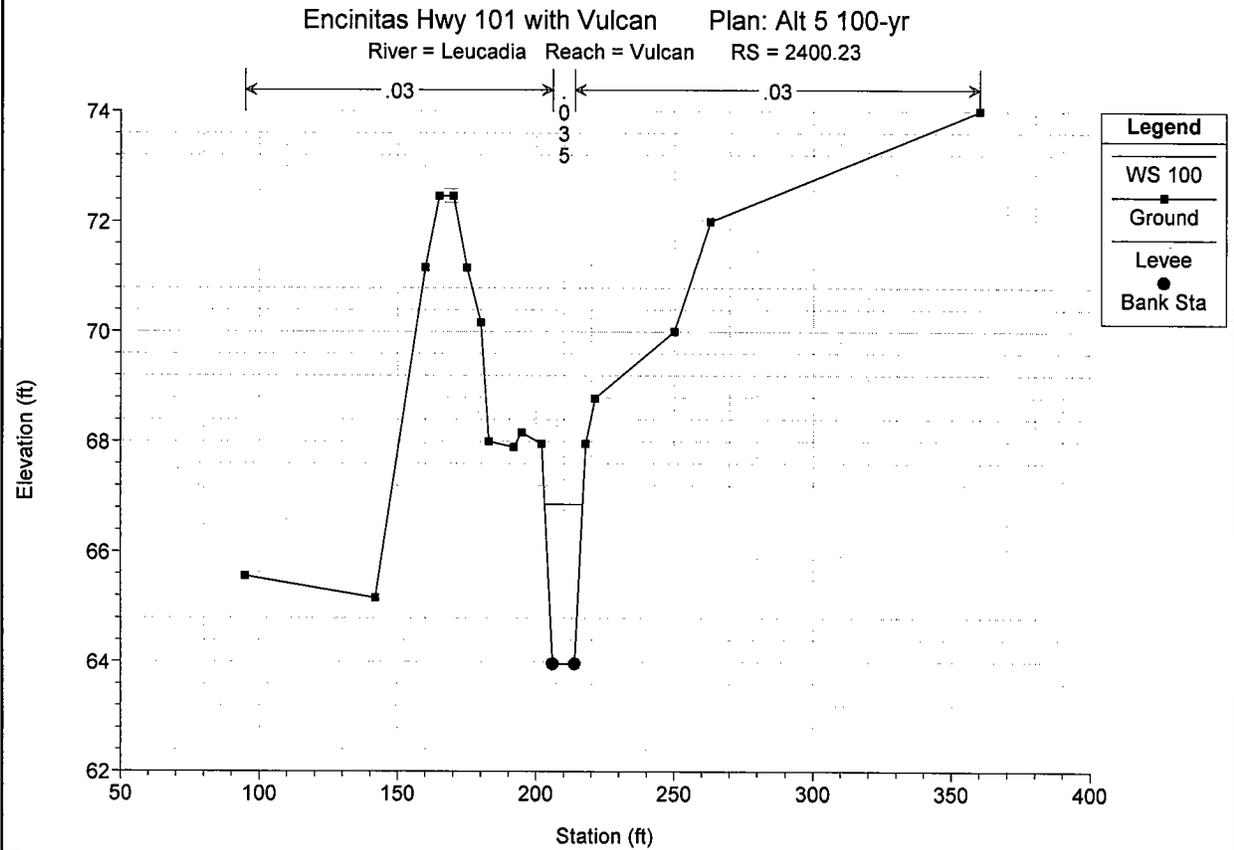
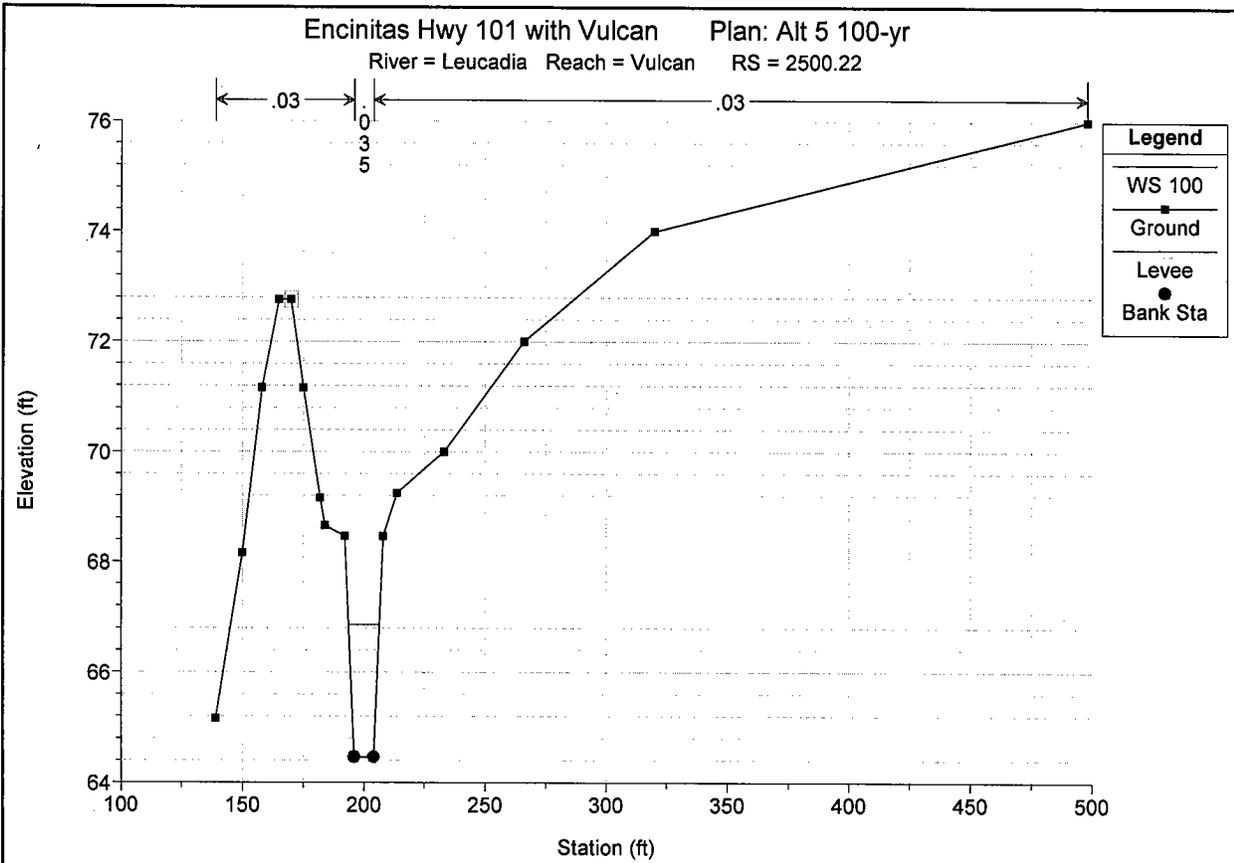


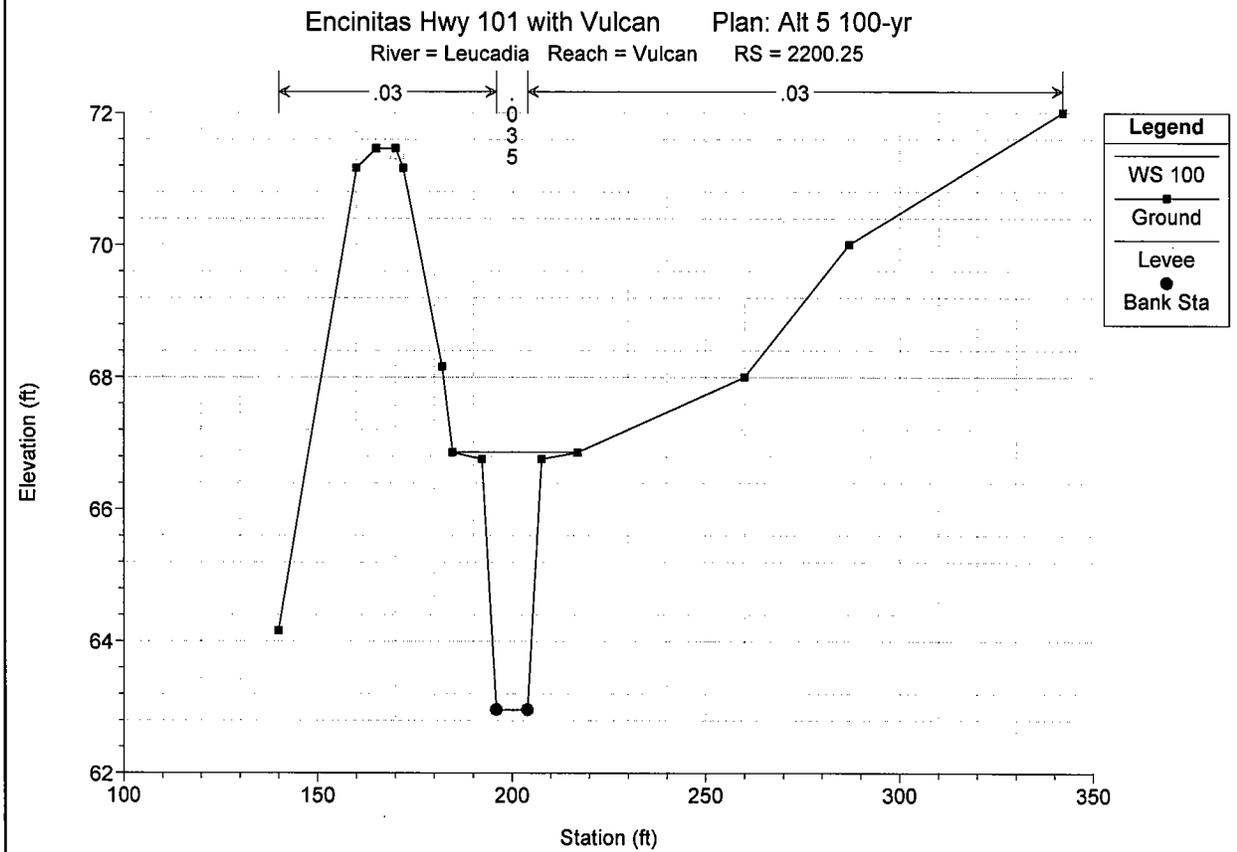
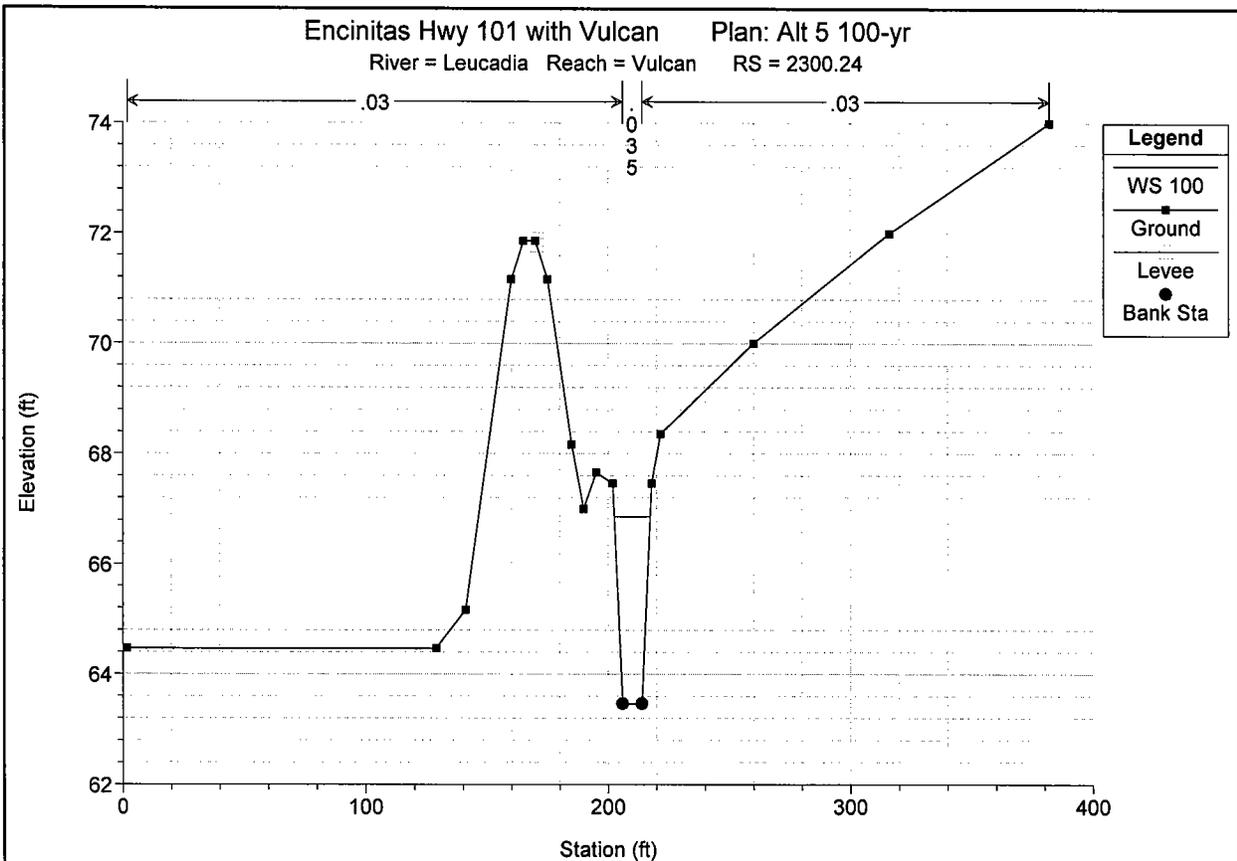


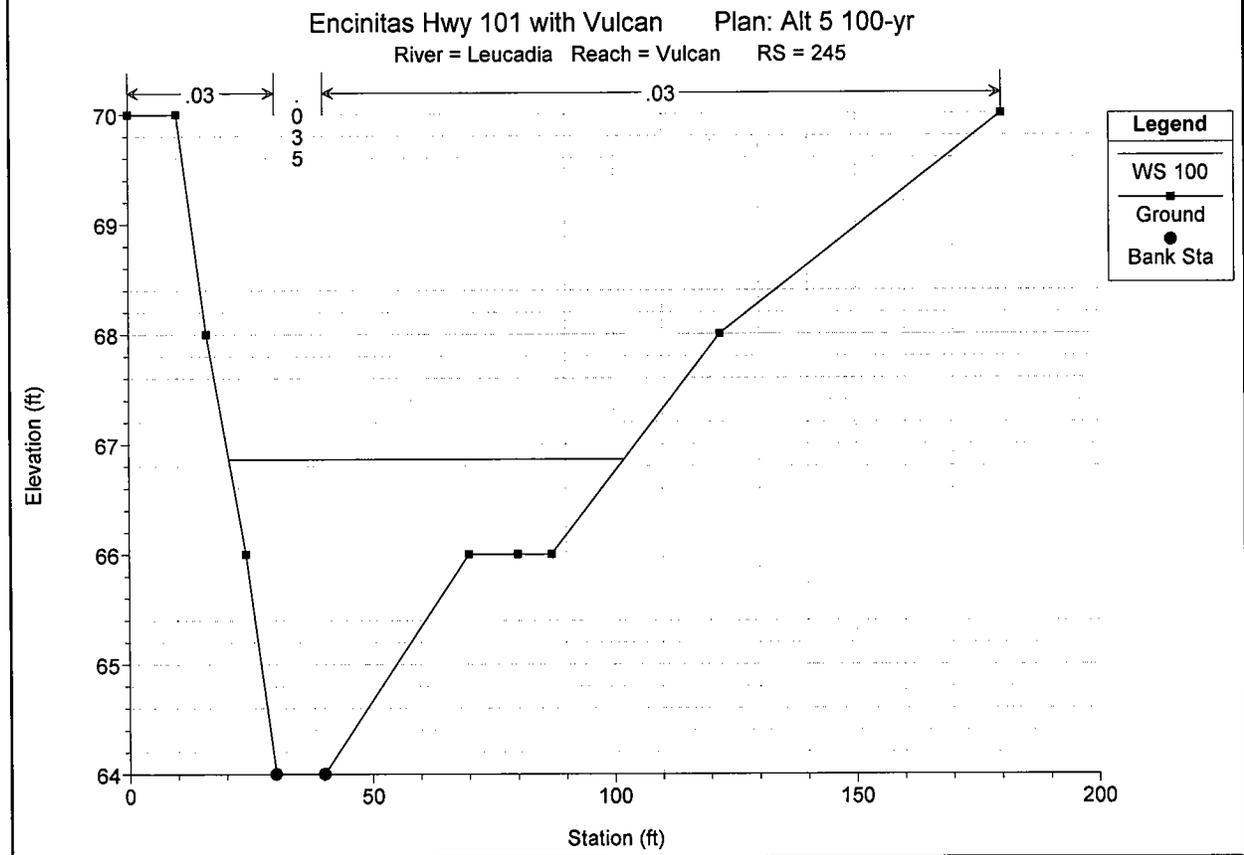
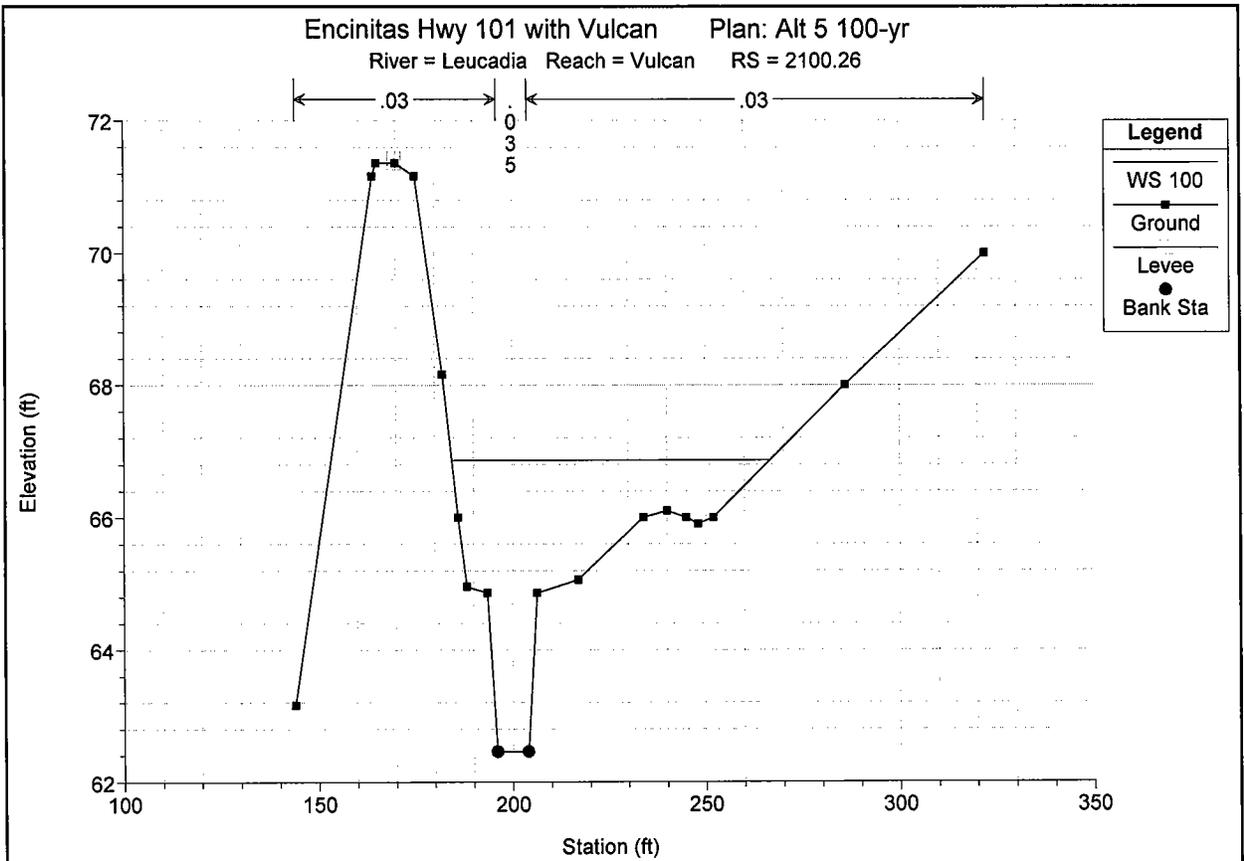


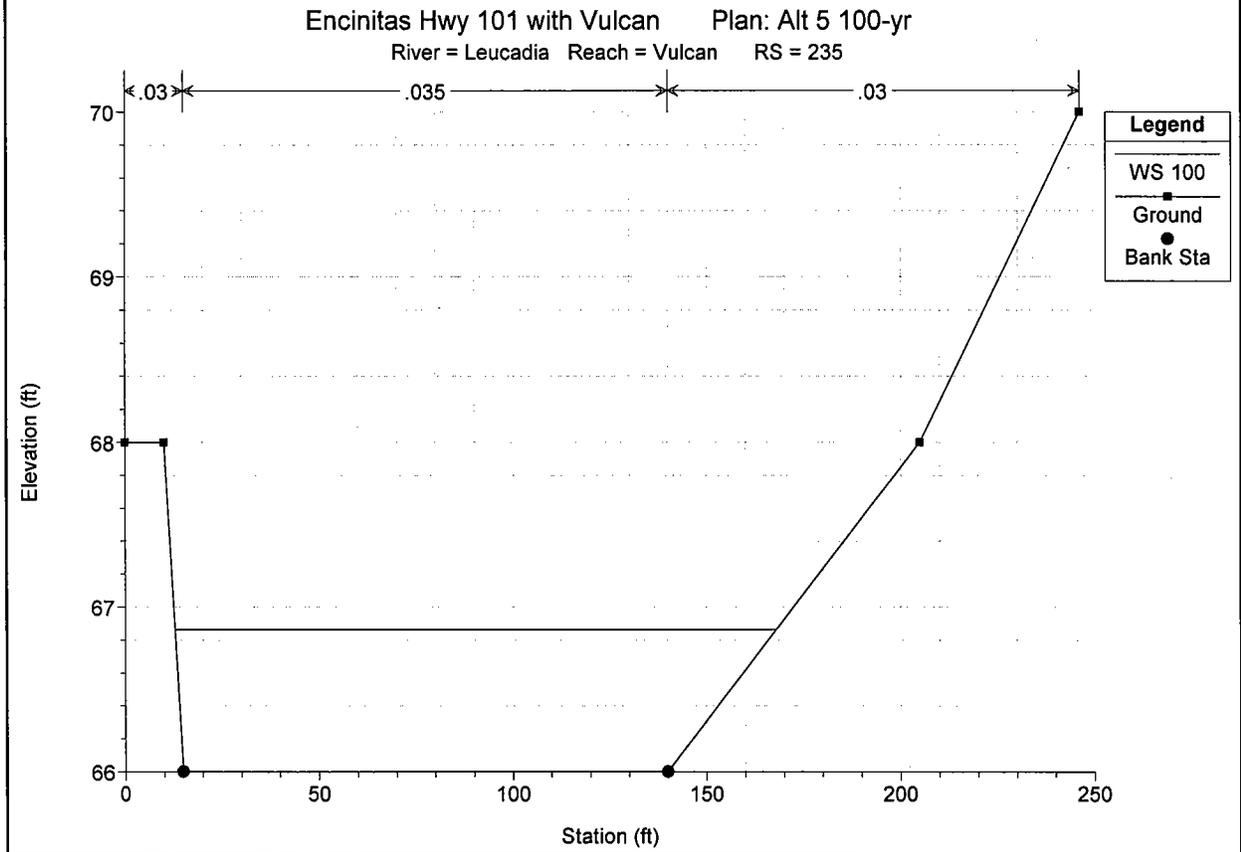
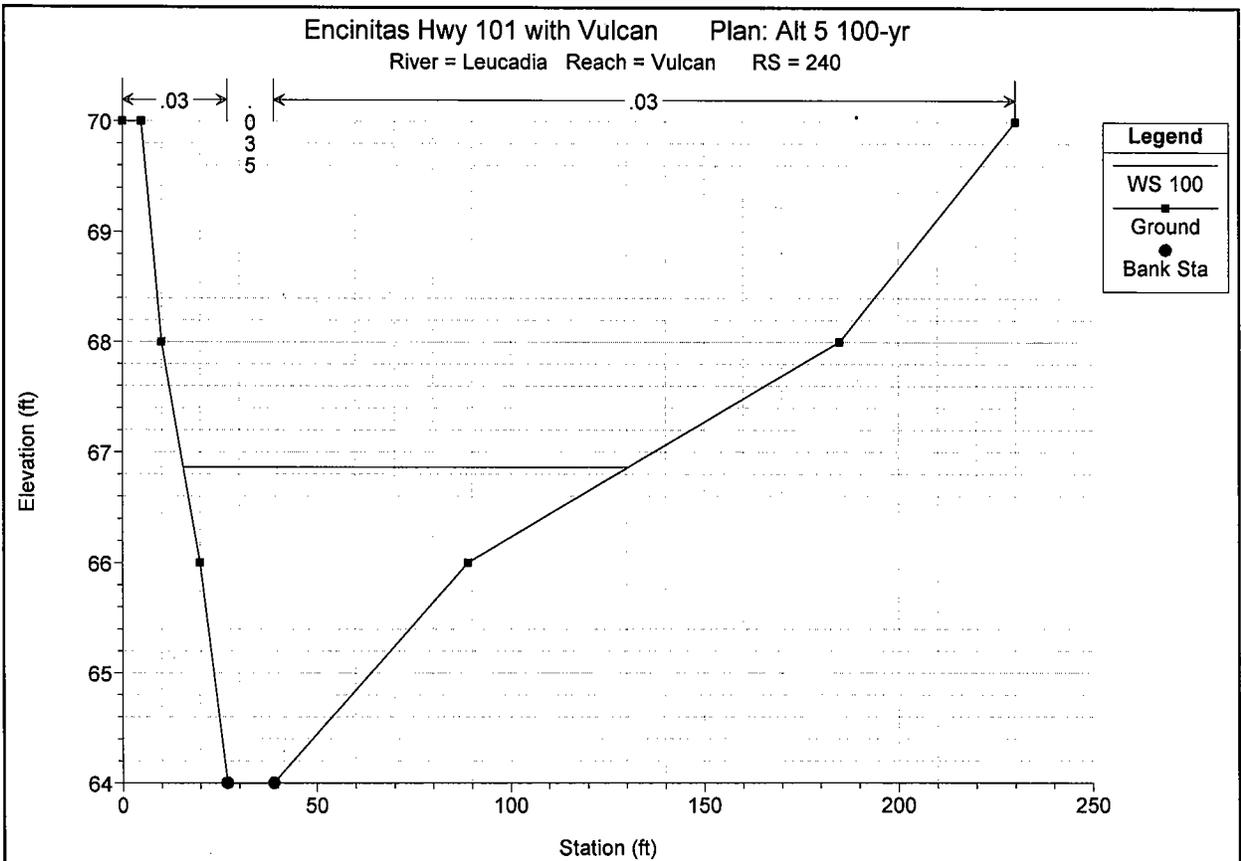


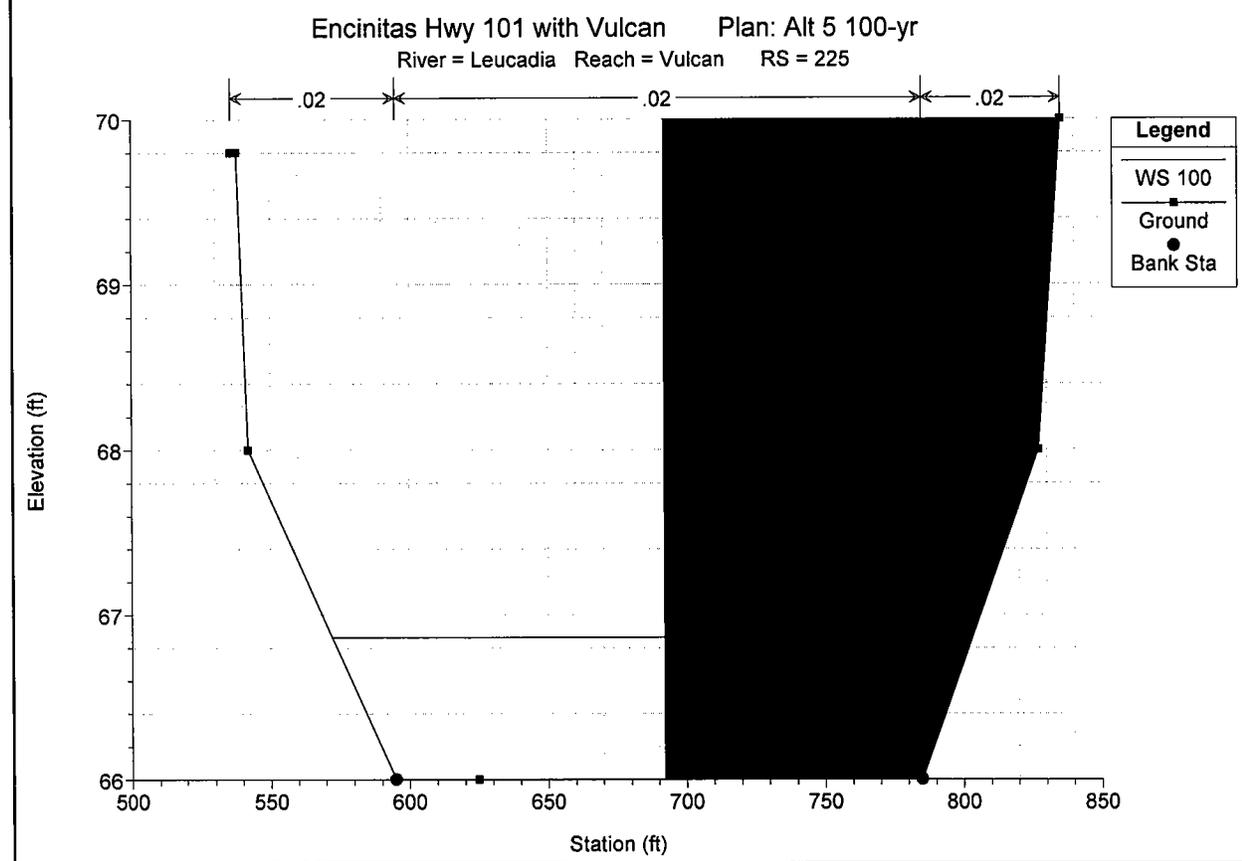
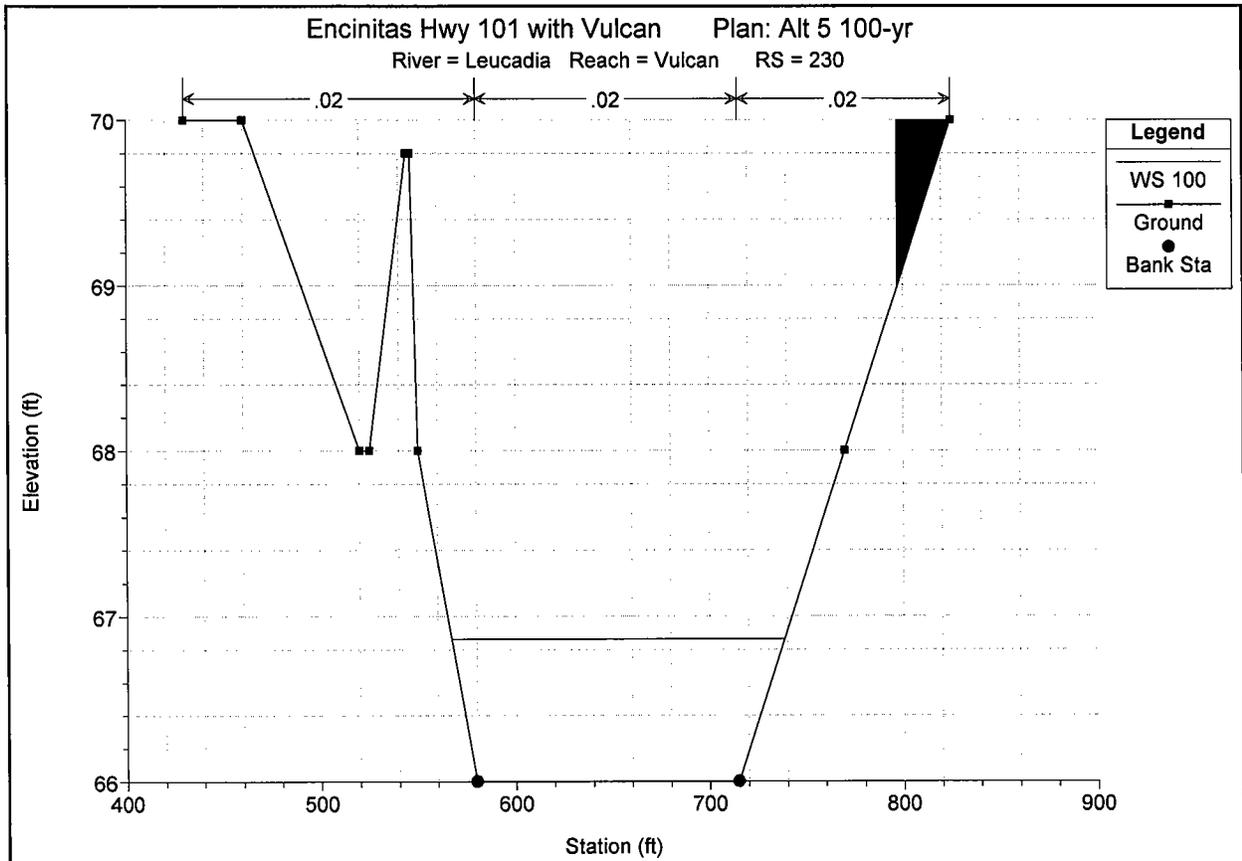


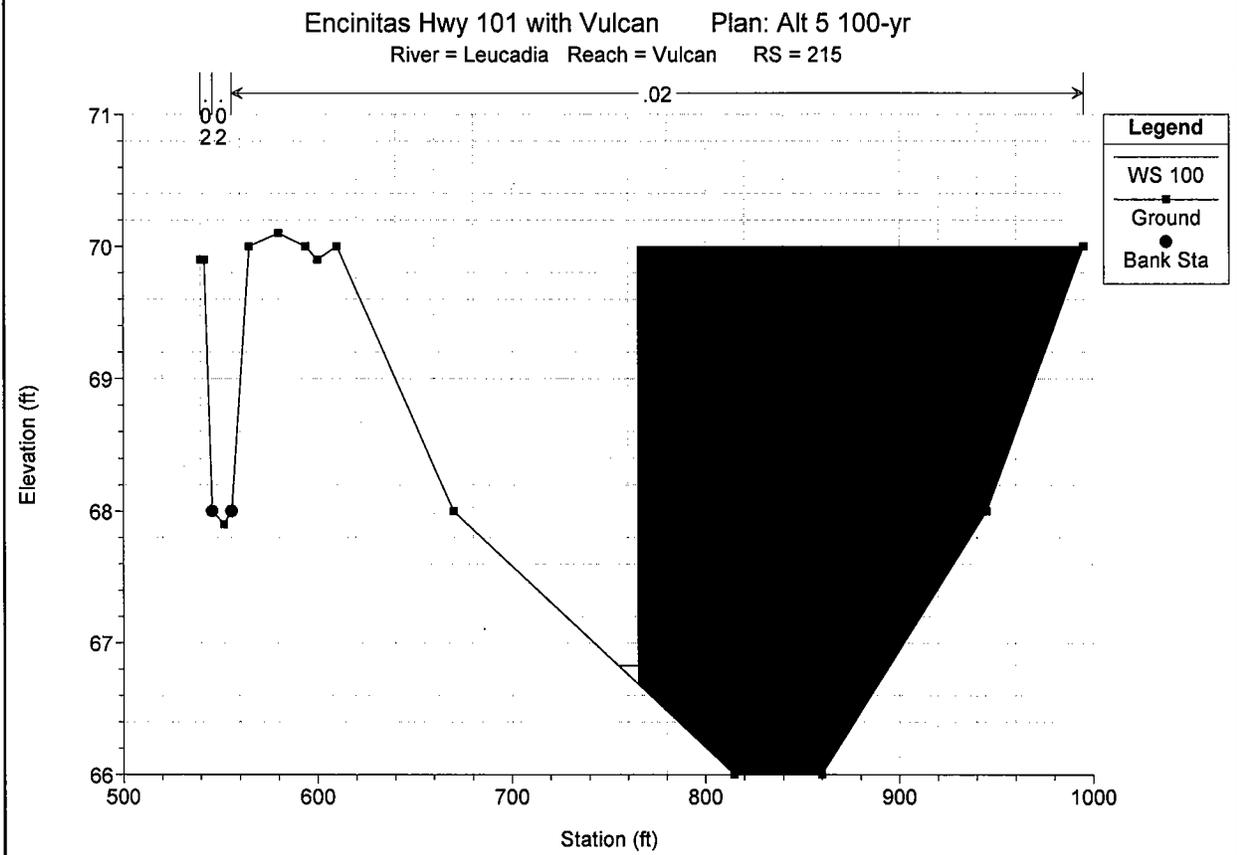
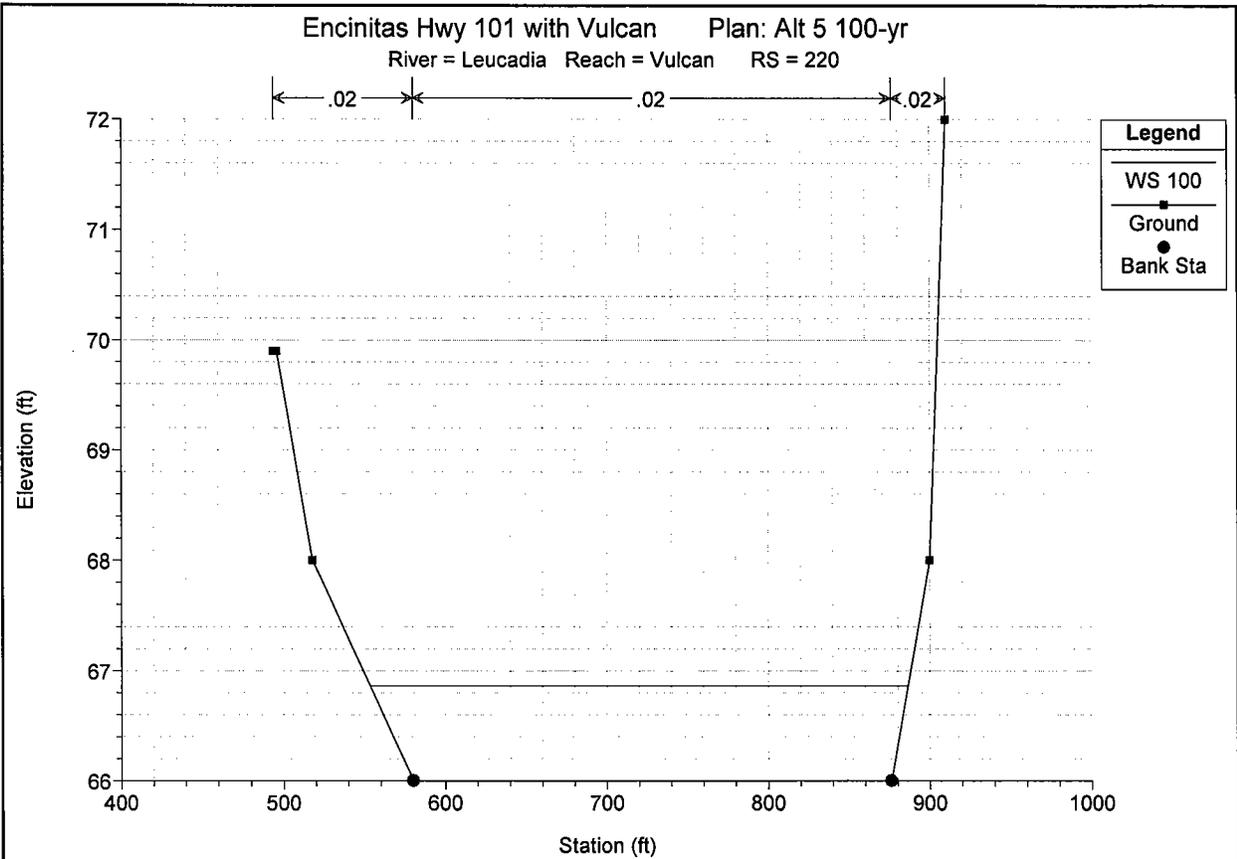


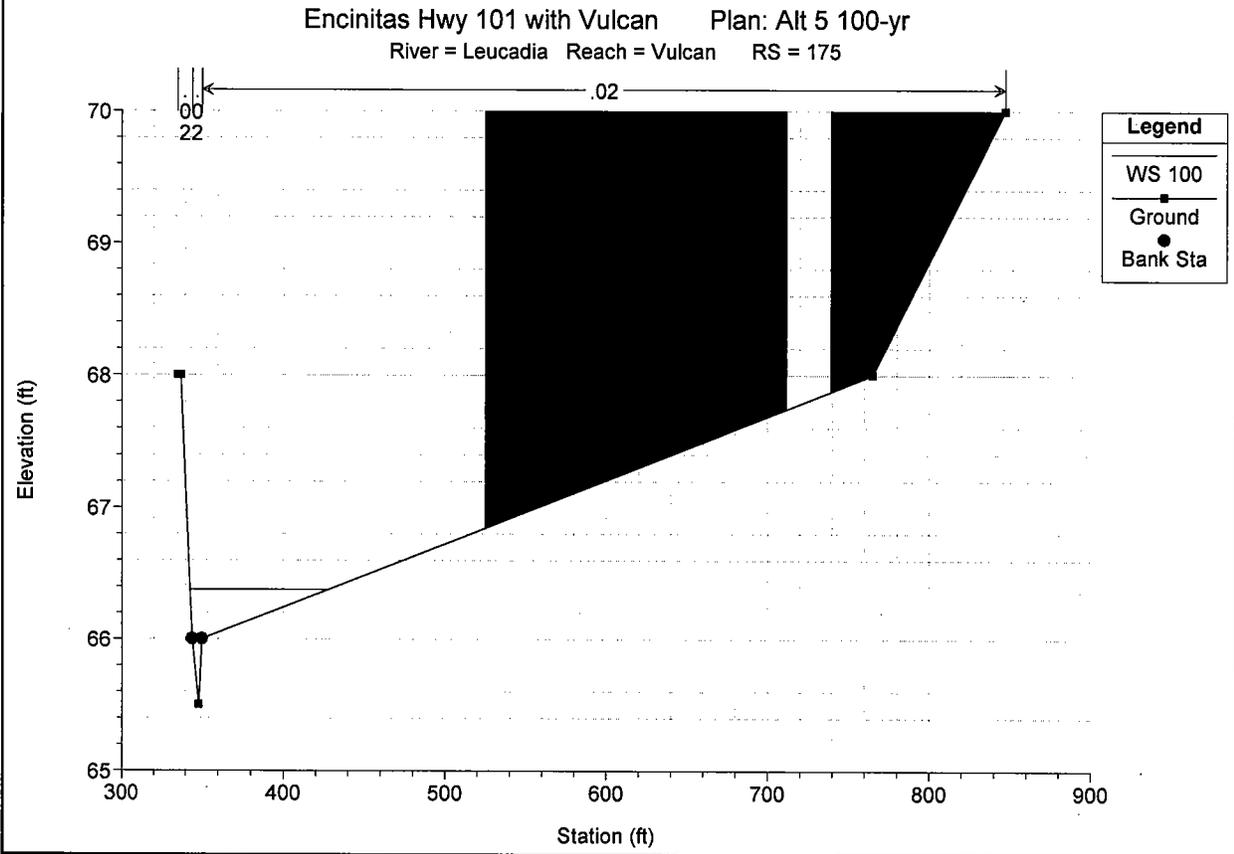
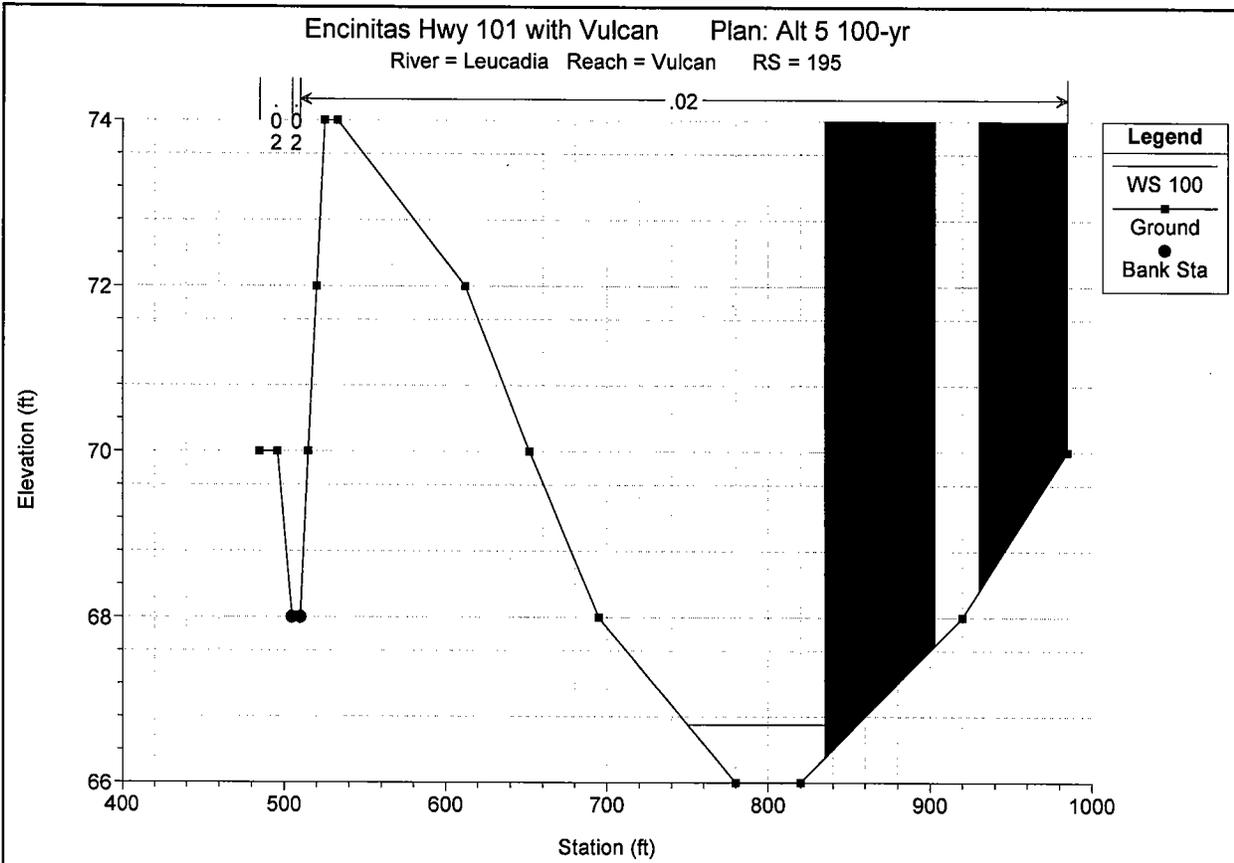


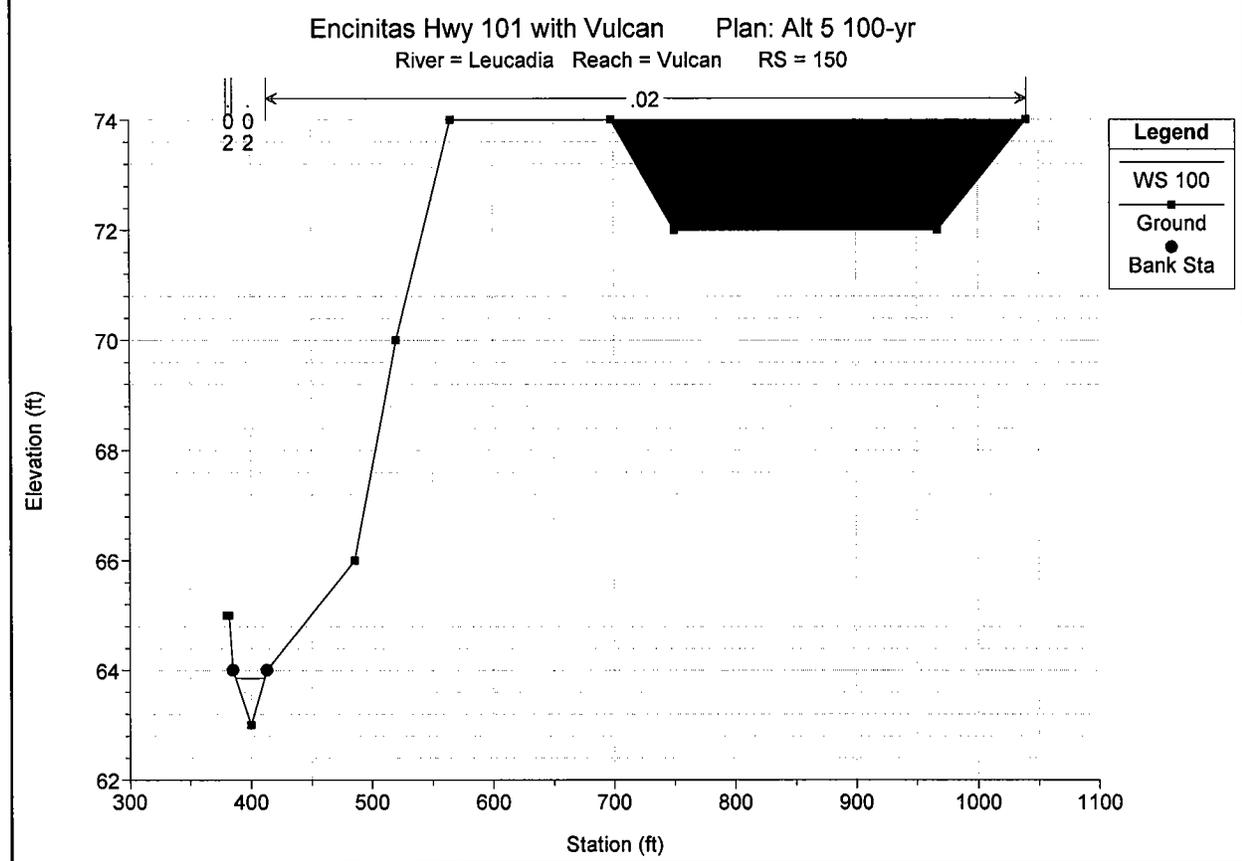
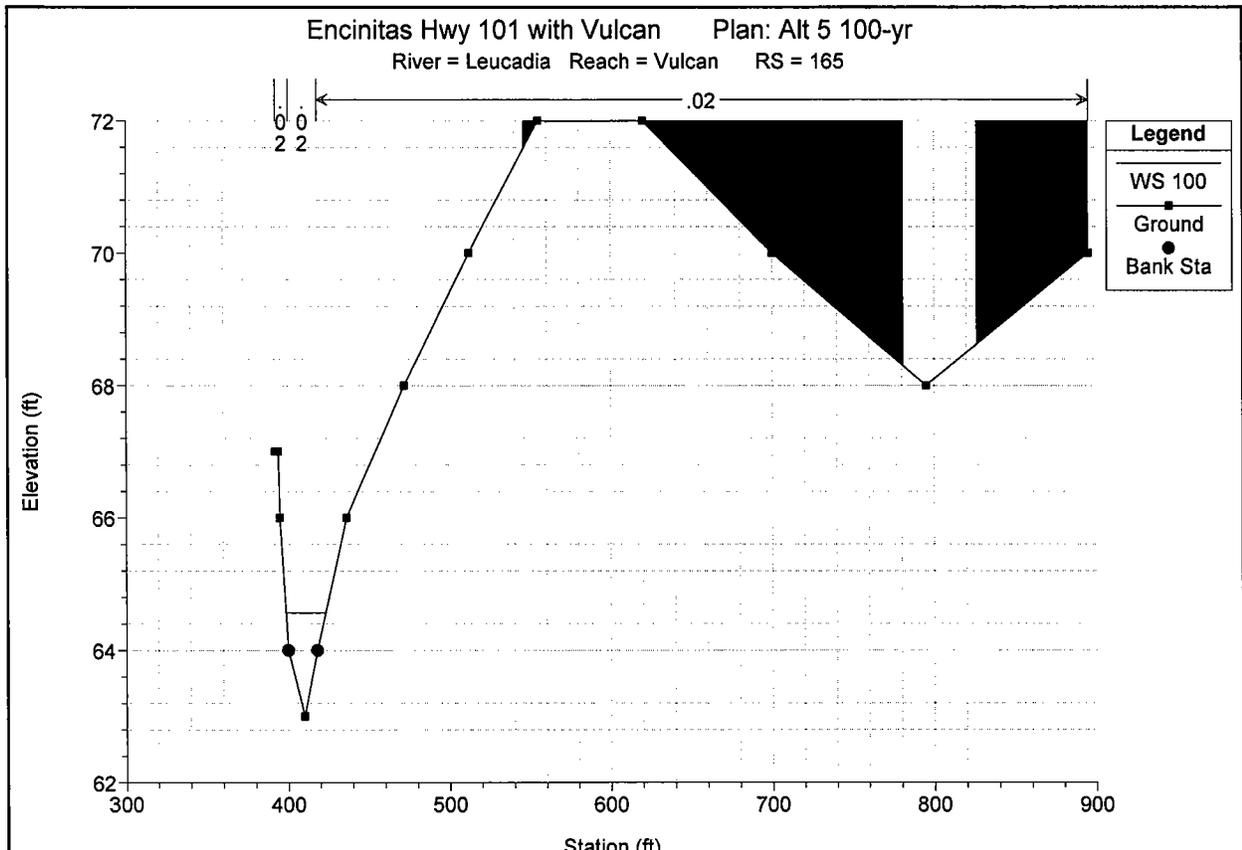


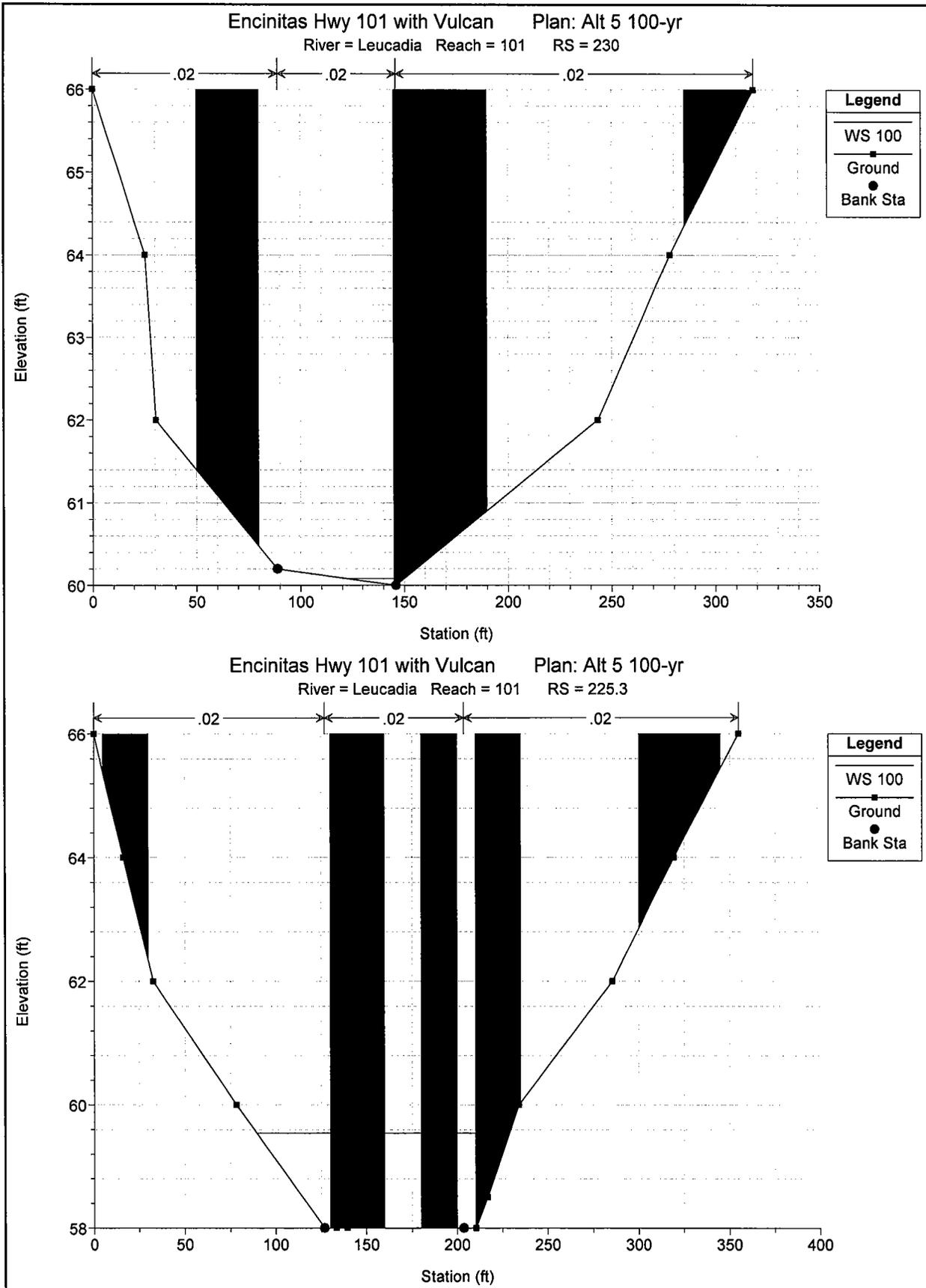


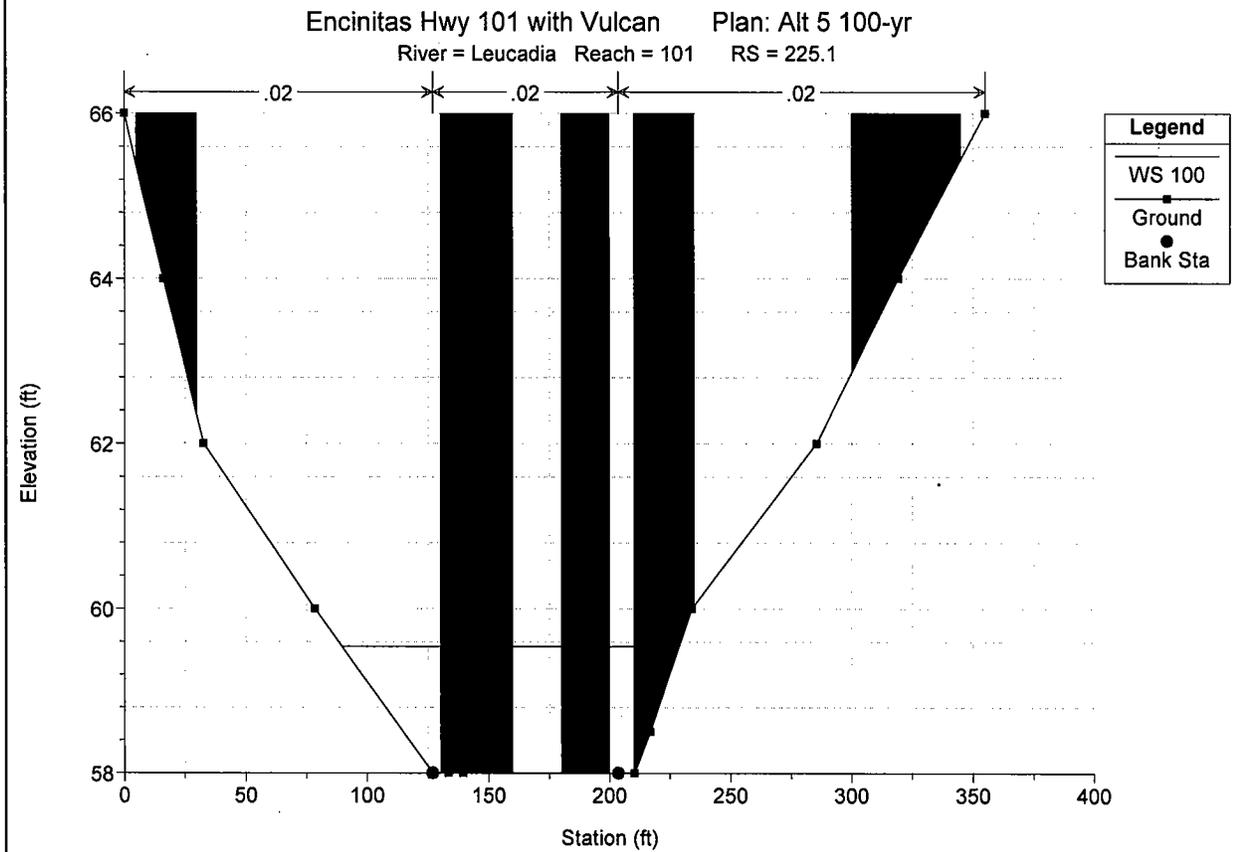
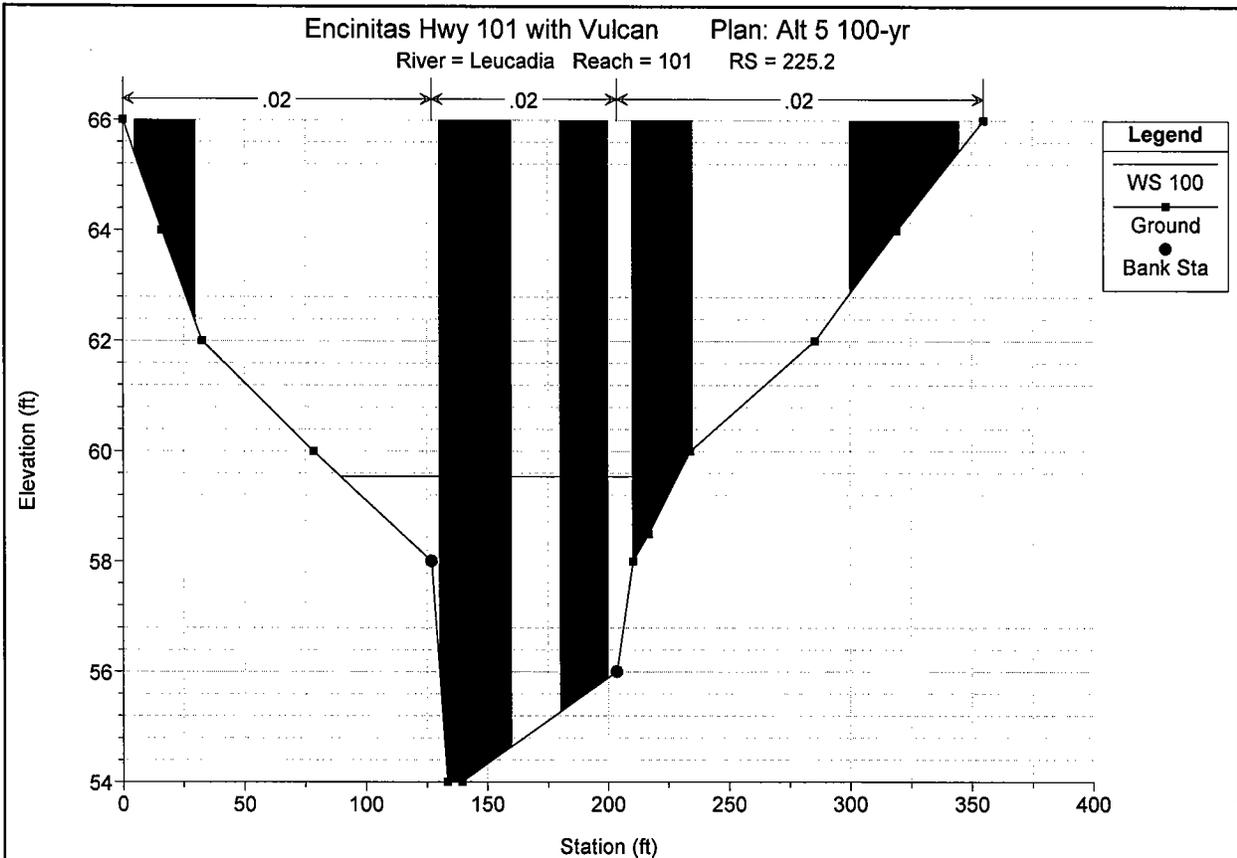




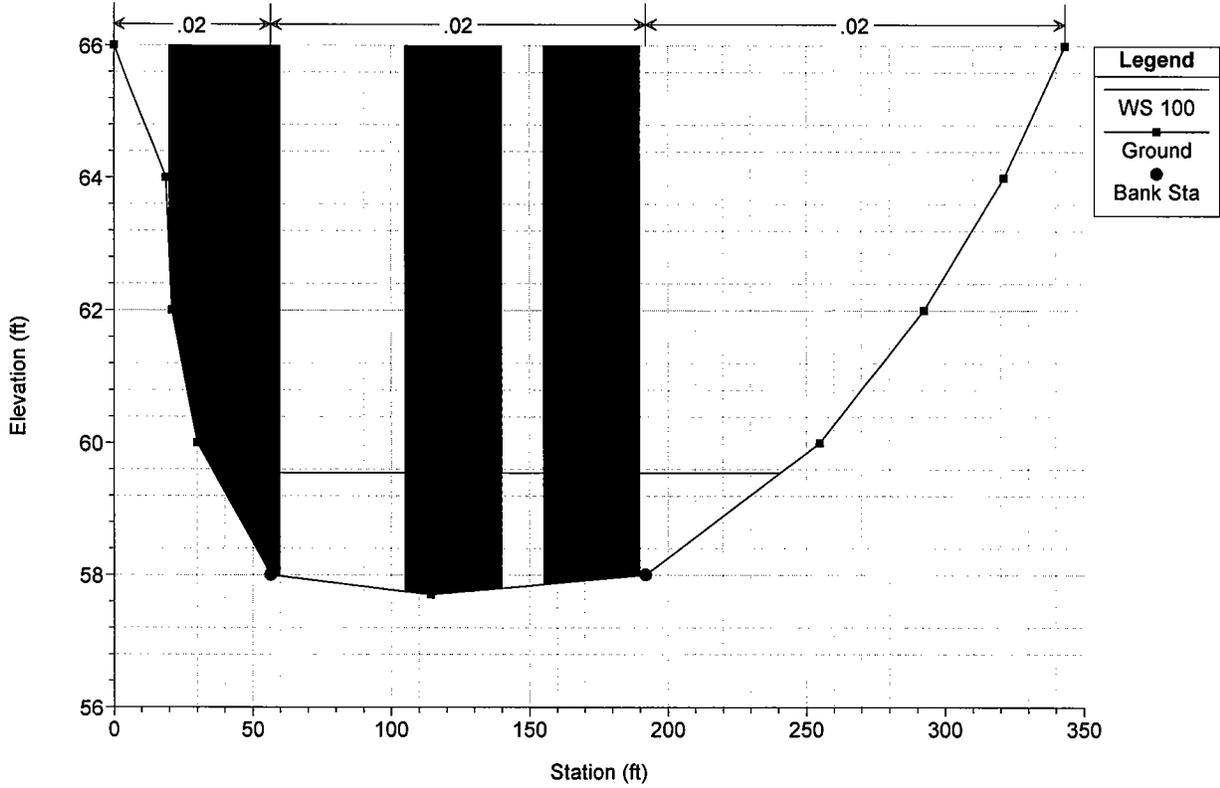




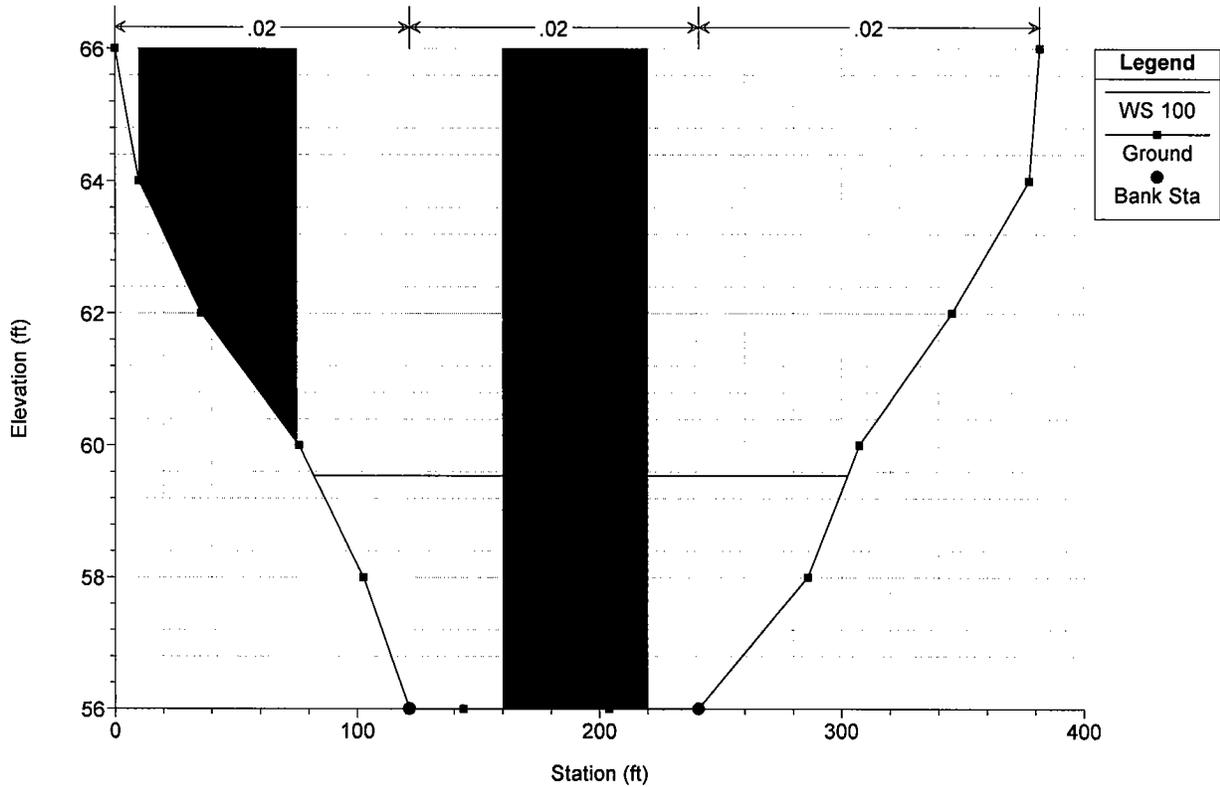


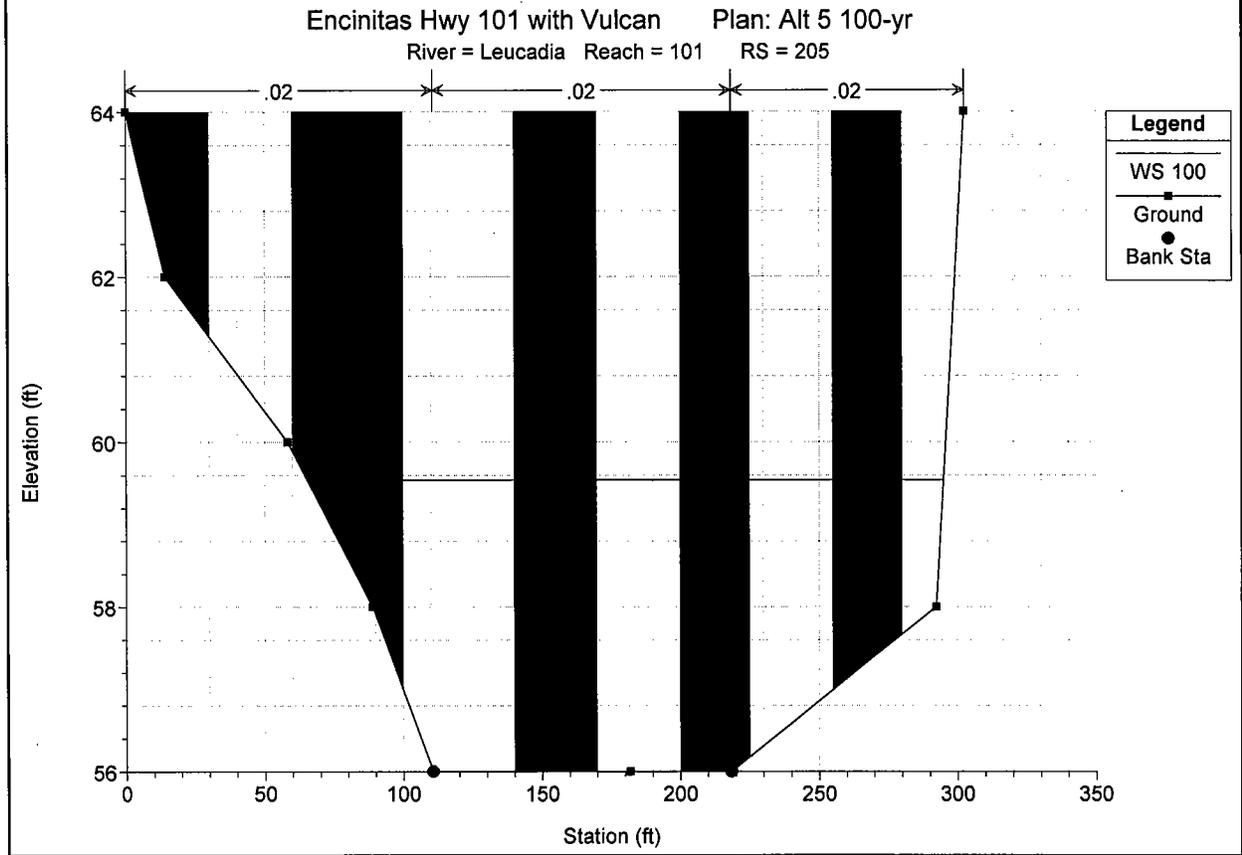
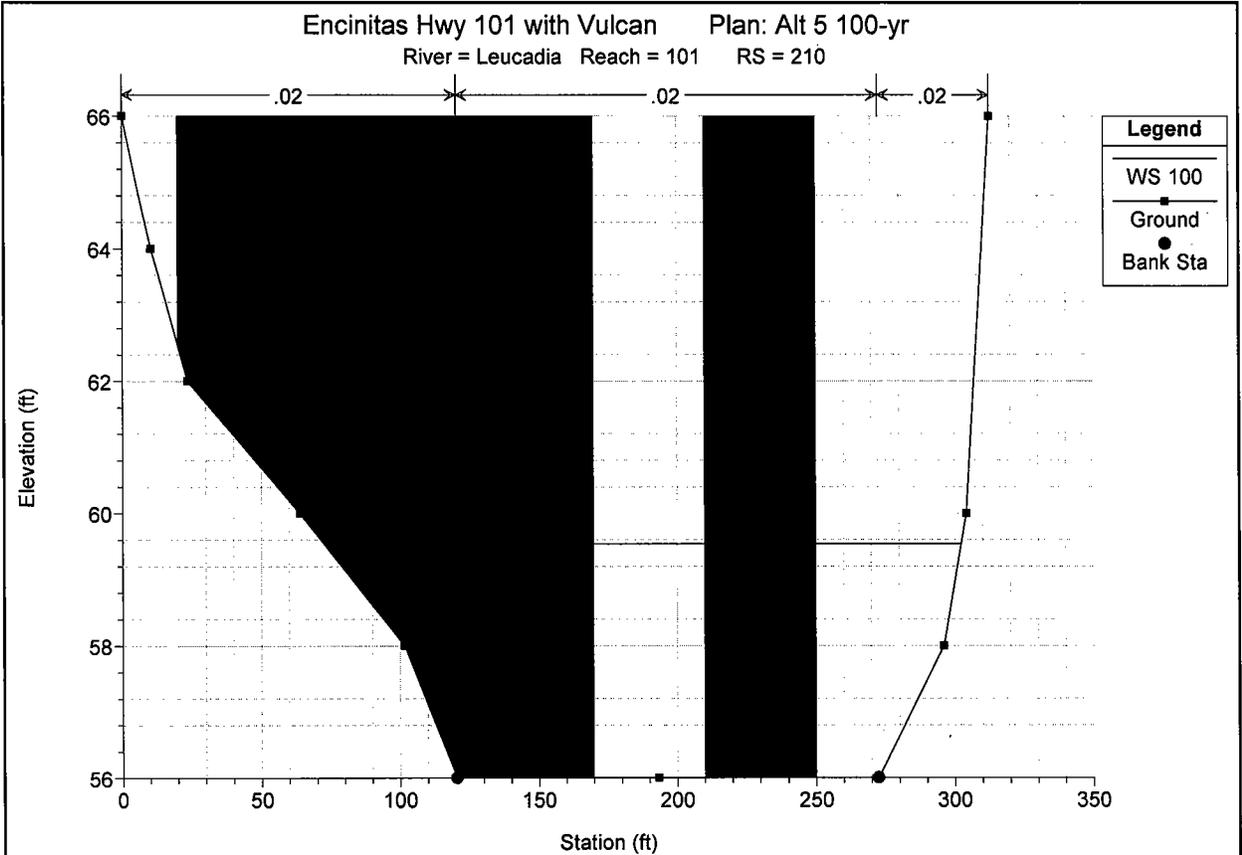


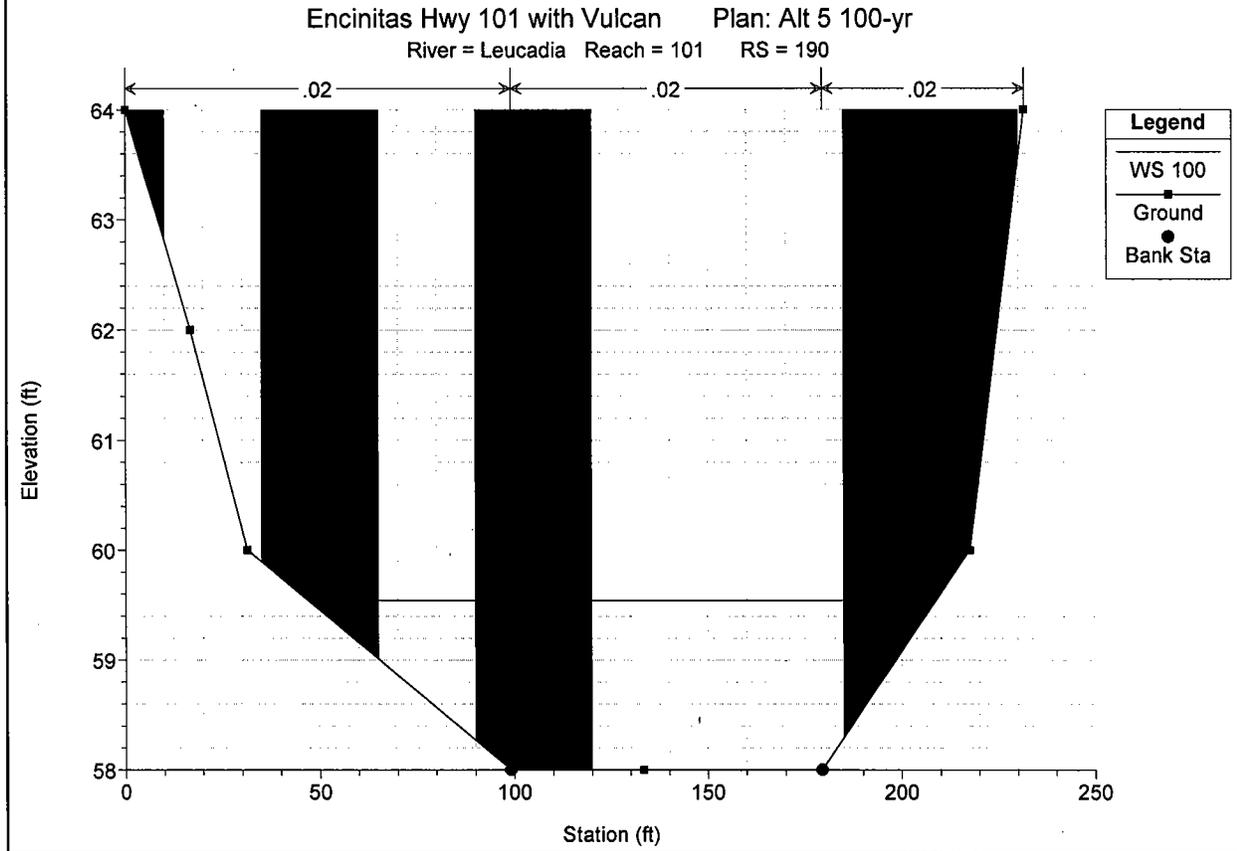
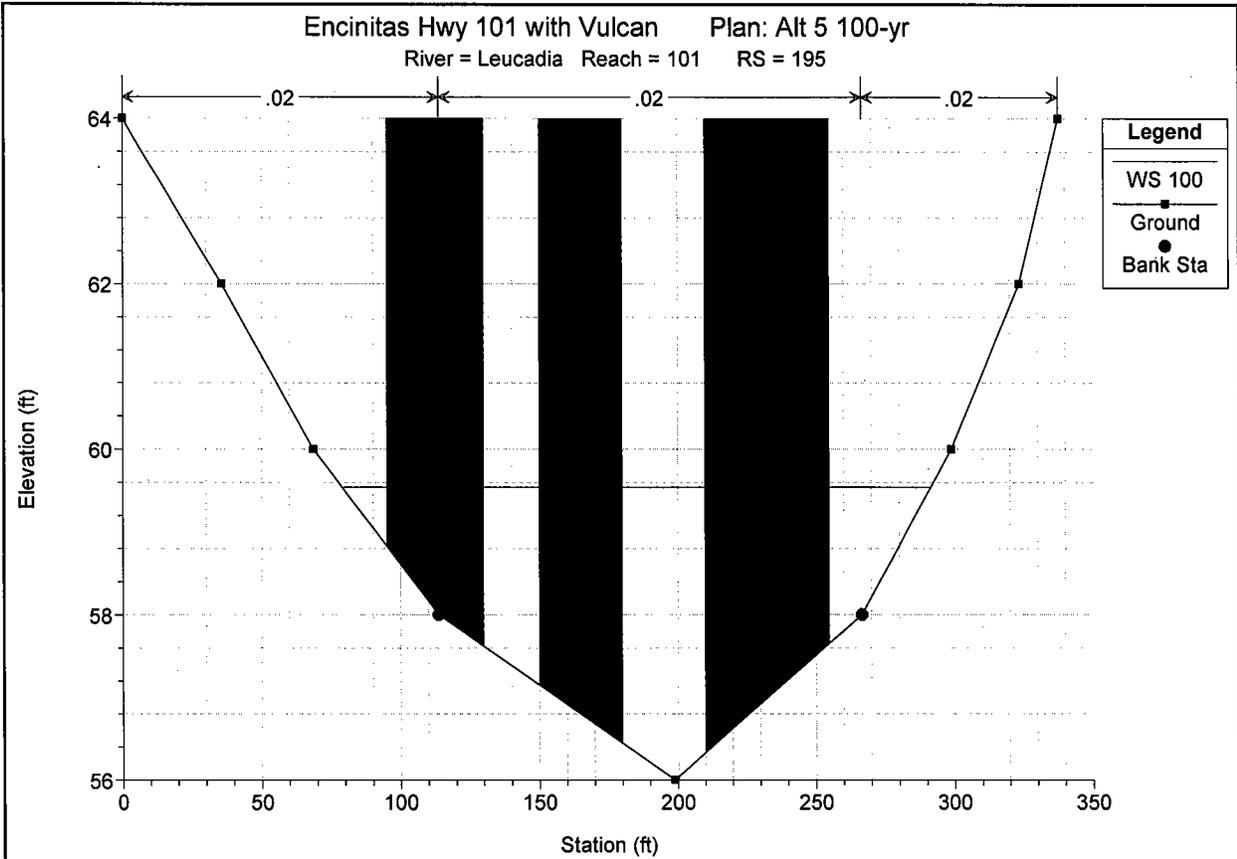
Encinitas Hwy 101 with Vulcan Plan: Alt 5 100-yr  
 River = Leucadia Reach = 101 RS = 220

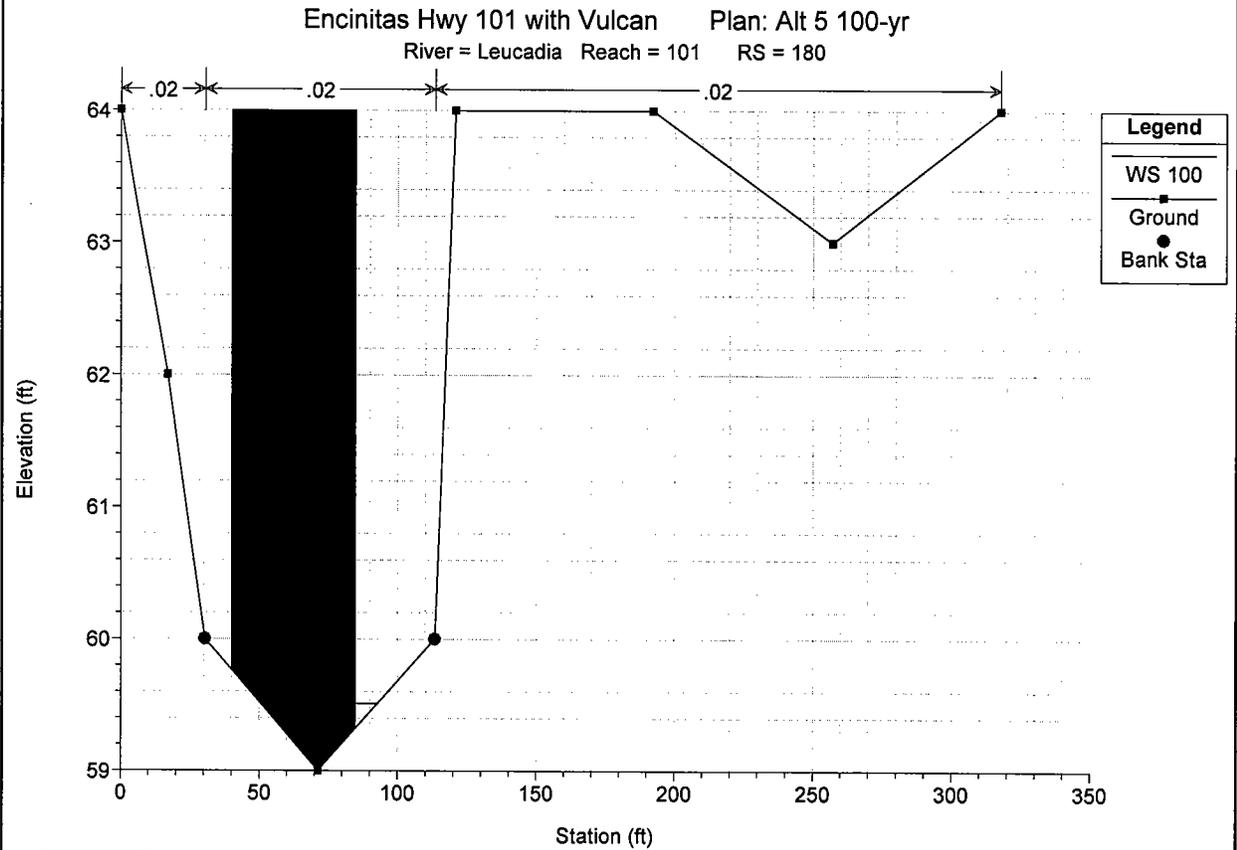
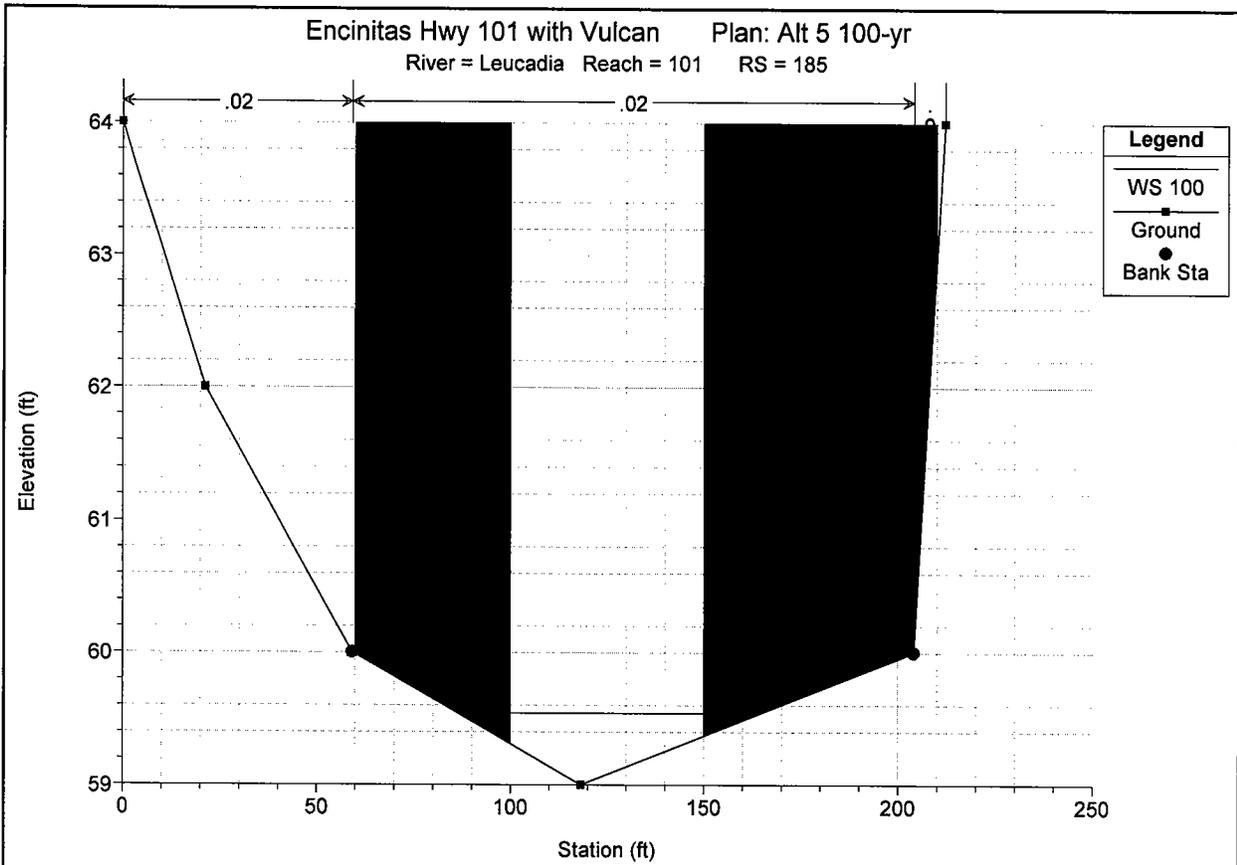


Encinitas Hwy 101 with Vulcan Plan: Alt 5 100-yr  
 River = Leucadia Reach = 101 RS = 215



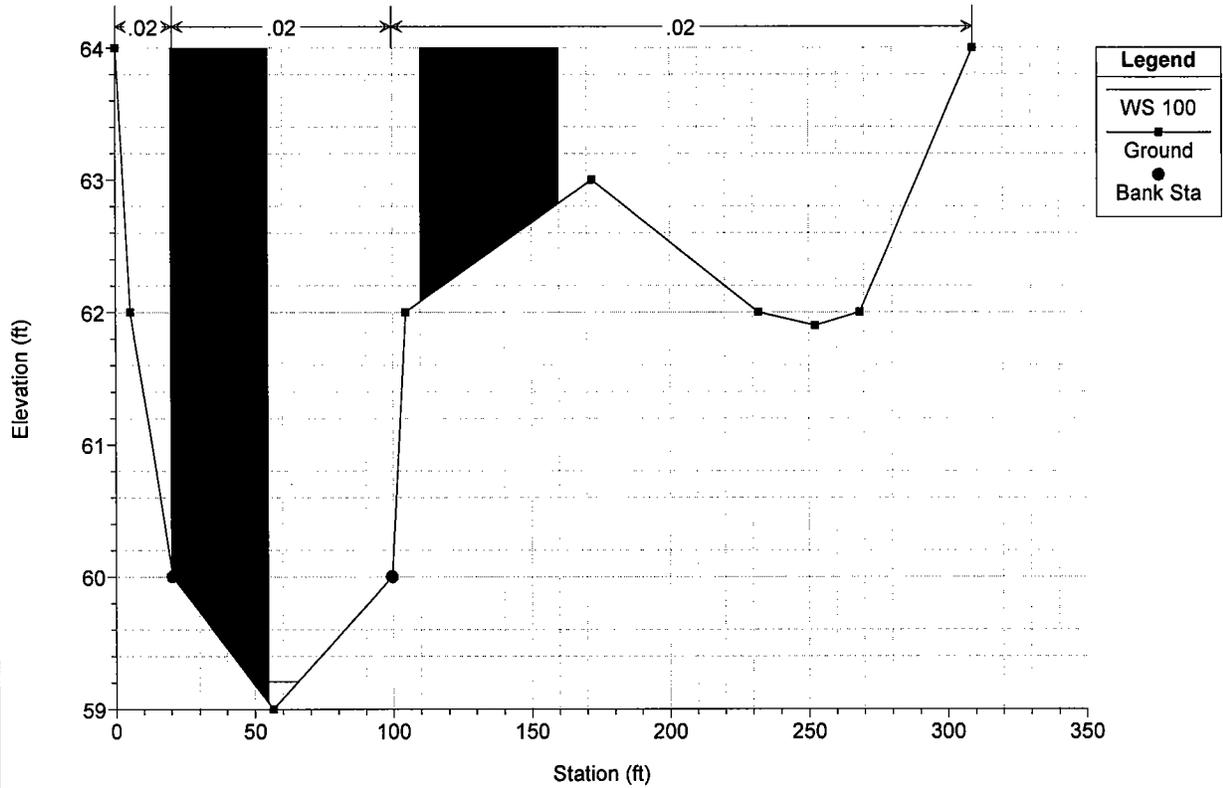






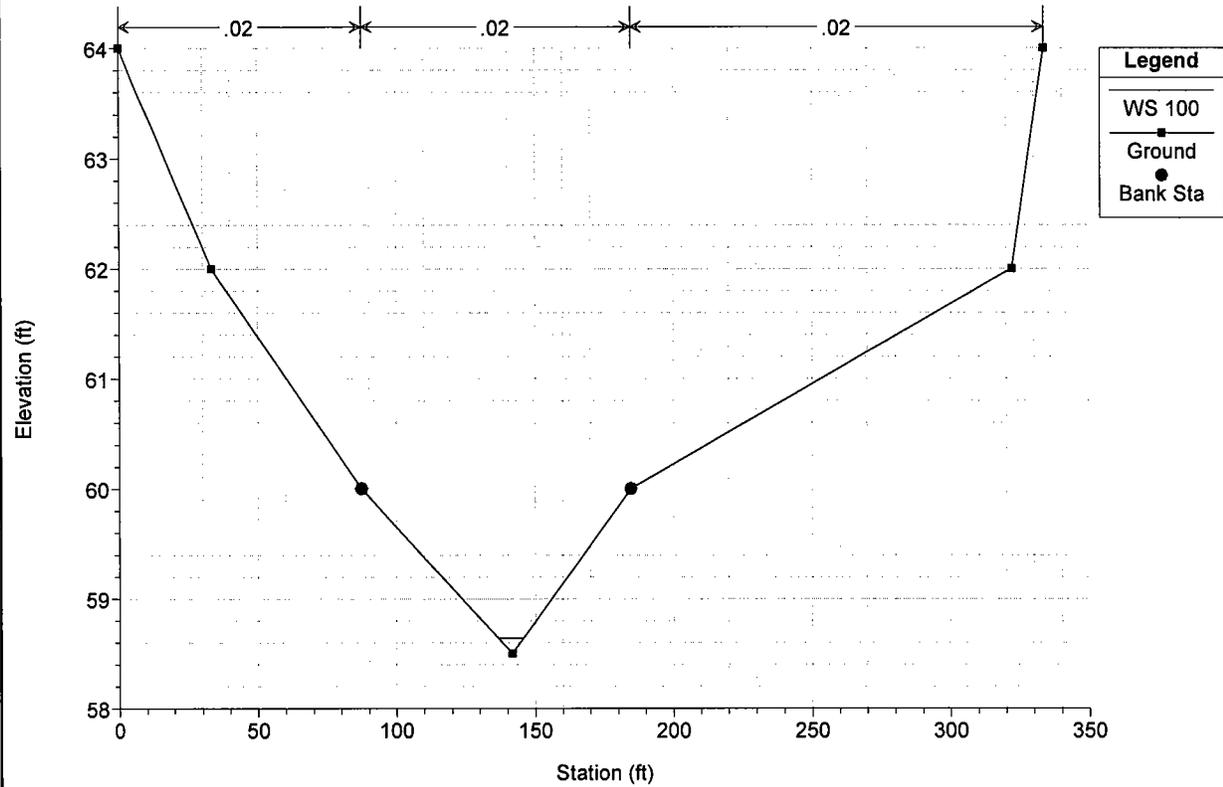
Encinitas Hwy 101 with Vulcan Plan: Alt 5 100-yr

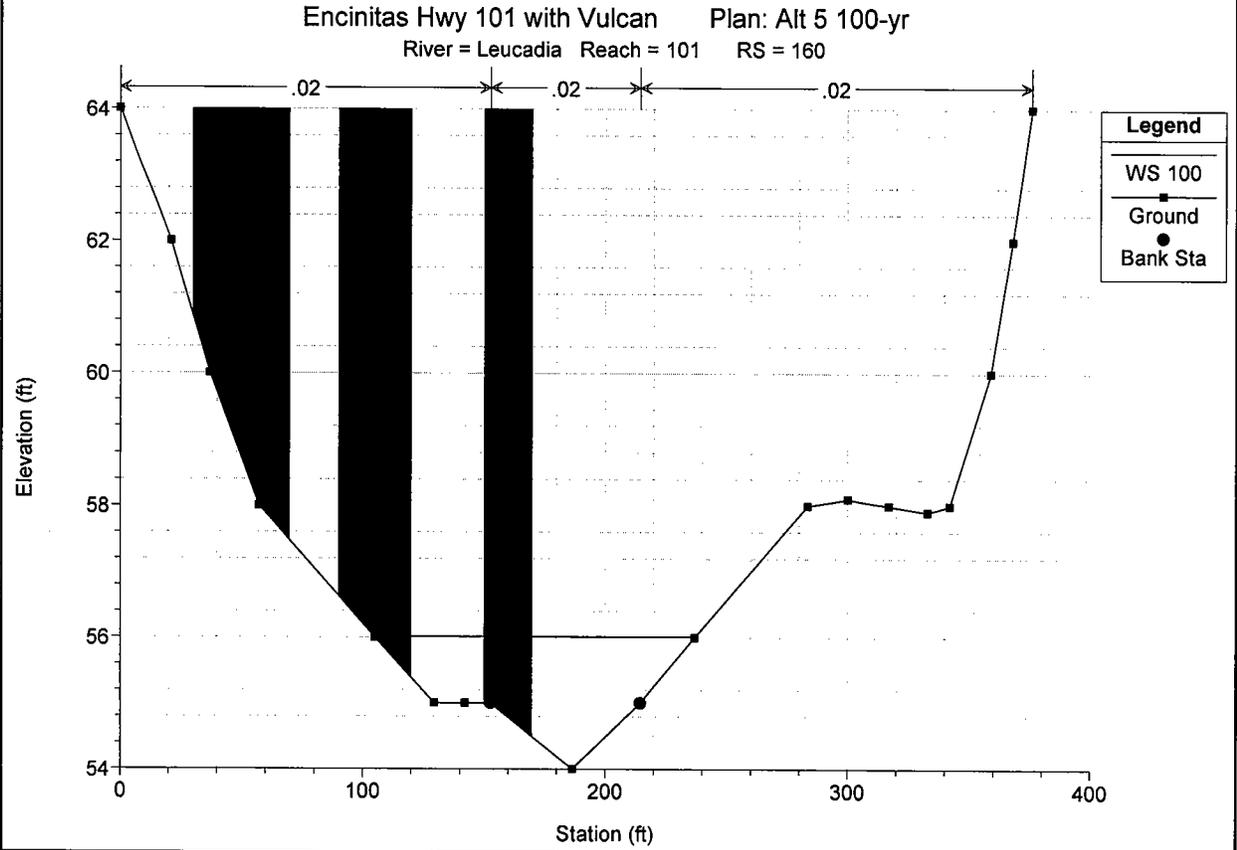
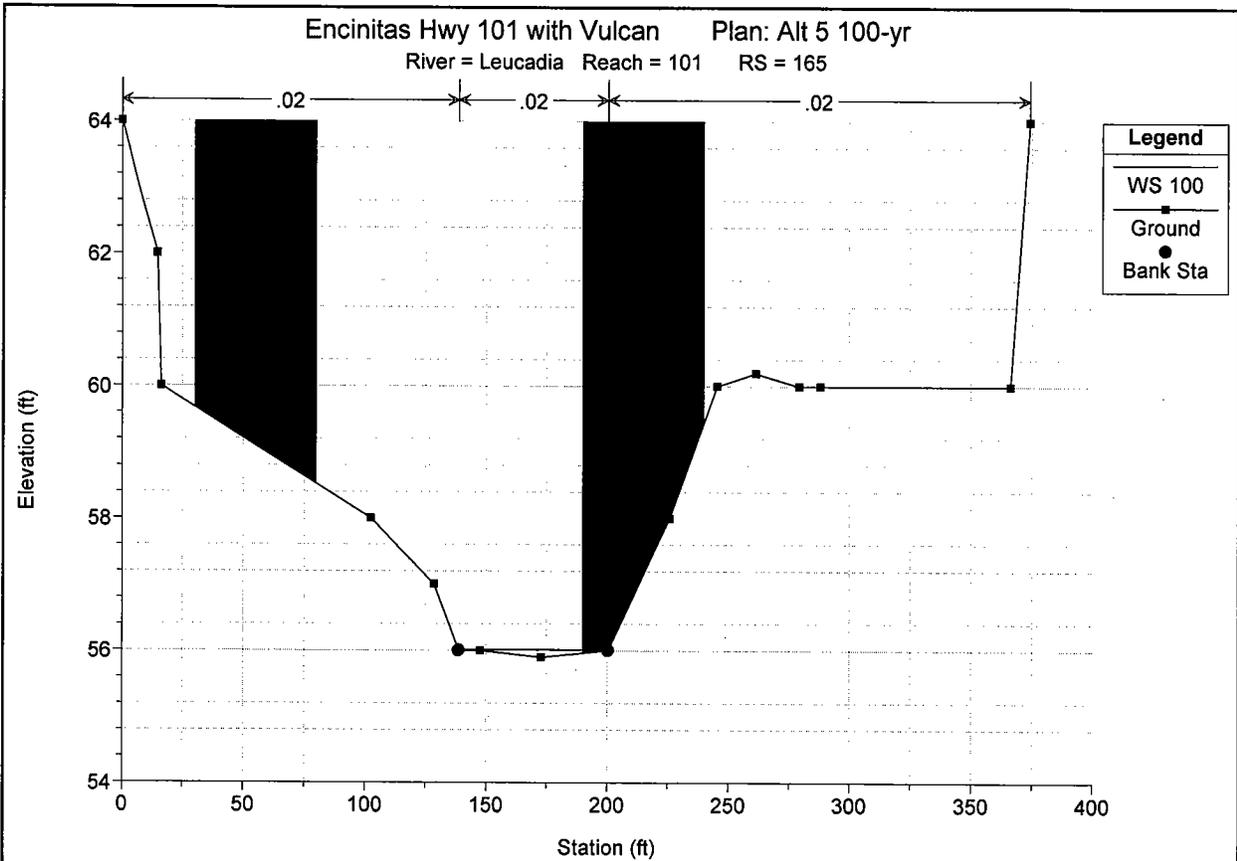
River = Leucadia Reach = 101 RS = 175

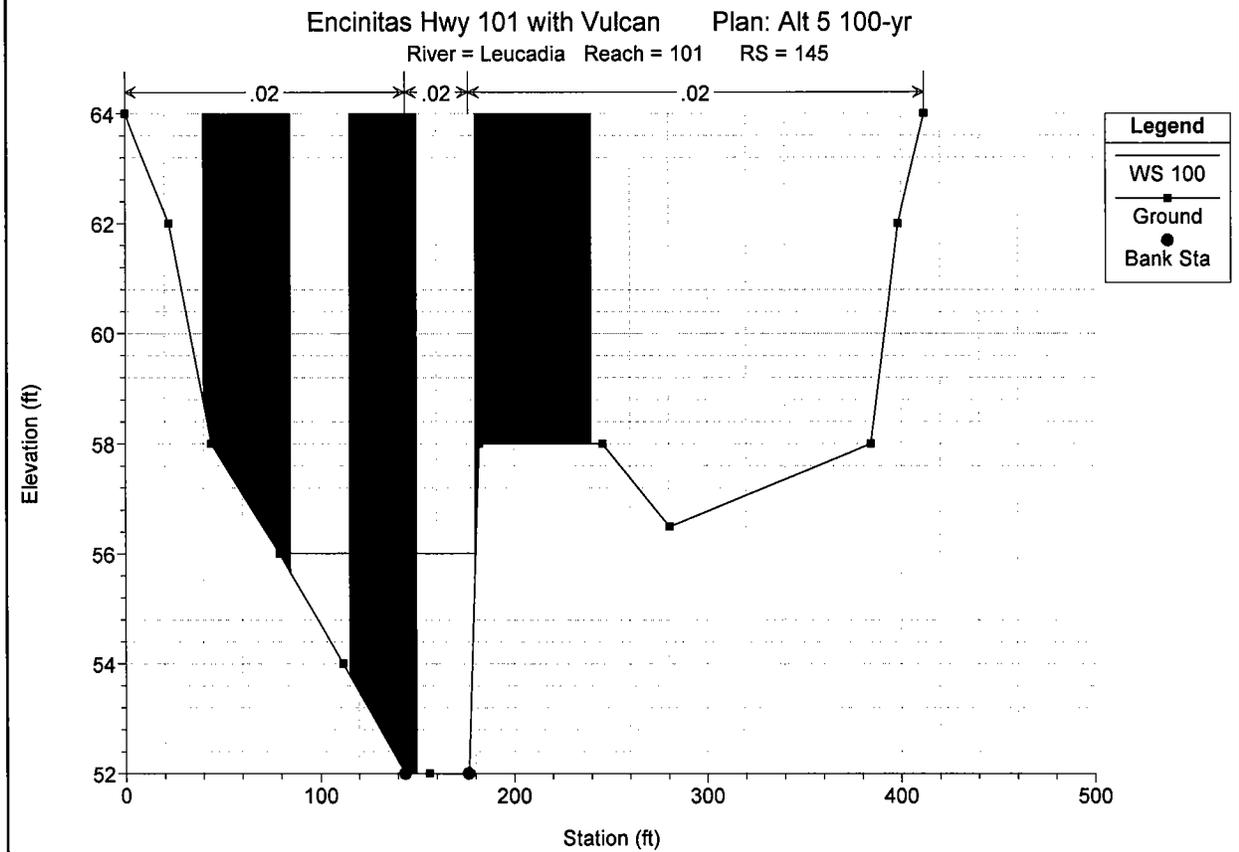
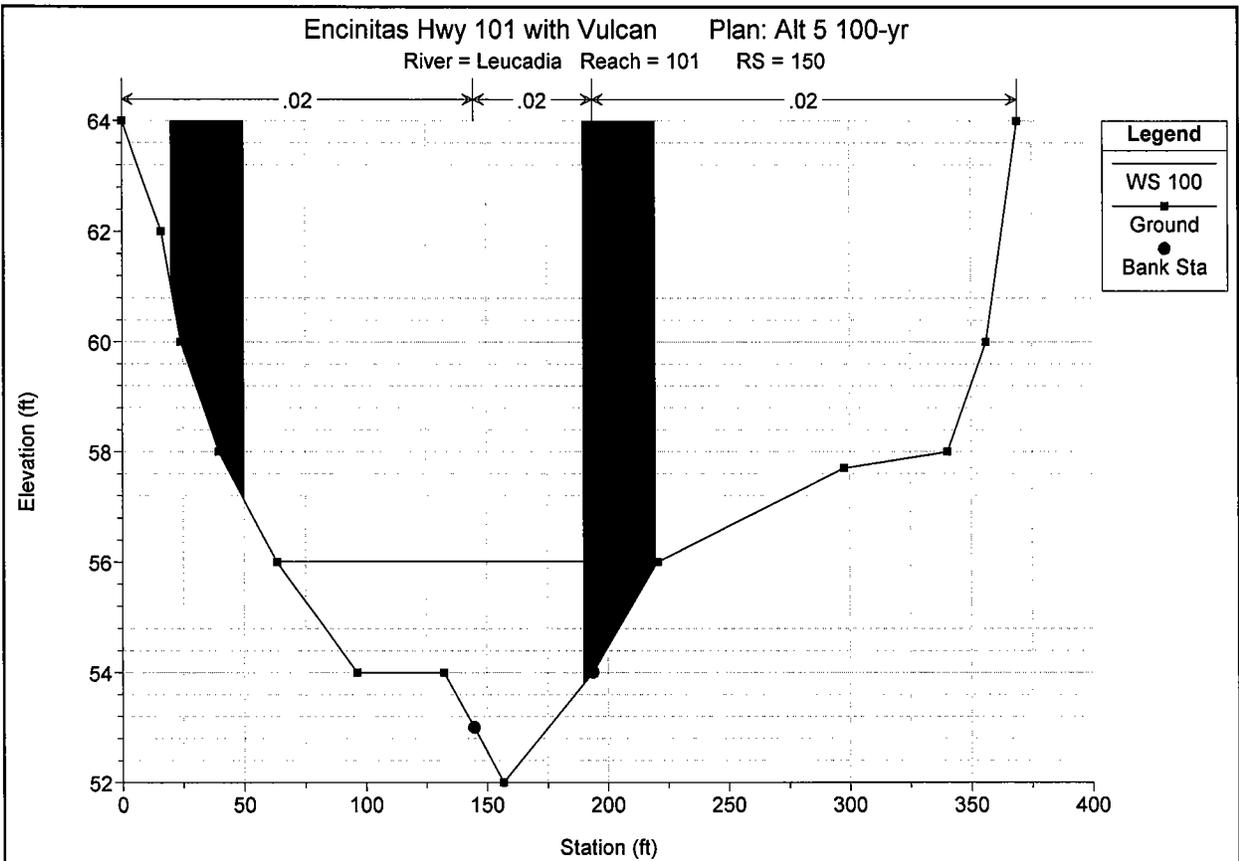


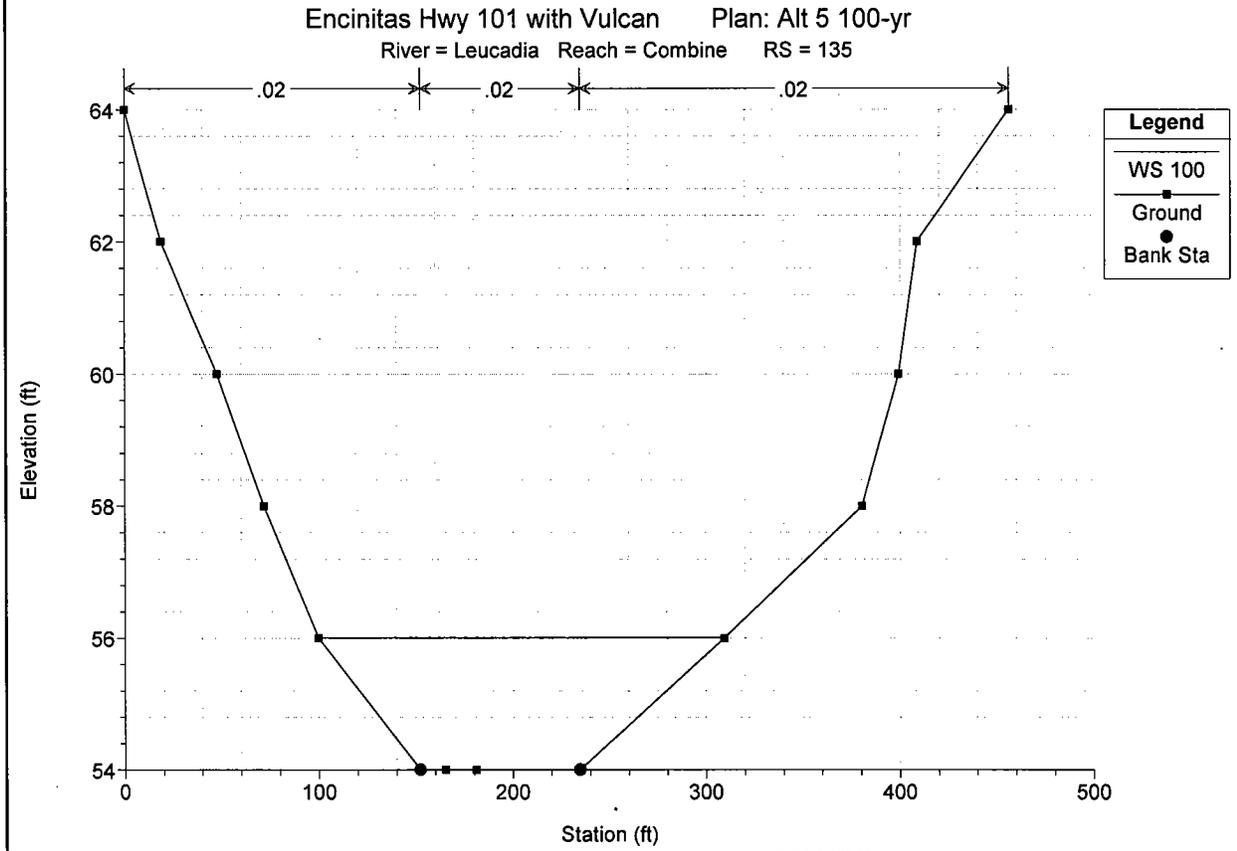
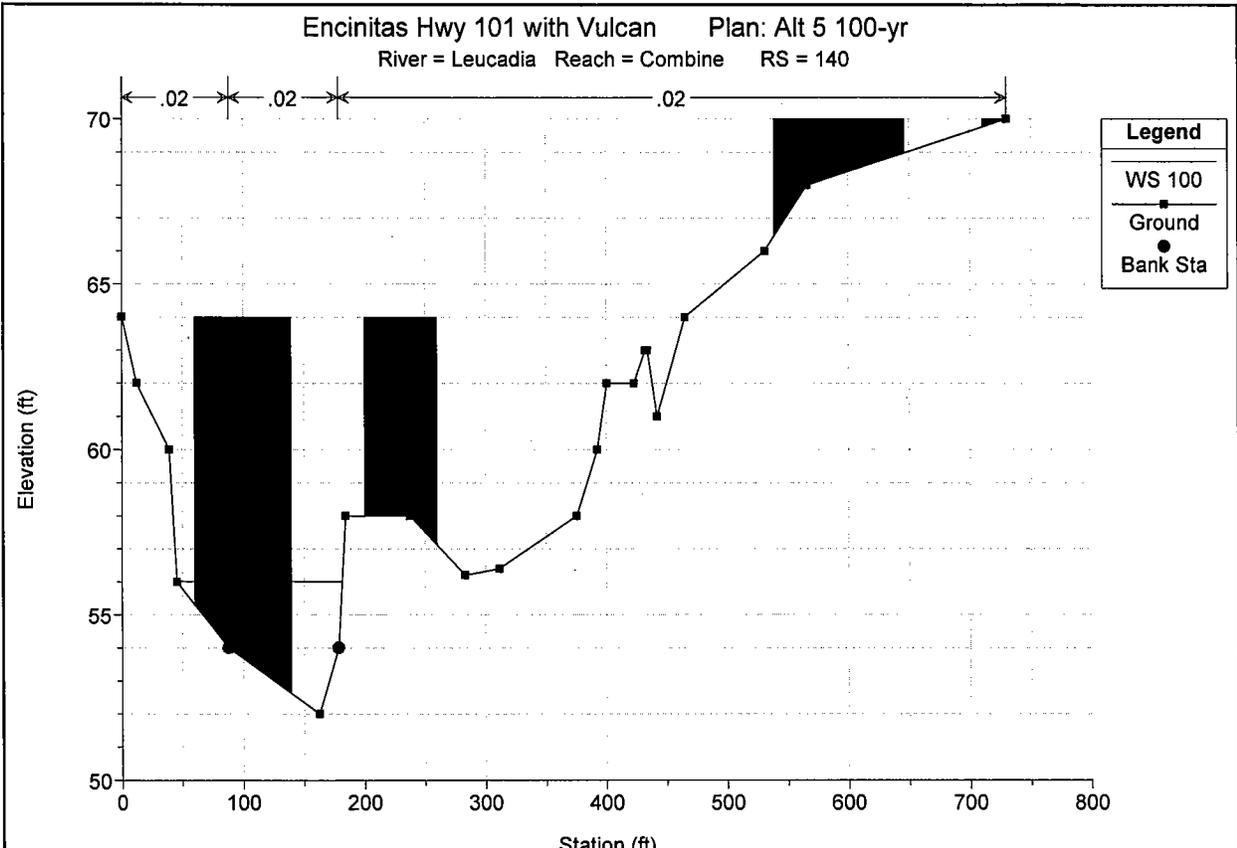
Encinitas Hwy 101 with Vulcan Plan: Alt 5 100-yr

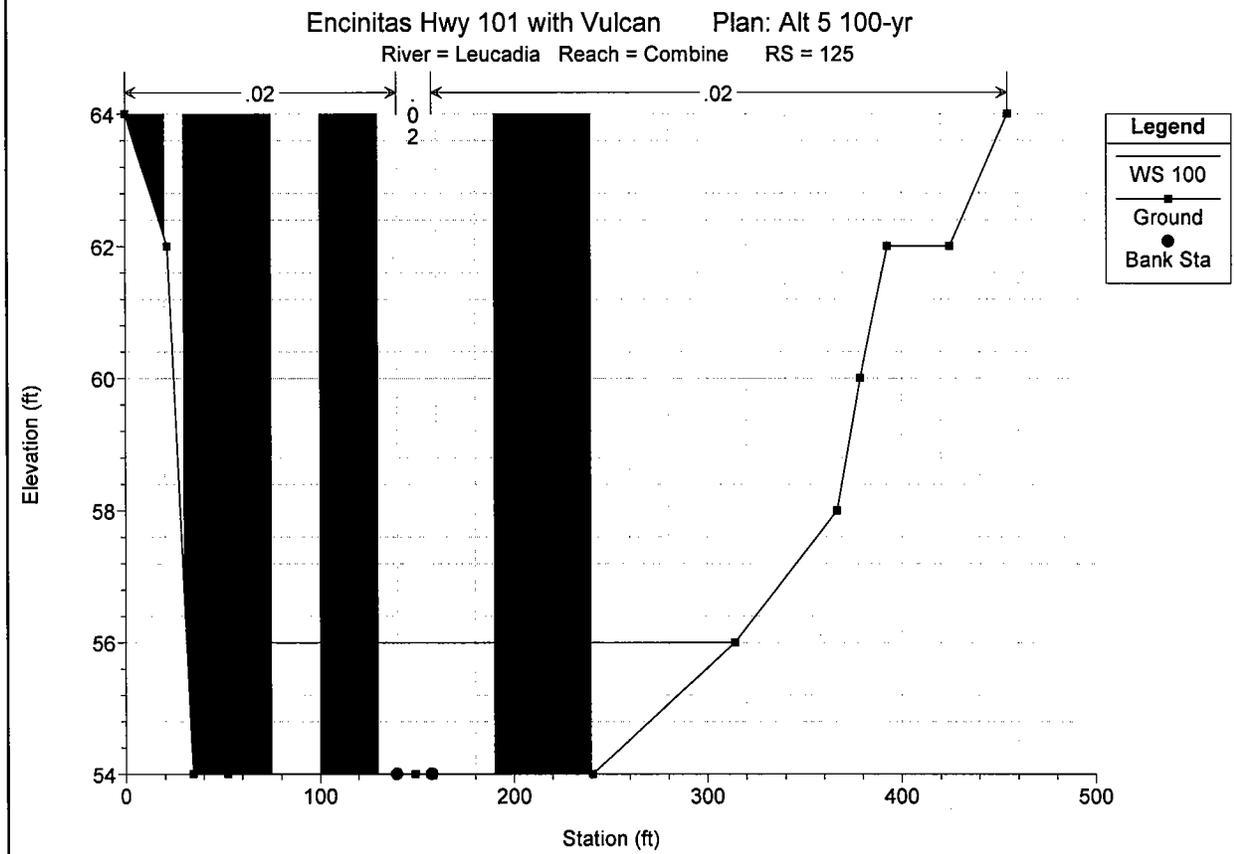
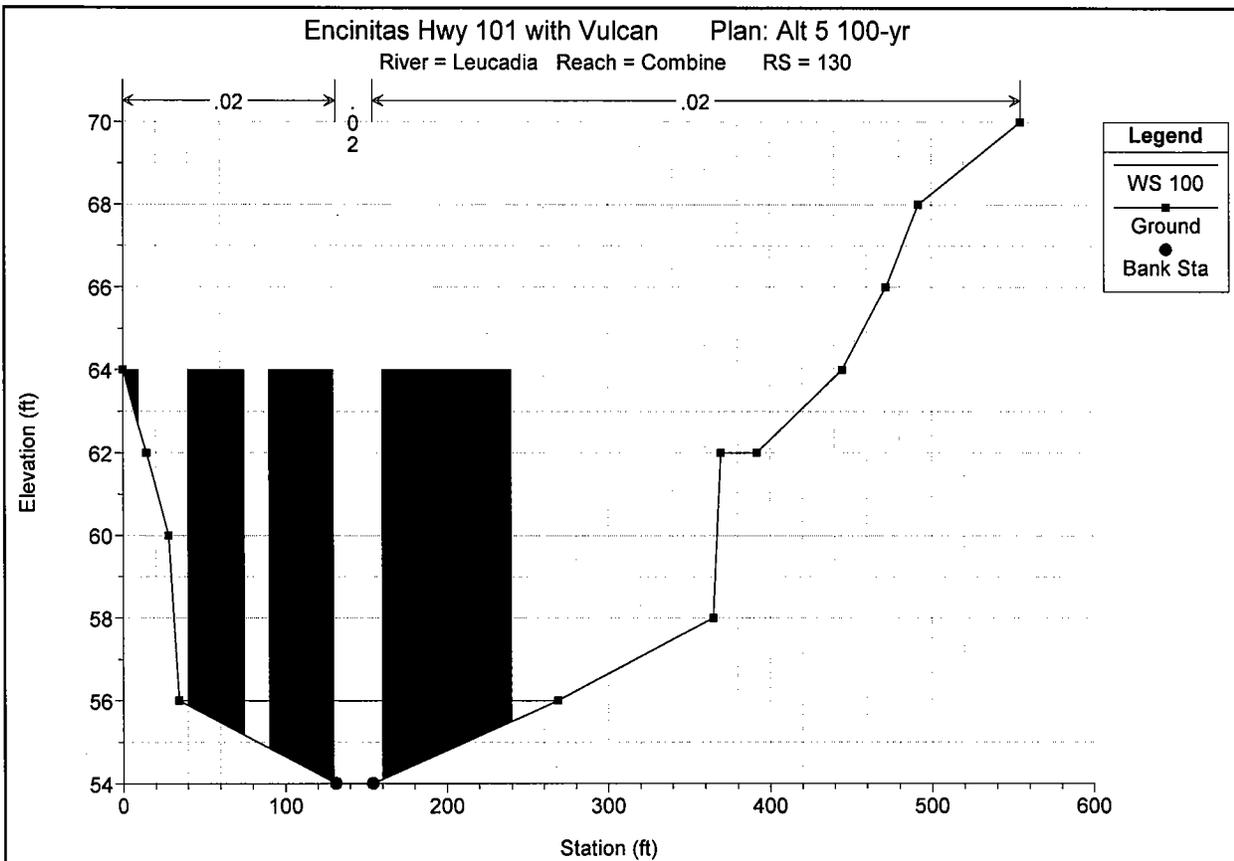
River = Leucadia Reach = 101 RS = 170

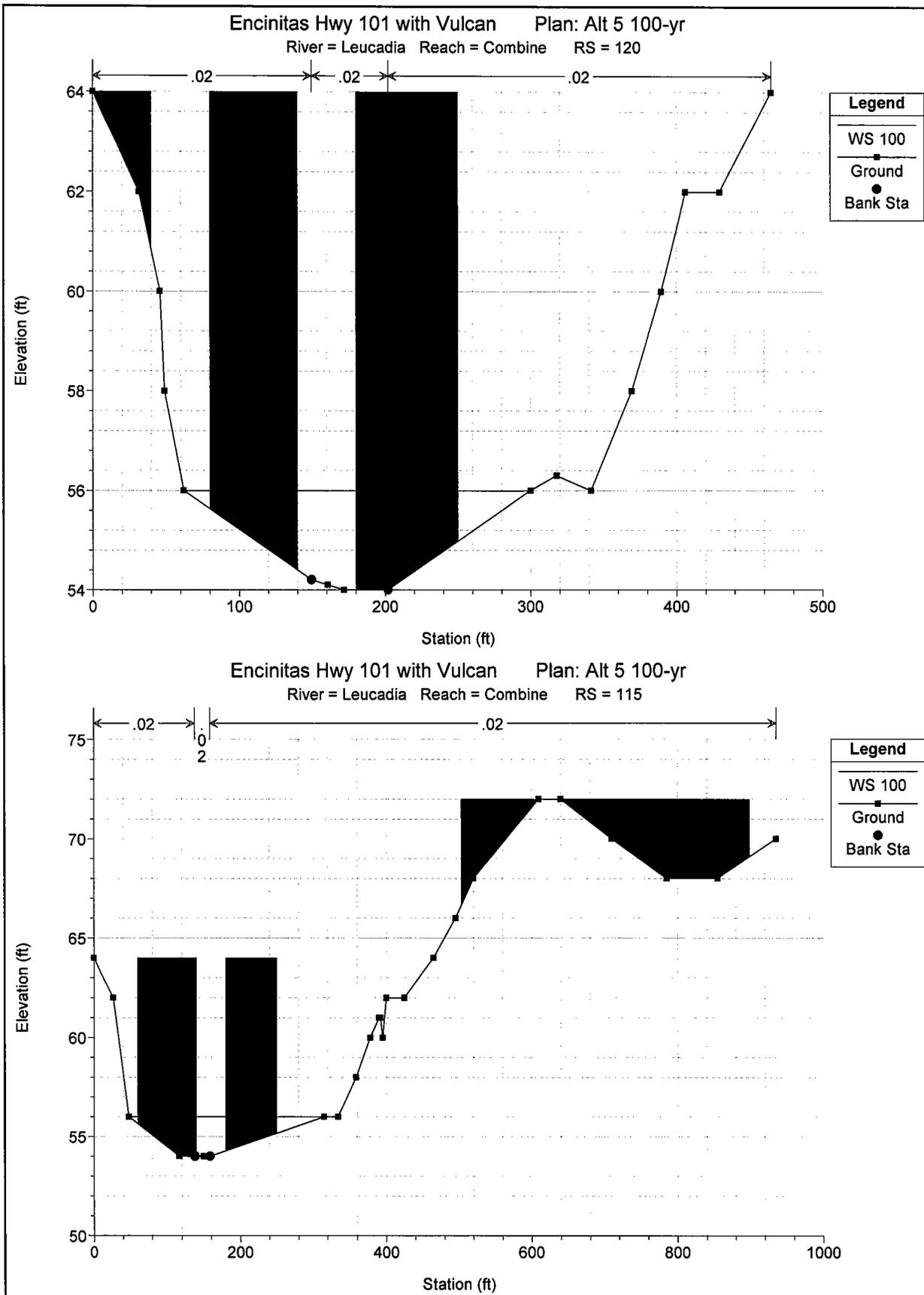


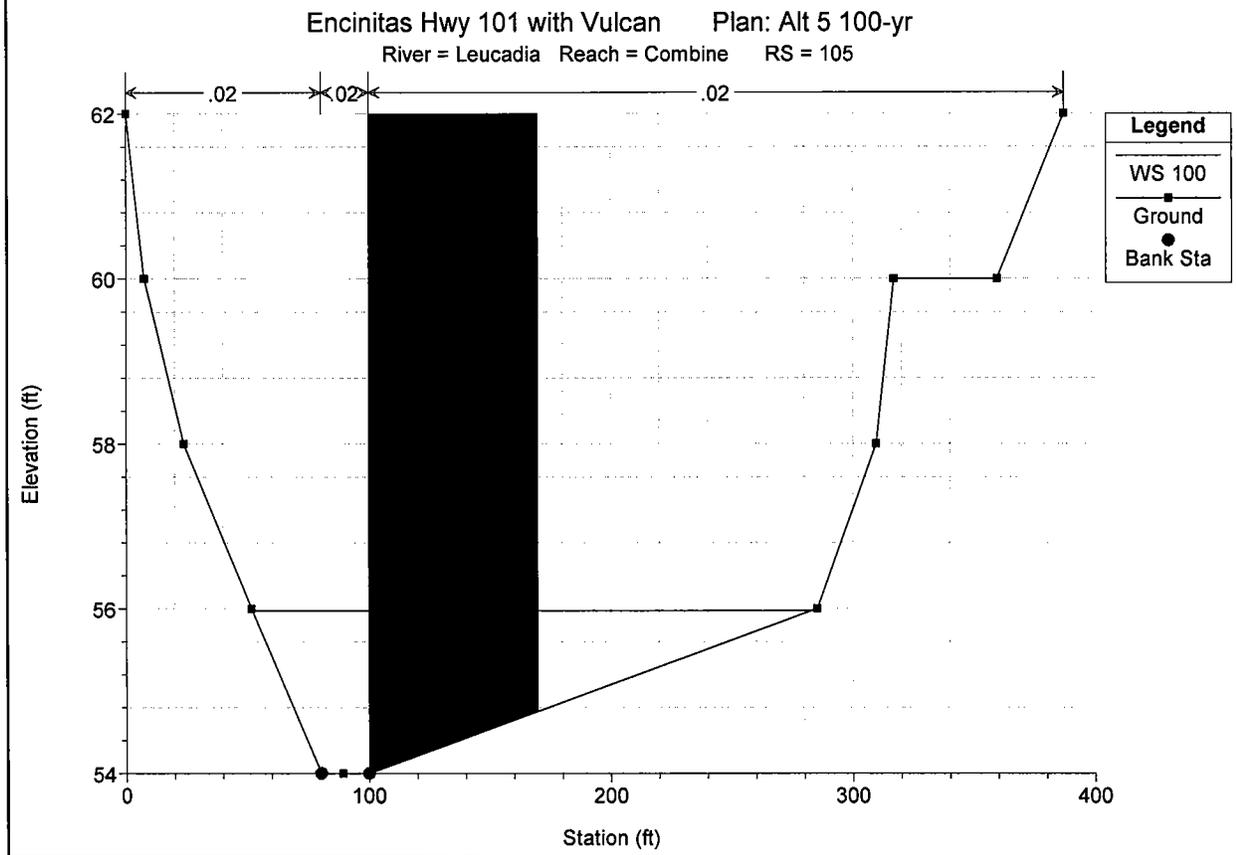
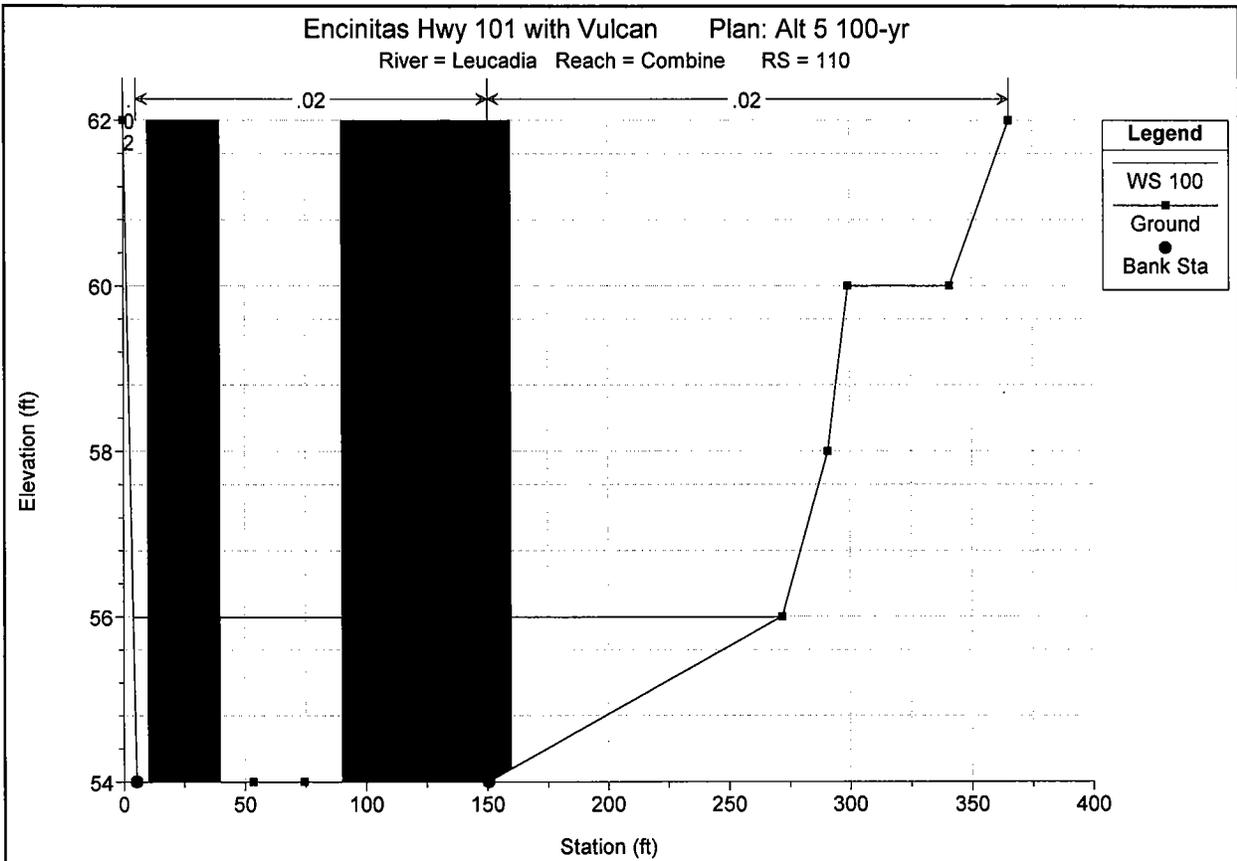


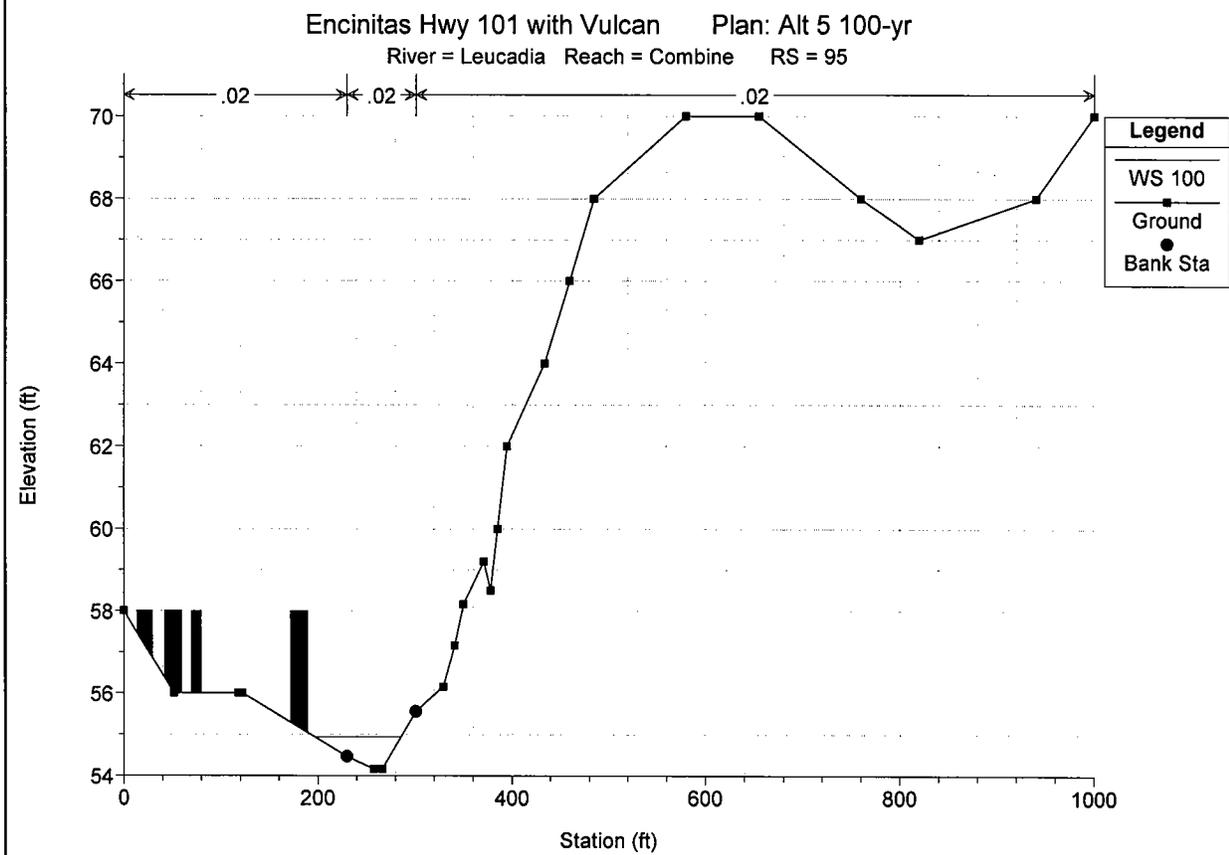
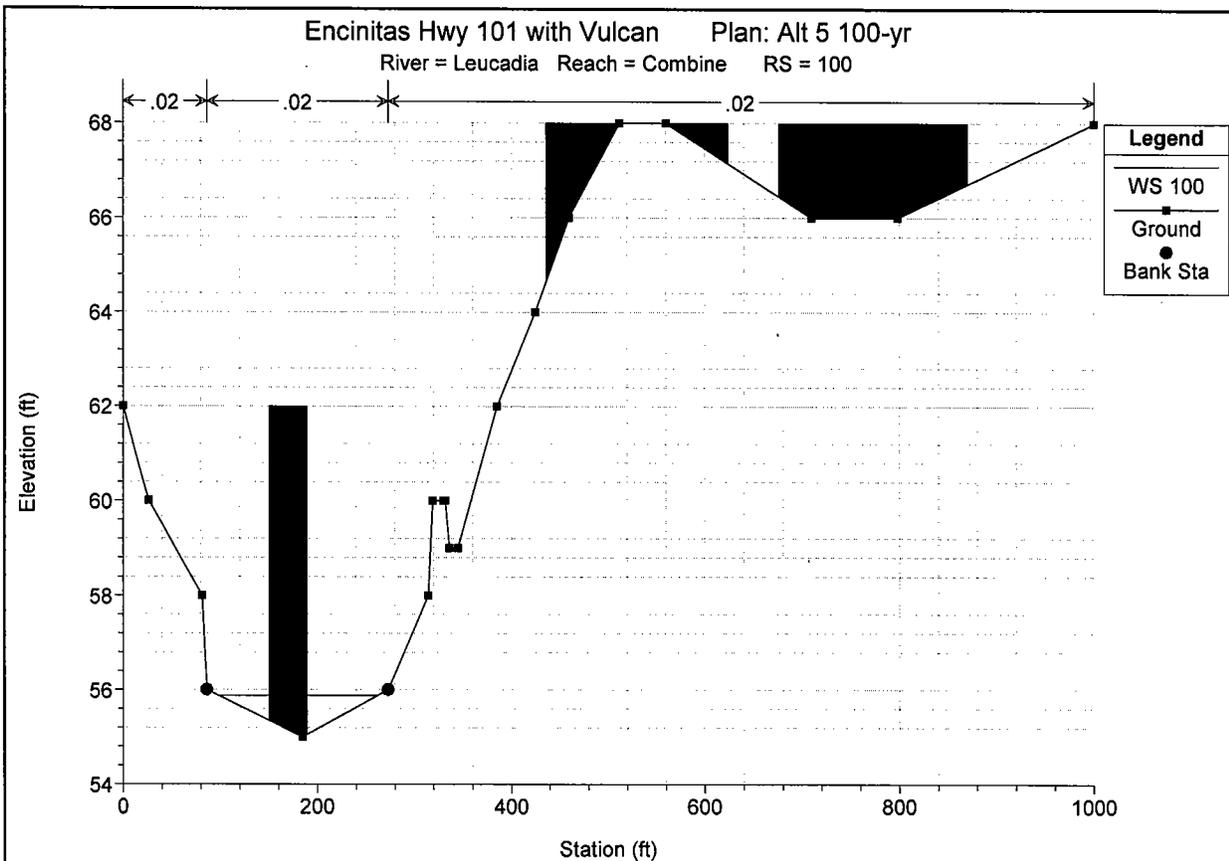


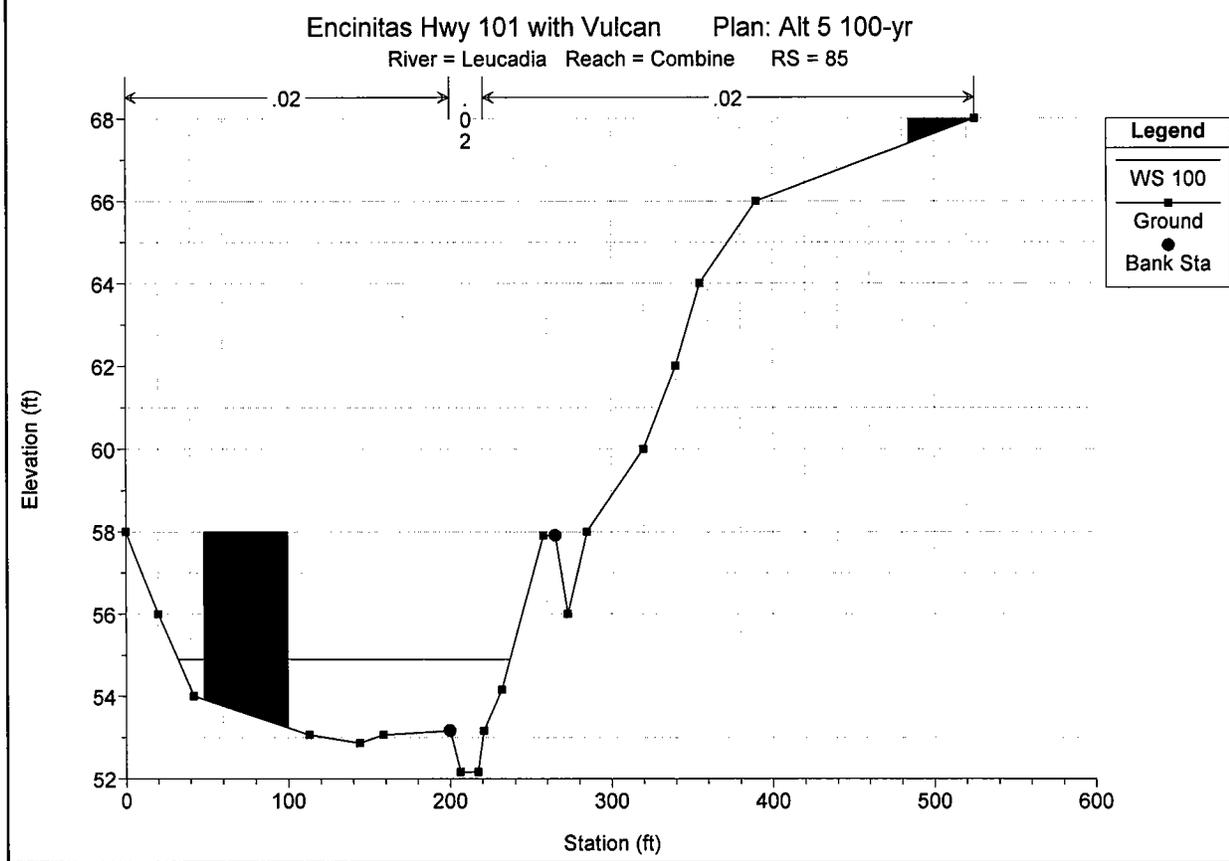
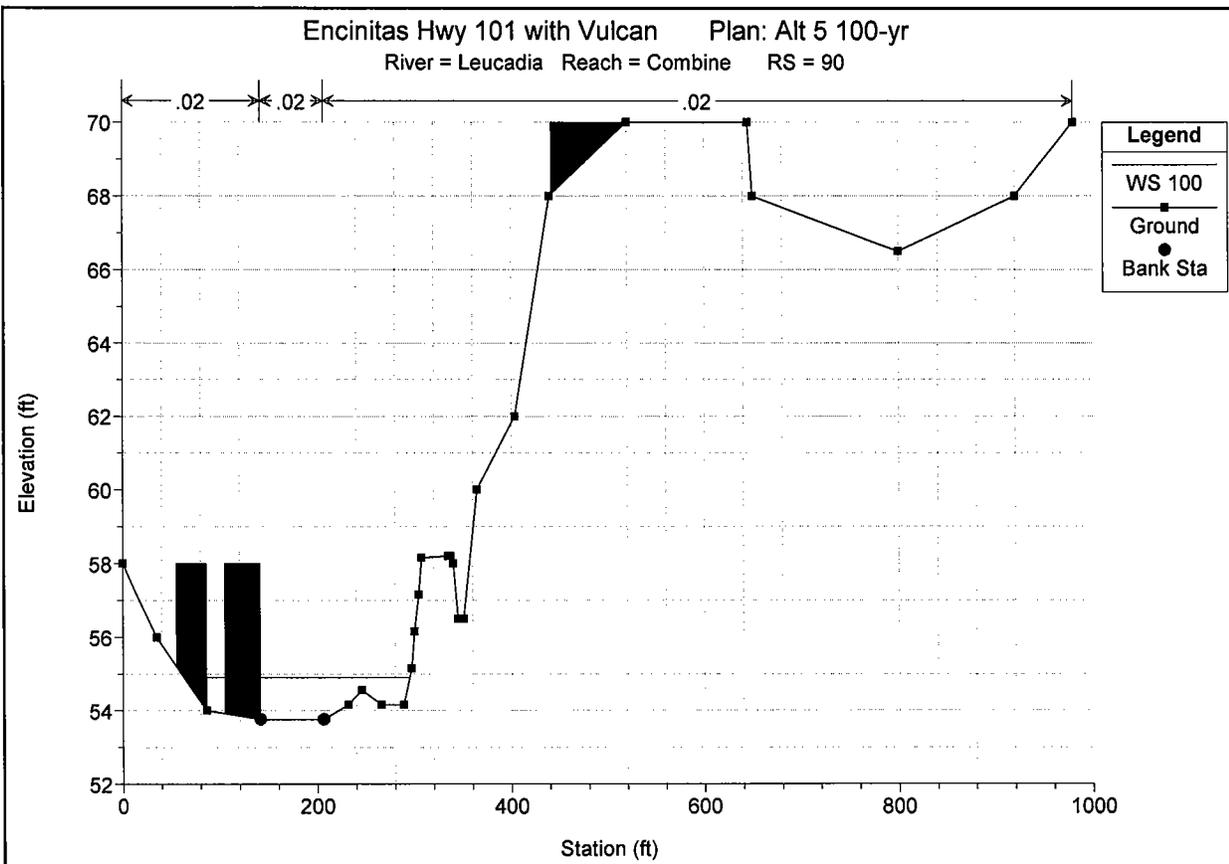


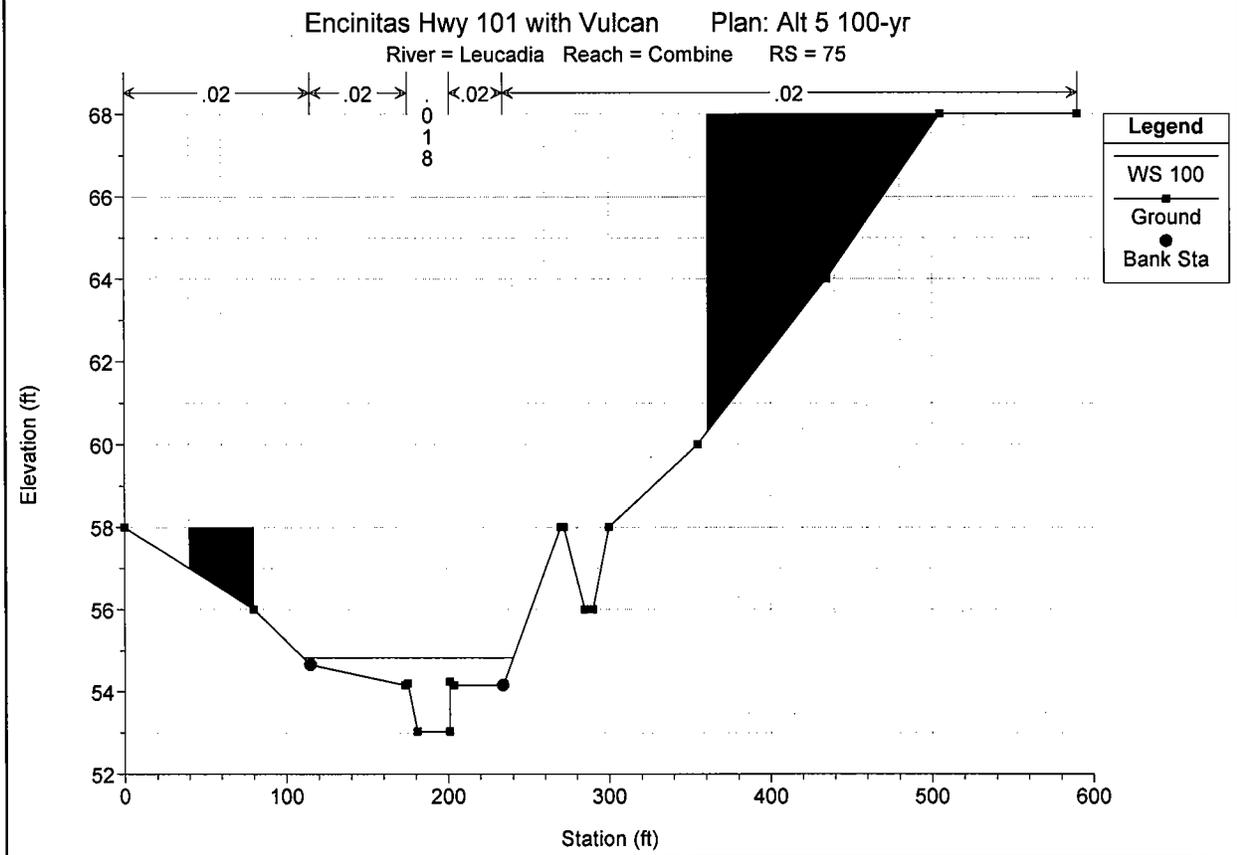
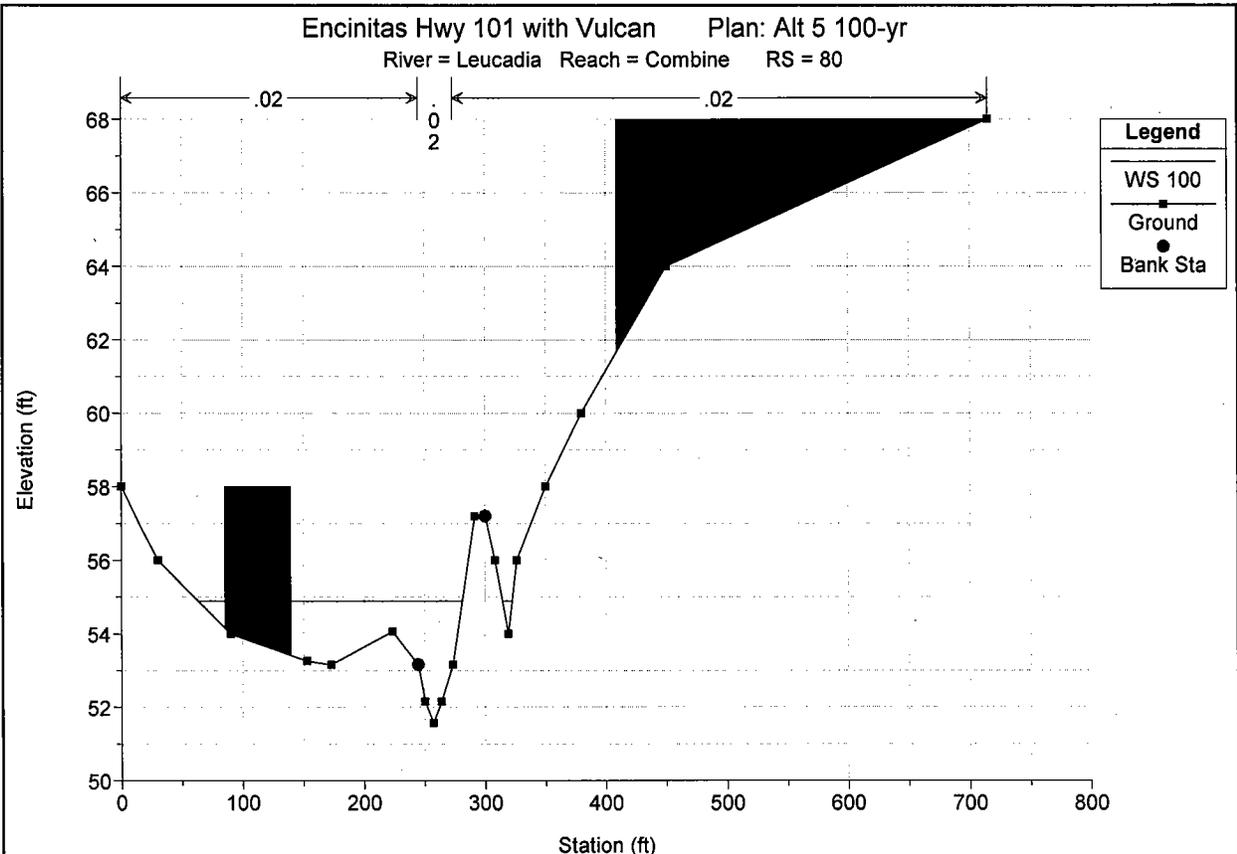


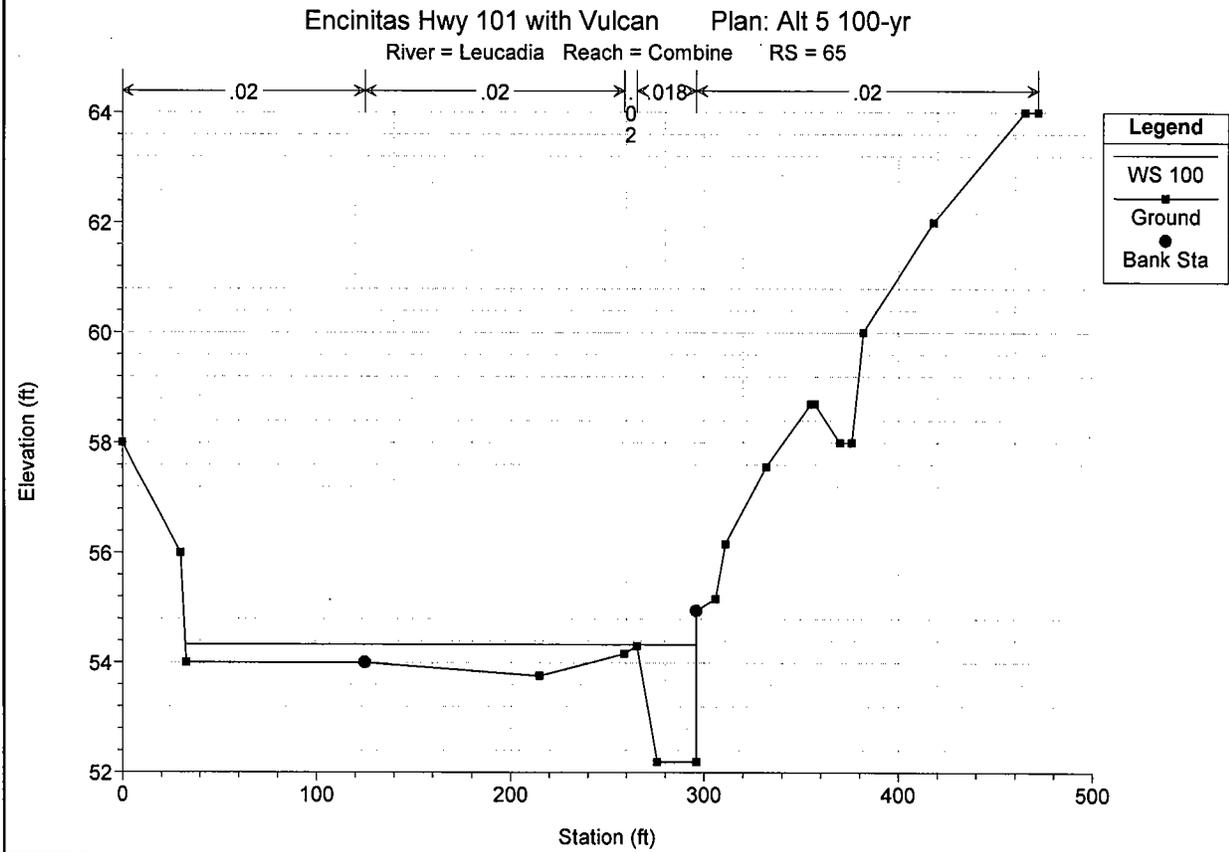
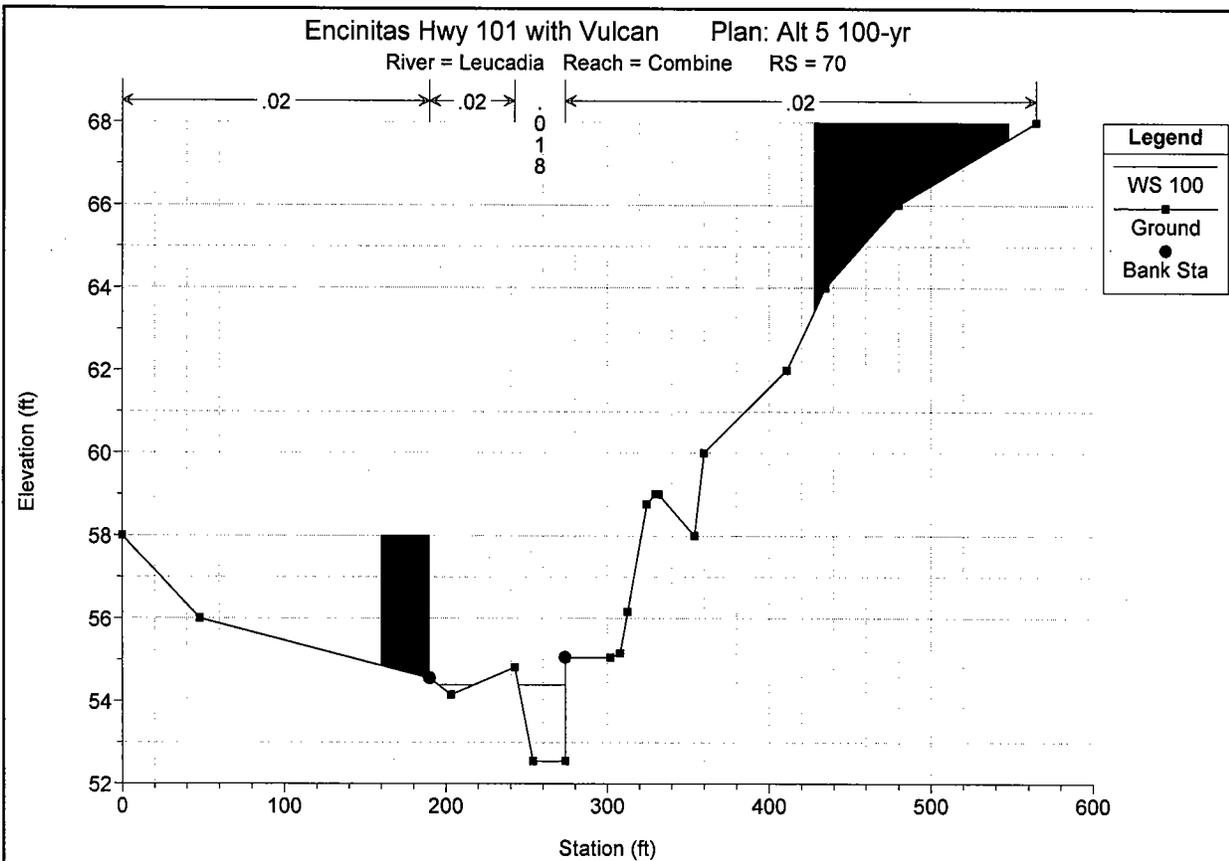


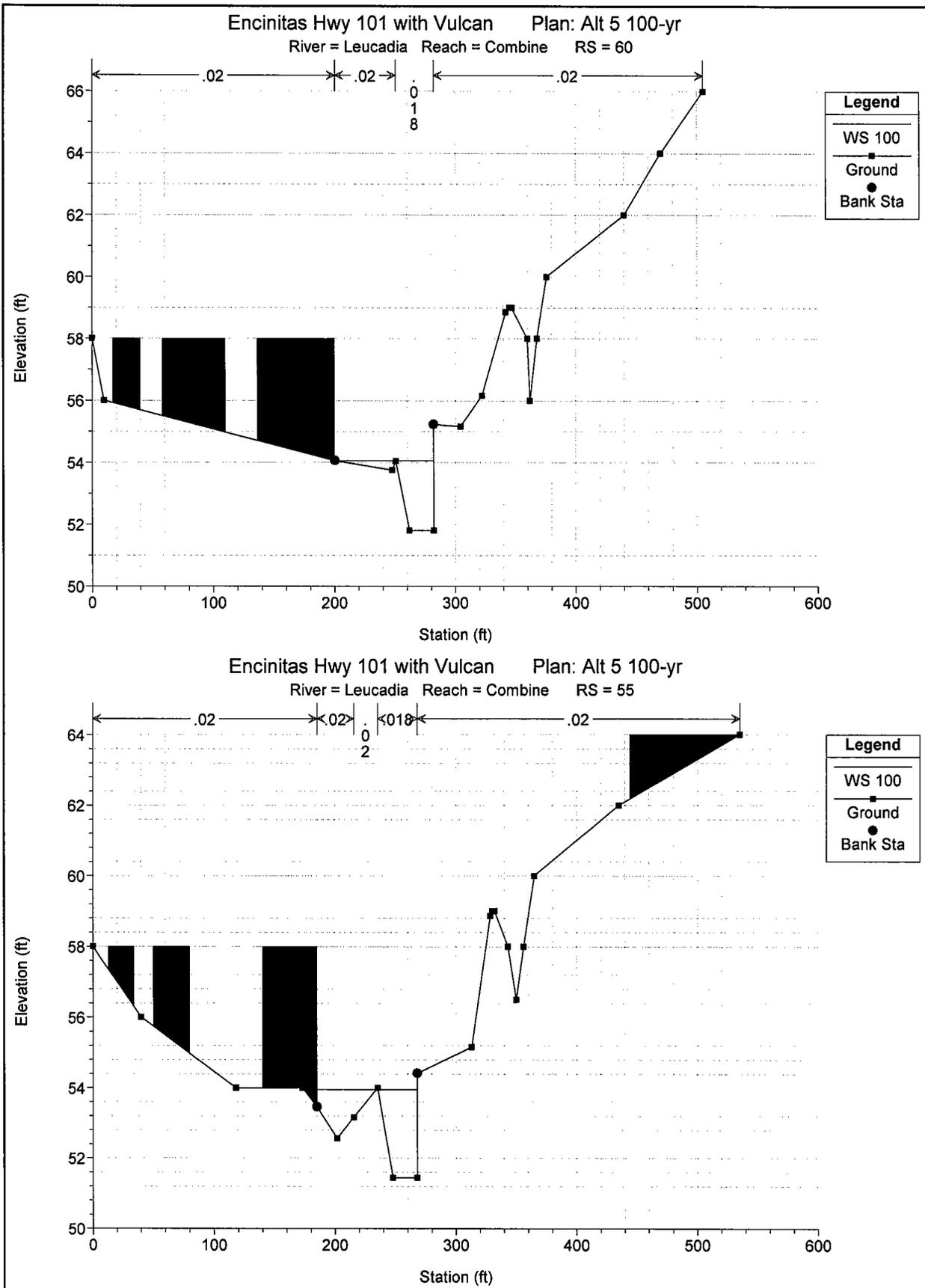


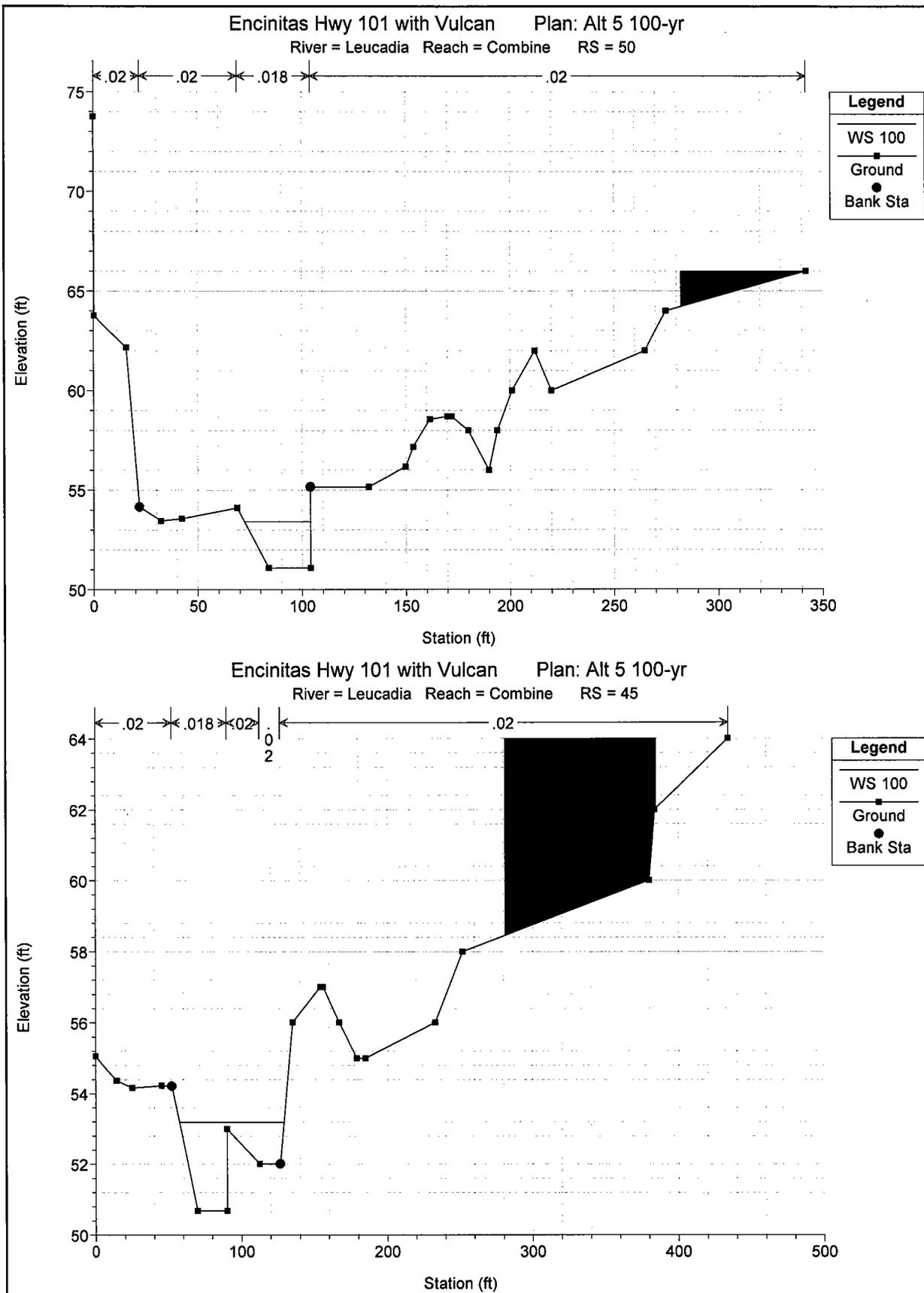


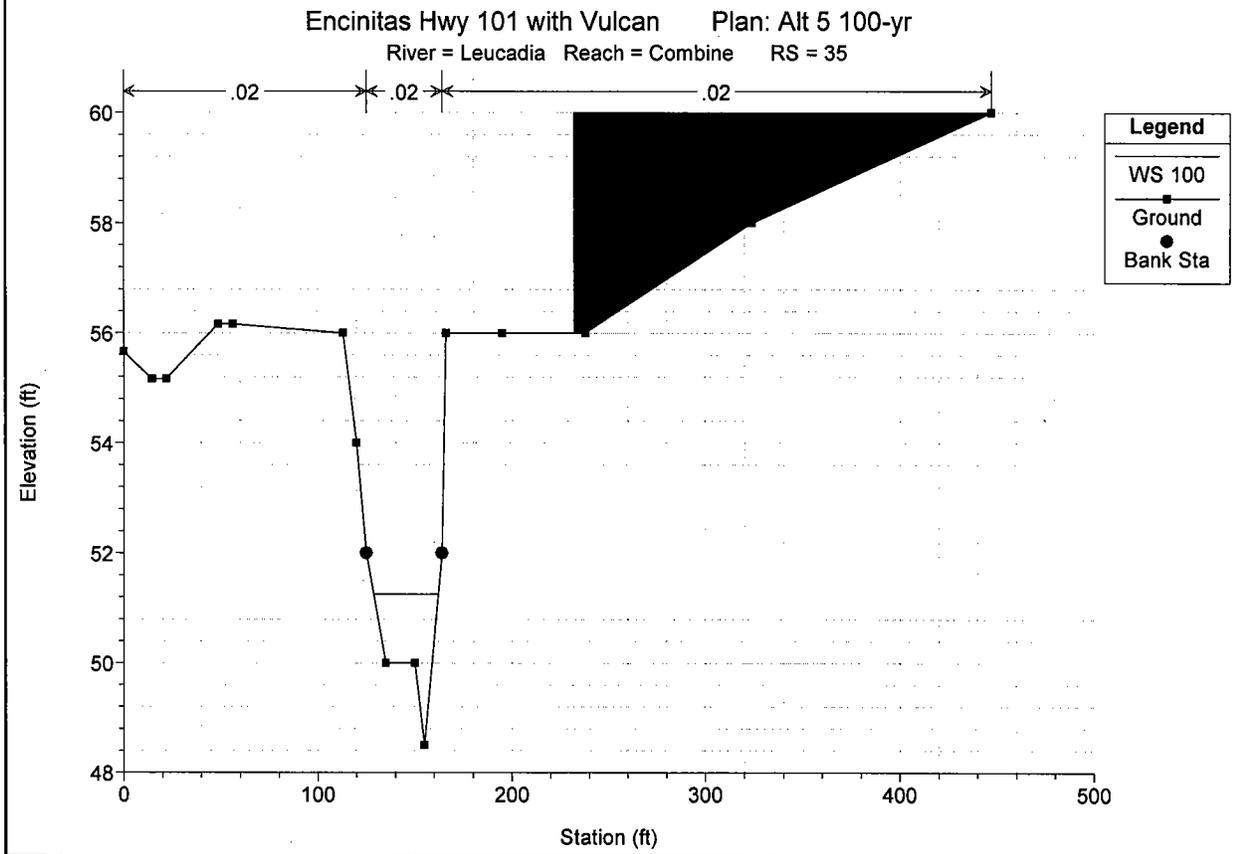
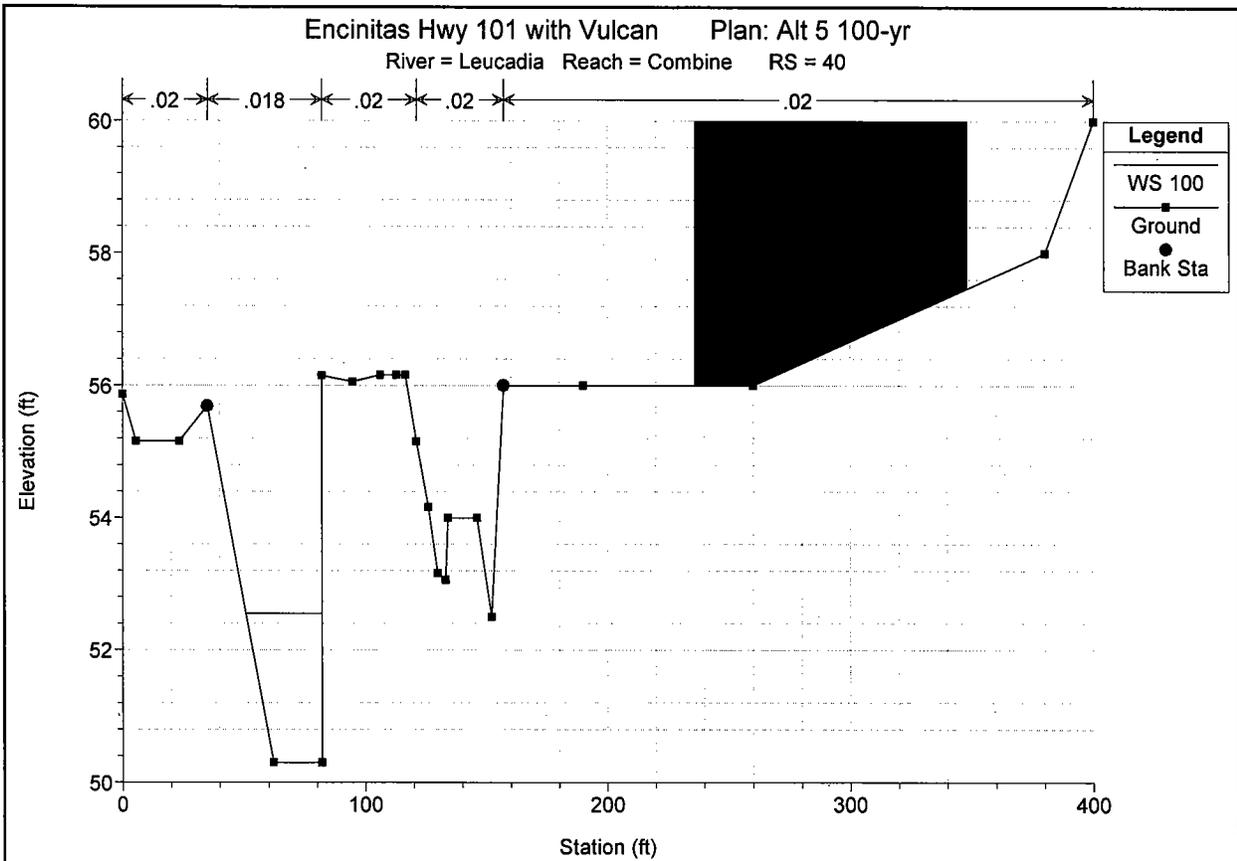






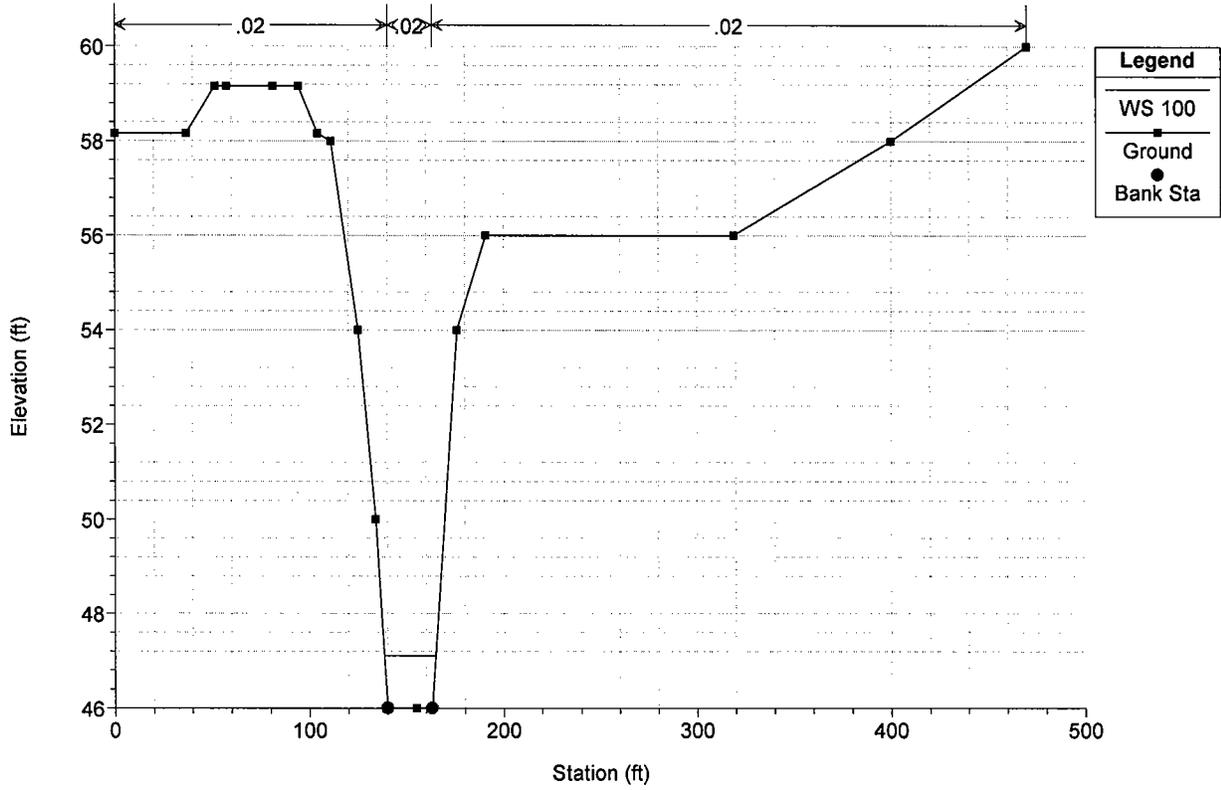






Encinitas Hwy 101 with Vulcan Plan: Alt 5 100-yr

River = Leucadia Reach = Combine RS = 30



HEC-RAS Version 3.0.1 Mar 2001  
 U.S. Army Corp of Engineers  
 Hydrologic Engineering Center  
 609 Second Street, Suite D  
 Davis, California 95616-4687  
 (916) 756-1104

```

X   X   XXXXXX   XXXX   XXXX   XX   XXXX
X   X   X       X   X   X   X   X   X
X   X   X       X       X   X   X   X   X
XXXXXXXX XXXX   X       XXX XXXX XXXXXX XXXX
X   X   X       X       X   X   X   X   X
X   X   X       X   X   X   X   X   X
X   X   XXXXXX   XXXX   X   X   X   X   XXXXX
  
```

PROJECT DATA

Project Title: Encinitas Hwy 101 with Vulcan  
 Project File : 101Vul.prj  
 Run Date and Time: 8/30/2004 5:48:13 AM

Project in English units

Project Description:

ENCINITAS COAST HIGHWAY 101 -100-YR & 10-YR ANALYSIS  
 JN: 14413 DECEMBER 23,  
 2003  
 BASED ON HEC-2 FILENAME: ENC\_1.HC2  
 X-SECTIONS LEFT TO RIGHT LOOKING  
 DOWNSTREAM

PLAN DATA

Plan Title: Alt 5 100-yr  
 Plan File : w:\14413\Hec-Ras 101\101Vul.p17

Geometry Title: Alt 2 Option C  
 Geometry File : w:\14413\Hec-Ras 101\101Vul.g20

Flow Title : Alt 5 100-yr  
 Flow File : w:\14413\Hec-Ras 101\101Vul.f22

Plan Description:

100-YEAR RUN\*\* Includes blocked obstructions in alley  
 Varying Qs based on  
 HEC-1 FN: 100det8.hcl  
 Extended XS from 95 down to encompass 100-yr  
 floodplain  
 Vertical Datum NAVD 88

Plan Summary Information:

Number of:	Cross Sections =	65	Multiple Openings =	0
	Culverts =	0	Inline Weirs =	0
	Bridges =	0		

Computational Information

Water surface calculation tolerance =	0.003
Critical depth calculation tolerance =	0.003
Maximum number of iterations =	20
Maximum difference tolerance =	0.1
Flow tolerance factor =	0.001

Computation Options

Critical depth computed only where necessary  
 Conveyance Calculation Method: At breaks in n values only  
 Friction Slope Method: Average Conveyance  
 Computational Flow Regime: Mixed Flow

FLOW DATA

Flow Title: Alt 5 100-yr  
 Flow File : w:\14413\Hec-Ras 101\101Vul.f22

Flow Data (cfs)

River	Reach	RS	
Leucadia	Vulcan	3300.14	100
Leucadia	Vulcan	240	13
Leucadia	Vulcan	195	1
Leucadia	Vulcan	195	38
Leucadia	101	230	1
Leucadia	101	225.3	1
Leucadia	101	190	1
Leucadia	Combine	140	47
Leucadia	Combine	120	57
Leucadia	Combine	105	90
Leucadia	Combine	90	106
Leucadia	Combine	75	152
Leucadia	Combine	60	186
Leucadia	Combine	50	276

Boundary Conditions

River	Reach	Profile	Upstream	
Downstream				
Leucadia	Vulcan	100	Critical	
Leucadia	101	100	Critical	
Leucadia	Combine	100		Normal S

= .01

GEOMETRY DATA

Geometry Title: Alt 2 Option C  
 Geometry File : w:\14413\Hec-Ras 101\101Vul.g20

Reach Connection Table

River	Reach	Upstream Boundary	Downstream Boundary
Leucadia	Vulcan		Junction
Leucadia	101		Junction
Leucadia	Combine	Junction	

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 3300.14

INPUT

Description:

Station Elevation Data		num= 21	
Sta	Elev	Sta	Elev
110	76.16	143	76.56
170	77.56	180	77.16
204	72.16	206.4	74.56
240	74.1	245	74
420	78		

Manning's n Values

Sta	n Val	Sta	n Val
110	.03	196	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	196	204		100	100	.1	.3
Left Levee	Station=	169.51	Elevation=	77.58			

CROSS SECTION RIVER: Leucadia



Left Levee 196 204 Station= 169.51 100 100 100 Elevation= 75.38 .1 .3

CROSS SECTION RIVER: Leucadia  
REACH: Vulcan RS: 2800.19

INPUT

Description:

Station Elevation Data num= 17

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
70	70.06	113	69.46	126	70.16	150	71.16	155	73.16
160	74.16	164	74.66	169	74.66	174	74.16	175.1	73.56
192	73.26	196	69.26	204	69.26	208	73.26	225	74.16
456	76	523	78						

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
70	.03	196	.035	204	.03

Bank Sta: Left 196 Right 204 Lengths: Left Channel 100 Right 100 Coeff Contr. .1 Expan. .3  
Left Levee Station= 168.93 Elevation= 74.71

CROSS SECTION RIVER: Leucadia  
REACH: Vulcan RS: 2700.20

INPUT

Description:

Station Elevation Data num= 18

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
125	68.16	139	68.86	146	69.16	150	70.16	154	71.16
160	73.16	165	73.86	170	73.86	175	73.16	176.2	72.26
192	71.96	196	67.96	204	67.96	208	71.96	212.73	72.57
258	74	423	76	535	78				

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
125	.03	196	.035	204	.03

Bank Sta: Left 196 Right 204 Lengths: Left Channel 100 Right 100 Coeff Contr. .1 Expan. .3  
Left Levee Station= 170.68 Elevation= 73.86

CROSS SECTION RIVER: Leucadia  
REACH: Vulcan RS: 2600.21

INPUT

Description:

Station Elevation Data num= 20

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
109	66.46	135	66.46	146	68.16	152	69.16	155	70.16
157	71.16	162	73.16	165	73.26	170	73.26	173	73.16
181	71.16	185.1	70.06	192	69.96	196	65.96	204	65.96
208	69.96	215.42	70.99	237	72	286	74	456	76

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
109	.03	196	.035	204	.03

Bank Sta: Left 196 Right 204 Lengths: Left Channel 100 Right 100 Coeff Contr. .1 Expan. .3  
Left Levee Station= 170.09 Elevation= 73.26

CROSS SECTION RIVER: Leucadia  
REACH: Vulcan RS: 2500.22

INPUT

Description:

Station Elevation Data num= 17

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
139	65.16	150	68.16	158	71.16	165	72.76	170	72.76
175	71.16	182	69.16	184	68.66	192	68.46	196	64.46
204	64.46	208	68.46	213.55	69.25	233	70	266	72
320	74	498	76						

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
139	.03	196	.035	204	.03

Bank Sta: Left	Right	Lengths: Left Channel	Right	Coeff	Contr.	Expan.
196	204	100	100	.1	.3	
Left Levee	Station=	170.09	Elevation=	72.78		

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 2400.23

INPUT

Description:

Station Elevation Data	num=	18							
Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev
95 65.56	142 65.16	160 71.16	165 72.46	170 72.46	175 71.16	180 70.16	183 68	192 67.9	194.8 68.16
202 67.96	206 63.96	214 63.96	218 67.96	221.32 68.78	250 70	263 72	360 74		

Manning's n Values	num=	3			
Sta n Val	Sta n Val	Sta n Val			
95 .03	206 .035	214 .03			

Bank Sta: Left	Right	Lengths: Left Channel	Right	Coeff	Contr.	Expan.
206	214	100	100	.1	.3	
Left Levee	Station=	169.39	Elevation=	72.47		

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 2300.24

INPUT

Description:

Station Elevation Data	num=	18							
Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev
2 64.46	129 64.46	141 65.16	160 71.16	165 71.86	170 71.86	175 71.16	185 68.16	190 67	195.2 67.66
202 67.46	206 63.46	214 63.46	218 67.46	221.7 68.36	260 70	316 72	382 74		

Manning's n Values	num=	3			
Sta n Val	Sta n Val	Sta n Val			
2 .03	206 .035	214 .03			

Bank Sta: Left	Right	Lengths: Left Channel	Right	Coeff	Contr.	Expan.
206	214	100	100	.1	.3	
Left Levee	Station=	170.56	Elevation=	71.89		

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 2200.25

INPUT

Description:

Station Elevation Data	num=	15							
Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev
140 64.16	160 71.16	165 71.46	170 71.46	172 71.16	182 68.16	184.7 66.86	192.3 66.76	196 62.96	204 62.96
207.7 66.76	217 66.86	260 68	287 70	342 72					

Manning's n Values	num=	3			
Sta n Val	Sta n Val	Sta n Val			
140 .03	196 .035	204 .03			

Bank Sta: Left	Right	Lengths: Left Channel	Right	Coeff	Contr.	Expan.
196	204	100	100	.1	.3	
Left Levee	Station=	170.39	Elevation=	71.43		

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 2100.26

INPUT

Description:

Station Elevation Data	num=	20							
Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev
144 63.16	164 71.16	165 71.36	170 71.36	175 71.16	182 68.16	186 66	188.3 64.96	193.6 64.86	196 62.46
204 62.46	206.4 64.86	217 65.06	234 66	240 66.1					

245 66 248 65.9 252 66 286 68 322 70

Manning's n Values num= 3  
Sta n Val Sta n Val Sta n Val  
144 .03 196 .035 204 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
196 204 15 15 15 .1 .3  
Left Levee Station= 169.8 Elevation= 71.43

CROSS SECTION RIVER: Leucadia  
REACH: Vulcan RS: 245

INPUT

Description:

Station Elevation Data num= 11  
Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
0 70 10 70 16 68 24 66 30 64  
40 64 70 66 80 66 87 66 122 68  
180 70

Manning's n Values num= 3  
Sta n Val Sta n Val Sta n Val  
0 .03 30 .035 40 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
30 40 175 175 175 .1 .3

CROSS SECTION RIVER: Leucadia  
REACH: Vulcan RS: 240

INPUT

Description:

Station Elevation Data num= 9  
Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
0 70 5 70 10 68 20 66 27 64  
39 64 89 66 185 68 230 70

Manning's n Values num= 3  
Sta n Val Sta n Val Sta n Val  
0 .03 27 .035 39 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
27 39 275 275 275 .1 .3

CROSS SECTION RIVER: Leucadia  
REACH: Vulcan RS: 235

INPUT

Description:

Station Elevation Data num= 6  
Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
0 68 10 68 15 66 140 66 205 68  
246 70

Manning's n Values num= 3  
Sta n Val Sta n Val Sta n Val  
0 .03 15 .035 140 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
15 140 120 120 120 .1 .3

CROSS SECTION RIVER: Leucadia  
REACH: Vulcan RS: 230

INPUT

Description:

Station Elevation Data num= 11  
Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
430 70 460 70 520 68 525 68 544 69.8  
546 69.8 550 68 580 66 715 66 770 68  
825 70

Manning's n Values num= 3  
Sta n Val Sta n Val Sta n Val  
430 .02 580 .02 715 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 580 715 175 180 185 .1 .3  
 Blocked Obstructions num= 1  
 Sta L Sta R Elev  
 797 825 70

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 225

INPUT

Description:  
 Station Elevation Data num= 8  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 536 69.8 538 69.8 542 68 595 66 625 66  
 785 66 827 68 835 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 536 .02 595 .02 785 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 595 785 190 185 185 .1 .3  
 Blocked Obstructions num= 1  
 Sta L Sta R Elev  
 692 835 70

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 220

INPUT

Description:  
 Station Elevation Data num= 7  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 494 69.9 496 69.9 518 68 580 66 876 66  
 900 68 910 72

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 494 .02 580 .02 876 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 580 876 175 175 175 .1 .3

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 215

INPUT

Description:  
 Station Elevation Data num= 15  
 Sta Elev  
 540 69.9 542 69.9 546 68 552 67.9 556 68  
 565 70 580 70.1 594 70 600 69.9 610 70  
 670 68 815 66 860 66 945 68 995 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 540 .02 546 .02 556 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 546 556 290 290 290 .1 .3  
 Blocked Obstructions num= 1  
 Sta L Sta R Elev  
 765 995 70

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 195

INPUT

Description:  
 Station Elevation Data num= 15  
 Sta Elev  
 485 70 496 70 505 68 510 68 515 70  
 520 72 525 74 533 74 612 72 652 70  
 695 68 780 66 820 66 920 68 985 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 485 .02 505 .02 510 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 505 510 340 340 340 .1 .3  
 Blocked Obstructions num= 2  
 Sta L Sta R Elev Sta L Sta R Elev  
 835 903 74 930 985 74

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 175

INPUT  
 Description:  
 Station Elevation Data num= 7  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 335 68 337 68 344 66 348 65.5 350 66  
 765 68 847 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 335 .02 344 .02 350 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 344 350 225 220 220 .1 .3  
 Blocked Obstructions num= 2  
 Sta L Sta R Elev Sta L Sta R Elev  
 525 712 70 739 847 70

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 165

INPUT  
 Description:  
 Station Elevation Data num= 14  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 392 67 394 67 395 66 400 64 410 63  
 418 64 436 66 472 68 512 70 555 72  
 620 72 700 70 795 68 895 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 392 .02 400 .02 418 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 400 418 360 360 360 .1 .3  
 Blocked Obstructions num= 2  
 Sta L Sta R Elev Sta L Sta R Elev  
 546 781 72 826 895 72

CROSS SECTION RIVER: Leucadia  
 REACH: Vulcan RS: 150

INPUT  
 Description:  
 Station Elevation Data num= 12  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 380 65 382 65 385 64 400 63 413 64  
 486 66 520 70 565 74 698 74 750 72  
 967 72 1040 74

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 380 .02 385 .02 413 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 385 413 305 305 305 .1 .3  
 Blocked Obstructions num= 1  
 Sta L Sta R Elev  
 606 1040 74

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 230

INPUT

Description:

Station Elevation Data			num=	8					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	66	25.4	64	30.5	62	88.9	60.2	146	60
243.4	62	278	64	318.4	66				

Manning's n Values			num=	3			
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.02	88.9	.02	146	.02		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	88.9	146		104.1	100.2		.1	.3

Blocked Obstructions			num=	3				
Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta L	Sta R	Elev
50	80	66	145	190	66	285	350	66

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 225.3

INPUT

Description:

Station Elevation Data			num=	14					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	66	16	64	32.6	62	78.4	60	126.9	58
133.4	58	139.4	58	203.7	58	210.3	58	216.8	58.5
233.9	60	285.5	62	319.2	64	355	66		

Manning's n Values			num=	3			
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.02	126.9	.02	203.7	.02		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	126.9	203.7		5	5		.1	.3

Blocked Obstructions			num=	5				
Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta L	Sta R	Elev
5	30	66	130	160	66	180	200	66
210	235	66	300	345	66			

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 225.2

INPUT

Description:

Station Elevation Data			num=	14					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	66	16	64	32.6	62	78.4	60	126.9	58
133.4	54	139.4	54	203.7	56	210.3	58	216.8	58.5
233.9	60	285.5	62	319.2	64	355	66		

Manning's n Values			num=	3			
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.02	126.9	.02	203.7	.02		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	126.9	203.7		5	5		.1	.3

Blocked Obstructions			num=	5				
Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta L	Sta R	Elev
5	30	66	130	160	66	180	200	66
210	235	66	300	345	66			

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 225.1

INPUT

Description:

Station Elevation Data			num=	14					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	66	16	64	32.6	62	78.4	60	126.9	58
133.4	58	139.4	58	203.7	58	210.3	58	216.8	58.5
233.9	60	285.5	62	319.2	64	355	66		

Manning's n Values			num=	3			
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.02	126.9	.02	203.7	.02		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
-----------	------	-------	----------	--------------	-------	-------	--------	--------

	126.9	203.7		134.2	131.9	133.3		.1	.3
Blocked Obstructions	num=		5						
Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta L	Sta R	Elev	
5	30	66	130	160	66	180	200	66	
210	235	66	300	345	66				

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 220

INPUT

Description:

Station Elevation Data	num=		11						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	66	18.9	64	21	62	30.1	60	56.5	58
114.4	57.7	192	58	255	60	292.4	62	321.2	64
343.3	66								

Manning's n Values	num=		3						
Sta	n Val	Sta	n Val	Sta	n Val				
0	.02	56.5	.02	192	.02				

Bank Sta: Left	Right	Lengths: Left	Channel	Right	Coeff	Contr.	Expan.
56.5	192	222.7	215.1	206.1	.1	.3	

Blocked Obstructions	num=		3						
Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta L	Sta R	Elev	
20	60	66	105	140	66	155	190	66	

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 215

INPUT

Description:

Station Elevation Data	num=		14						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	66	10	64	35.7	62	75.9	60	102.5	58
121.6	56	143.9	56	204.1	56	241	56	286	58
307.5	60	345.4	62	377.3	64	381.6	66		

Manning's n Values	num=		3						
Sta	n Val	Sta	n Val	Sta	n Val				
0	.02	121.6	.02	241	.02				

Bank Sta: Left	Right	Lengths: Left	Channel	Right	Coeff	Contr.	Expan.
121.6	241	78.2	80.6	89.6	.1	.3	

Blocked Obstructions	num=		2						
Sta L	Sta R	Elev	Sta L	Sta R	Elev				
10	75	66	160	220	66				

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 210

INPUT

Description:

Station Elevation Data	num=		11						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	66	10.4	64	23.6	62	63.8	60	101.7	58
120.4	56	193.3	56	272.5	56	296.1	58	304.2	60
312.7	66								

Manning's n Values	num=		3						
Sta	n Val	Sta	n Val	Sta	n Val				
0	.02	120.4	.02	272.5	.02				

Bank Sta: Left	Right	Lengths: Left	Channel	Right	Coeff	Contr.	Expan.
120.4	272.5	47.1	45.4	64.5	.1	.3	

Blocked Obstructions	num=		2						
Sta L	Sta R	Elev	Sta L	Sta R	Elev				
20	170	66	210	250	66				

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 205

INPUT

Description:

Station Elevation Data	num=		9						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev

0	64	14	62	58.3	60	89	58	110.7	56
182	56	218.5	56	292.3	58	302.4	64		

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 110.7 .02 218.5 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 110.7 218.5 141.2 142.6 152.6 .1 .3  
 Blocked Obstructions num= 5  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 0 30 64 60 100 64 140 170 64  
 200 225 64 255 280 64

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 195

INPUT  
 Description:  
 Station Elevation Data num= 9  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 64 35.6 62 68.6 60 113.8 58 198.9 56  
 266.6 58 298.8 60 323.4 62 337.5 64

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 113.8 .02 266.6 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 113.8 266.6 143.6 102.4 81.7 .1 .3  
 Blocked Obstructions num= 3  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 95 130 64 150 180 64 210 255 64

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 190

INPUT  
 Description:  
 Station Elevation Data num= 8  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 64 16.8 62 31.4 60 99.1 58 133.4 58  
 179.5 58 217.5 60 231.5 64

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 99.1 .02 179.5 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 99.1 179.5 109.2 93.8 106 .1 .3  
 Blocked Obstructions num= 4  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 0 10 64 35 65 64 90 120 64  
 185 230 64

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 185

INPUT  
 Description:  
 Station Elevation Data num= 6  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 64 21.3 62 59.2 60 118.2 59 204.1 60  
 212.1 64

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 59.2 .02 204.1 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 59.2 204.1 56.4 82.7 111.4 .1 .3  
 Blocked Obstructions num= 2  
 Sta L Sta R Elev Sta L Sta R Elev  
 60 100 64 150 210 64

CROSS SECTION RIVER: Leucadia

REACH: 101 RS: 180

INPUT

Description:

Station Elevation Data		num= 9		Sta Elev		Sta Elev		Sta Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	64	17	62	30.5	60	71.4	59	113.4	60
120.7	64	192.2	64	257.1	63	317.6	64		

Manning's n Values		num= 3		Sta n Val	
Sta	n Val	Sta	n Val	Sta	n Val
0	.02	30.5	.02	113.4	.02

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	30.5	113.4		83.8	85.3		.1	.3

Blocked Obstructions		num= 2		Sta L Sta R Elev	
Sta L	Sta R	Elev	Sta L	Sta R	Elev
40	85	64	130	190	64

CROSS SECTION RIVER: Leucadia  
REACH: 101 RS: 175

INPUT

Description:

Station Elevation Data		num= 11		Sta Elev		Sta Elev		Sta Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	64	5.6	62	20.6	60	56.6	59	99.6	60
104.6	62	172	63	232	62	252.5	61.9	268.5	62
309.1	64								

Manning's n Values		num= 3		Sta n Val	
Sta	n Val	Sta	n Val	Sta	n Val
0	.02	20.6	.02	99.6	.02

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	20.6	99.6		120.2	124.8		.1	.3

Blocked Obstructions		num= 2		Sta L Sta R Elev	
Sta L	Sta R	Elev	Sta L	Sta R	Elev
20	55	64	110	160	64

CROSS SECTION RIVER: Leucadia  
REACH: 101 RS: 170

INPUT

Description:

Station Elevation Data		num= 7		Sta Elev		Sta Elev		Sta Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	64	33.4	62	87.4	60	141.8	58.5	184.7	60
322	62	333.5	64						

Manning's n Values		num= 3		Sta n Val	
Sta	n Val	Sta	n Val	Sta	n Val
0	.02	87.4	.02	184.7	.02

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	87.4	184.7		137.5	137.6		.1	.3

CROSS SECTION RIVER: Leucadia  
REACH: 101 RS: 165

INPUT

Description:

Station Elevation Data		num= 16		Sta Elev		Sta Elev		Sta Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	64	14.5	62	16	60	102.4	58	128.4	57
138.5	56	147.5	56	172.9	55.9	200.4	56	225.9	58
245.3	60	261.4	60.2	279.4	60	288.3	60	366.3	60
374.3	64								

Manning's n Values		num= 3		Sta n Val	
Sta	n Val	Sta	n Val	Sta	n Val
0	.02	138.5	.02	200.4	.02

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	138.5	200.4		309.6	309.5		.1	.3

Blocked Obstructions		num= 2		Sta L Sta R Elev	

Sta L	Sta R	Elev	Sta L	Sta R	Elev
30	80	64	190	240	64

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 160

INPUT

Description:

Station Elevation Data	num=	19
Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev		
0 64 21 62 37 60 57.5 58 105 56		
129.5 55 142.1 55 152.6 55 186.5 54 214.5 55		
237 56 283.6 58 300.1 58.1 317 58 333 57.9		
342 58 359 60 368 62 376 64		

Manning's n Values	num=	3
Sta n Val Sta n Val Sta n Val		
0 .02 152.6 .02 214.5 .02		

Bank Sta: Left	Right	Lengths: Left	Channel	Right	Coeff	Contr.	Expan.
152.6	214.5	48.6	52.6	51.9	.1	.3	

Blocked Obstructions	num=	3
Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev		
30 70 64 90 120 64 150 170 64		

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 150

INPUT

Description:

Station Elevation Data	num=	15
Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev		
0 64 16 62 24 60 39.5 58 63.4 56		
96.4 54 132.3 54 144.8 53 156.9 52 193.8 54		
220.8 56 297.7 57.7 340.3 58 356.3 60 369.2 64		

Manning's n Values	num=	3
Sta n Val Sta n Val Sta n Val		
0 .02 144.8 .02 193.8 .02		

Bank Sta: Left	Right	Lengths: Left	Channel	Right	Coeff	Contr.	Expan.
144.8	193.8	151.2	154.7	157.7	.1	.3	

Blocked Obstructions	num=	2
Sta L Sta R Elev Sta L Sta R Elev		
20 50 64 190 220 64		

CROSS SECTION RIVER: Leucadia  
 REACH: 101 RS: 145

INPUT

Description:

Station Elevation Data	num=	14
Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev		
0 64 22.3 62 44.3 58 79.3 56 111.6 54		
143.9 52 156.1 52 176.6 52 182.1 58 246 58		
280.5 56.5 384.4 58 398.4 62 411.9 64		

Manning's n Values	num=	3
Sta n Val Sta n Val Sta n Val		
0 .02 143.9 .02 176.6 .02		

Bank Sta: Left	Right	Lengths: Left	Channel	Right	Coeff	Contr.	Expan.
143.9	176.6	175.6	160.5	160.3	.1	.3	

Blocked Obstructions	num=	3
Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev		
40 85 64 115 150 64 180 240 64		

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 140

INPUT

Description:

Station Elevation Data	num=	22
Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev		
0 64 12.5 62 39 60 45.5 56 88 54		
162.6 52 178.6 54 184.6 58 237.6 58 283.1 56.2		

311.6	56.4	375.5	58	392.5	60	400.6	62	422.6	62
432	63	434	63	442	61	465	64	531	66
566	68	730	70						

Manning's n Values num= 3  
 Sta n Val Sta n Val  
 0 .02 88 .02 178.6 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 88 178.6 141.5 123.2 117.1 .1 .3

Blocked Obstructions num= 4  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 60 140 64 200 260 64 539 646 70  
 710 730 70

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 135

INPUT

Description:  
 Station Elevation Data num= 14  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 64 18.7 62 47.7 60 71.8 58 99.9 56  
 152.2 54 165.3 54 181.2 54 234.9 54 309.4 56  
 380.6 58 399.2 60 408.7 62 456.1 64

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 152.2 .02 234.9 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 152.2 234.9 122.2 126.9 132.7 .1 .3

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 130

INPUT

Description:  
 Station Elevation Data num= 14  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 64 14.5 62 28 60 34.5 56 131.4 54  
 154.3 54 268.8 56 365.1 58 370 62 392 62  
 445 64 472 66 492 68 555 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 131.4 .02 154.3 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 131.4 154.3 197.5 197.3 196.3 .1 .3

Blocked Obstructions num= 4  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 0 10 64 40 75 64 90 130 64  
 160 240 64

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 125

INPUT

Description:  
 Station Elevation Data num= 14  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 64 21.6 62 34.6 54 52.6 54 139.7 54  
 149.2 54 157.7 54 240.8 54 314.2 56 366.8 58  
 378.8 60 392.8 62 424.8 62 454.4 64

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 139.7 .02 157.7 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 139.7 157.7 131.2 129.8 132.3 .1 .3

Blocked Obstructions num= 4  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 0 20 64 30 75 64 100 130 64  
 190 240 64



Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 80.4 .02 100.1 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 80.4 100.1 106.7 119.5 229.1 .1 .3

Blocked Obstructions num= 1  
 Sta L Sta R Elev  
 100 170 62

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 100

INPUT

Description:

Station Elevation Data num= 20  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 62 26.6 60 81.5 58 86.5 56 185 55  
 273.2 56 314.6 58 319.3 60 330 60 332 60  
 336 59 345 59 385 62 425 64 460 66  
 512 68 560 68 710 66 798 66 1000 68

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 86.5 .02 273.2 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 86.5 273.2 360 340 360 .1 .3

Blocked Obstructions num= 3  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 150 190 62 436 624 68 676 870 68

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 95

INPUT

Description:

Station Elevation Data num= 24  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 58 52 56 118 56 122 56 230 54.46  
 257.9 54.16 266.8 54.16 301.1 55.56 329.4 56.16 341.1 57.16  
 350.3 58.16 371 59.2 378 58.5 385 60 395 62  
 434 64 460 66 485 68 580 70 655 70  
 760 68 820 67 940 68 1000 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 230 .02 301.1 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 230 301.1 365.1 364.9 363 .1 .3

Blocked Obstructions num= 4  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 14 30 58 42 60 58 70 80 58  
 172 190 58

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 90

INPUT

Description:

Station Elevation Data num= 27  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 58 35 56 86 54 142 53.76 206.7 53.76  
 231.7 54.16 245.3 54.56 265.7 54.16 288.9 54.16 296.9 55.16  
 299.9 56.16 304.4 57.16 307.3 58.16 335 58.2 337 58.2  
 340 58 345 56.5 351 56.5 365 60 404 62  
 440 68 520 70 645 70 650 68 800 66.5  
 920 68 980 70

Manning's n Values num= 3  
 Sta n Val Sta n Val Sta n Val  
 0 .02 142 .02 206.7 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.



Station Elevation Data									
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	58	48	56	190	54.56	203	54.16	242.65	54.82
254	52.55	274	52.55	274	55.06	301.9	55.06	308.1	55.16
312.8	56.16	324.7	58.76	330	59	332	59	354	58
360	60	411	62	435	64	480	66	565	68

Manning's n Values									
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.02	190	.02	242.65	.018	274	.02		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	190	274		360 359.8	358.2		.1	.3

Blocked Obstructions						
Sta L	Sta R	Elev	Sta L	Sta R	Elev	
160	190	58	428	548	68	

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 65

INPUT

Description:

Station Elevation Data									
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	58	30	56	33	54	125	54	215	53.76
258.9	54.16	265.45	54.3	276	52.19	296	52.19	296	54.95
306	55.16	311.1	56.16	331.9	57.56	355	58.7	357	58.7
370	58	376	58	382	60	418	62	465	64
472	64								

Manning's n Values									
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.02	125	.02	258.9	.02	265.45	.018	296	.02

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	125	296		384.7 386.9	384.1		.1	.3

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 60

INPUT

Description:

Station Elevation Data									
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	58	10	56	200.3	54.06	247.7	53.76	250.73	54.05
262	51.8	282	51.8	282	55.23	304.3	55.16	322.1	56.16
342.1	58.86	345	59	347	59	360	58	362	56
368	58	376	60	440	62	470	64	505	66

Manning's n Values									
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.02	200.3	.02	250.73	.018	282	.02		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	200.3	282		364.2 363.7	367		.1	.3

Blocked Obstructions								
Sta L	Sta R	Elev	Sta L	Sta R	Elev	Sta L	Sta R	Elev
17	40	58	58	110	58	136	200	58

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 55

INPUT

Description:

Station Elevation Data									
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	58	40	56	118	54	173	54	185	53.46
201.7	52.56	215.5	53.16	235.2	54	248	51.44	268	51.44
268	54.42	313	55.16	328.4	58.86	330	59	332	59
343	58	350	56.5	356	58	365	60	435	62
535	64								

Manning's n Values									
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.02	185	.02	215.5	.02	235.2	.018	268	.02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 185 268 354.4 358.2 348.8 .1 .3  
 Blocked Obstructions num= 4  
 Sta L Sta R Elev Sta L Sta R Elev Sta L Sta R Elev  
 13 34 58 50 80 58 140 185 58  
 444 535 64

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 50

INPUT

Description:  
 Station Elevation Data num= 25  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 73.76 .3 63.76 15.6 62.16 21.9 54.16 32.2 53.46  
 42.3 53.56 68.84 54.11 84 51.08 104 51.08 104 55.16  
 132 55.16 149.9 56.16 153.5 57.16 161.6 58.56 170 58.7  
 172 58.7 180 58 190 56 194 58 201 60  
 212 62 220 60 265 62 275 64 342 66

Manning's n Values num= 4  
 Sta n Val Sta n Val Sta n Val Sta n Val  
 0 .02 21.9 .02 68.84 .018 104 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 21.9 104 393.5 397.9 398.7 .1 .3  
 Blocked Obstructions num= 1  
 Sta L Sta R Elev  
 282 342 66

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 45

INPUT

Description:  
 Station Elevation Data num= 21  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 55.06 14.4 54.36 25.2 54.16 45.21 54.22 52.34 54.21  
 70 50.68 90 50.68 90 53 112.5 52.01 126.52 52.01  
 135 56 154 57 156 57 167 56 179 55  
 185 55 233 56 252 58 380 60 384 62  
 434 64

Manning's n Values num= 5  
 Sta n Val  
 0 .02 52.34 .018 90 .02 112.5 .02 126.52 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 52.34 126.52 375 380 385 .1 .3  
 Blocked Obstructions num= 1  
 Sta L Sta R Elev  
 281 385 64

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 40

INPUT

Description:  
 Station Elevation Data num= 23  
 Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev  
 0 55.86 5.8 55.16 23.5 55.16 35.04 55.69 62 50.3  
 82 50.3 82 56.15 94.6 56.06 106.1 56.16 112.85 56.16  
 116.5 56.16 121 55.16 126 54.16 129.8 53.16 133 53.06  
 134 54 146 54 152 52.5 157 56 190 56  
 260 56 380 58 400 60

Manning's n Values num= 5  
 Sta n Val  
 0 .02 35.04 .018 82 .02 121 .02 157 .02

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 35.04 157 343.5 344.8 345.4 .1 .3  
 Blocked Obstructions num= 1  
 Sta L Sta R Elev  
 236 348 60

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 35

INPUT

Description:

Station Elevation Data		num= 17									
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	55.66	14.7	55.16	22.1	55.16	48.8	56.16	56.3	56.16		
113	56	120	54	125	52	135	50	150	50		
155	48.5	164	52	166	56	195	56	238	56		
324	58	447	60								

Manning's n Values		num= 3			
Sta	n Val	Sta	n Val	Sta	n Val
0	.02	125	.02	164	.02

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	125	164		345.5	336.8		.1	.3

Blocked Obstructions		num= 1	
Sta L	Sta R	Elev	
232	447	60	

CROSS SECTION RIVER: Leucadia  
 REACH: Combine RS: 30

INPUT

Description:

Station Elevation Data		num= 18									
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	58.16	36.8	58.16	59.999	59.16	57.59999	59.16	81.3	59.16		
94.39999	59.16	104.2	58.16	111	58	125	54	134	50		
140	46	155	46	163	46	176	54	191	56		
319	56	400	58	470	60						

Manning's n Values		num= 3			
Sta	n Val	Sta	n Val	Sta	n Val
0	.02	140	.02	163	.02

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	140	163		0	0		.1	.3

SUMMARY OF MANNING'S N VALUES

River:Leucadia

Reach	River Sta.	n1	n2	n3	n4	n5
Vulcan	3300.14	.03	.035	.03		
Vulcan	3200.15	.03	.035	.03		
Vulcan	3100.16	.03	.035	.03		
Vulcan	3000.17	.03	.035	.03		
Vulcan	2900.18	.03	.035	.03		
Vulcan	2800.19	.03	.035	.03		
Vulcan	2700.20	.03	.035	.03		
Vulcan	2600.21	.03	.035	.03		
Vulcan	2500.22	.03	.035	.03		
Vulcan	2400.23	.03	.035	.03		
Vulcan	2300.24	.03	.035	.03		
Vulcan	2200.25	.03	.035	.03		
Vulcan	2100.26	.03	.035	.03		
Vulcan	245	.03	.035	.03		
Vulcan	240	.03	.035	.03		
Vulcan	235	.03	.035	.03		
Vulcan	230	.02	.02	.02		
Vulcan	225	.02	.02	.02		
Vulcan	220	.02	.02	.02		
Vulcan	215	.02	.02	.02		
Vulcan	195	.02	.02	.02		
Vulcan	175	.02	.02	.02		
Vulcan	165	.02	.02	.02		
Vulcan	150	.02	.02	.02		
101	230	.02	.02	.02		
101	225.3	.02	.02	.02		
101	225.2	.02	.02	.02		

101	225.1	.02	.02	.02		
101	220	.02	.02	.02		
101	215	.02	.02	.02		
101	210	.02	.02	.02		
101	205	.02	.02	.02		
101	195	.02	.02	.02		
101	190	.02	.02	.02		
101	185	.02	.02	.02		
101	180	.02	.02	.02		
101	175	.02	.02	.02		
101	170	.02	.02	.02		
101	165	.02	.02	.02		
101	160	.02	.02	.02		
101	150	.02	.02	.02		
101	145	.02	.02	.02		
Combine	140	.02	.02	.02		
Combine	135	.02	.02	.02		
Combine	130	.02	.02	.02		
Combine	125	.02	.02	.02		
Combine	120	.02	.02	.02		
Combine	115	.02	.02	.02		
Combine	110	.02	.02	.02		
Combine	105	.02	.02	.02		
Combine	100	.02	.02	.02		
Combine	95	.02	.02	.02		
Combine	90	.02	.02	.02		
Combine	85	.02	.02	.02		
Combine	80	.02	.02	.02		
Combine	75	.02	.02	.018	.02	.02
Combine	70	.02	.02	.018	.02	.02
Combine	65	.02	.02	.02	.018	.02
Combine	60	.02	.02	.018	.02	.02
Combine	55	.02	.02	.02	.018	.02
Combine	50	.02	.02	.018	.02	.02
Combine	45	.02	.018	.02	.02	.02
Combine	40	.02	.018	.02	.02	.02
Combine	35	.02	.02	.02		
Combine	30	.02	.02	.02		

SUMMARY OF REACH LENGTHS

River: Leucadia

Reach	River Sta.	Left	Channel	Right
Vulcan	3300.14	100	100	100
Vulcan	3200.15	100	100	100
Vulcan	3100.16	100	100	100
Vulcan	3000.17	100	100	100
Vulcan	2900.18	100	100	100
Vulcan	2800.19	100	100	100
Vulcan	2700.20	100	100	100
Vulcan	2600.21	100	100	100
Vulcan	2500.22	100	100	100
Vulcan	2400.23	100	100	100
Vulcan	2300.24	100	100	100
Vulcan	2200.25	100	100	100
Vulcan	2100.26	15	15	15
Vulcan	245	175	175	175
Vulcan	240	275	275	275
Vulcan	235	120	120	120
Vulcan	230	175	180	185
Vulcan	225	190	185	185
Vulcan	220	175	175	175
Vulcan	215	290	290	290
Vulcan	195	340	340	340
Vulcan	175	225	220	220
Vulcan	165	360	360	360
Vulcan	150	305	305	305
101	230	104.1	100.2	136.3
101	225.3	5	5	5
101	225.2	5	5	5
101	225.1	134.2	131.9	133.3

101	220	222.7	215.1	206.1
101	215	78.2	80.6	89.6
101	210	47.1	45.4	64.5
101	205	141.2	142.6	152.6
101	195	143.6	102.4	81.7
101	190	109.2	93.8	106
101	185	56.4	82.7	111.4
101	180	83.8	85.3	85.6
101	175	120.2	124.8	122.1
101	170	137.5	137.6	138.7
101	165	309.6	309.5	308.6
101	160	48.6	52.6	51.9
101	150	151.2	154.7	157.7
101	145	175.6	160.5	160.3
Combine	140	141.5	123.2	117.1
Combine	135	122.2	126.9	132.7
Combine	130	197.5	197.3	196.3
Combine	125	131.2	129.8	132.3
Combine	120	86.1	88.2	95.5
Combine	115	218.8	211.7	222.6
Combine	110	180.1	165.1	173.7
Combine	105	106.7	119.5	229.1
Combine	100	360	340	360
Combine	95	365.1	364.9	363
Combine	90	356.3	355.5	353.7
Combine	85	353.7	357.5	356.9
Combine	80	357.5	355.1	356.2
Combine	75	488	485	489
Combine	70	360	359.8	358.2
Combine	65	384.7	386.9	384.1
Combine	60	364.2	363.7	367
Combine	55	354.4	358.2	348.8
Combine	50	393.5	397.9	398.7
Combine	45	375	380	385
Combine	40	343.5	344.8	345.4
Combine	35	345.5	336.8	337.3
Combine	30	0	0	0

SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS  
River: Leucadia

Reach	River Sta.	Contr.	Expan.
Vulcan	3300.14	.1	.3
Vulcan	3200.15	.1	.3
Vulcan	3100.16	.1	.3
Vulcan	3000.17	.1	.3
Vulcan	2900.18	.1	.3
Vulcan	2800.19	.1	.3
Vulcan	2700.20	.1	.3
Vulcan	2600.21	.1	.3
Vulcan	2500.22	.1	.3
Vulcan	2400.23	.1	.3
Vulcan	2300.24	.1	.3
Vulcan	2200.25	.1	.3
Vulcan	2100.26	.1	.3
Vulcan	245	.1	.3
Vulcan	240	.1	.3
Vulcan	235	.1	.3
Vulcan	230	.1	.3
Vulcan	225	.1	.3
Vulcan	220	.1	.3
Vulcan	215	.1	.3
Vulcan	195	.1	.3
Vulcan	175	.1	.3
Vulcan	165	.1	.3
Vulcan	150	.1	.3
101	230	.1	.3
101	225.3	.1	.3
101	225.2	.1	.3
101	225.1	.1	.3
101	220	.1	.3

101	215	.1	.3
101	210	.1	.3
101	205	.1	.3
101	195	.1	.3
101	190	.1	.3
101	185	.1	.3
101	180	.1	.3
101	175	.1	.3
101	170	.1	.3
101	165	.1	.3
101	160	.1	.3
101	150	.1	.3
101	145	.1	.3
Combine	140	.1	.3
Combine	135	.1	.3
Combine	130	.1	.3
Combine	125	.1	.3
Combine	120	.1	.3
Combine	115	.1	.3
Combine	110	.1	.3
Combine	105	.1	.3
Combine	100	.1	.3
Combine	95	.1	.3
Combine	90	.1	.3
Combine	85	.1	.3
Combine	80	.1	.3
Combine	75	.1	.3
Combine	70	.1	.3
Combine	65	.1	.3
Combine	60	.1	.3
Combine	55	.1	.3
Combine	50	.1	.3
Combine	45	.1	.3
Combine	40	.1	.3
Combine	35	.1	.3
Combine	30	.1	.3

**ATTACHMENT 5**

**RICK ENGINEERING COMPANY  
COST ESTIMATES FOR  
ALTERNATIVE 3 – PHASED CONSTRUCTION  
AND ALTERNATIVE 4**

# Alternative 3 - Main Line

## Cost Estimate for 100-Year Capacity Storm Drain System

OPINION OF PROBABLE CONSTRUCTION COSTS				
FOR: CITY OF ENCINITAS / HIGHWAY 101		JOB NO.:		14413
CUT AND COVER FOR PROPOSED STORM DRAIN - MAIN LINE		DATE:		06/03/04
ESTIMATED BY: CA		CHECKED BY: CSH		REVISED:
ITEM DESCRIPTION	QUANTITY	UNIT	UNIT PRICES	TOTAL COSTS
MOBILIZATION	1	LS	\$1,200,000.00	\$1,200,000
CONSTRUCTION STAKING	1	LS	\$25,000.00	\$25,000
EROSION CONTROL	1	LS	\$50,000.00	\$50,000
TRAFFIC CONTROL	1	LS	\$600,000.00	\$600,000
TRENCHING / EXCAVATION (20' DEEP)	20,000	CY	\$8.00	\$160,000
TRENCHING / EXCAVATION (30' DEEP)	40,000	CY	\$10.00	\$400,000
TRENCHING / EXCAVATION (40' DEEP)	50,000	CY	\$16.00	\$800,000
SHORING, STEEL SHEET PILES (20' DRIVE)	129,600	SF	\$18.00	\$2,332,800
SHORING, STEEL SHEET PILES (30' DRIVE)	181,200	SF	\$19.00	\$3,442,800
SHORING, STEEL SHEET PILES (40' DRIVE)	225,600	SF	\$20.00	\$4,512,000
SLURRY BACKFILLING	70,000	CY	\$50.00	\$3,500,000
DOZER BACKFILLING, AIR TAMPED (TOP 10	40,000	CY	\$8.00	\$320,000
EXPORT EXCAVATED MATERIAL	70,000	CY	\$10.00	\$700,000
36" RCP	470	LF	\$84.00	\$39,480
60" RCP	890	LF	\$188.00	\$167,320
66" RCP	510	LF	\$220.00	\$112,200
72" RCP	410	LF	\$250.00	\$102,500
78" RCP	960	LF	\$315.00	\$302,400
90" RCP	610	LF	\$430.00	\$262,300
96" RCP	1,750	LF	\$475.00	\$831,250
102" RCP	2,080	LF	\$525.00	\$1,092,000
108" RCP	1,400	LF	\$575.00	\$805,000
GASKETS AND FITTINGS	1	LS	\$200,000.00	\$200,000
CLEANOUT STRUCTURE 36" RCP	1	EA	\$10,000.00	\$10,000
CLEANOUT STRUCTURE 60" RCP	1	EA	\$12,000.00	\$12,000
CLEANOUT STRUCTURE 66" RCP	1	EA	\$14,000.00	\$14,000
CLEANOUT STRUCTURE 72" RCP	1	EA	\$14,000.00	\$14,000
CLEANOUT STRUCTURE 78" RCP	1	EA	\$18,000.00	\$18,000
CLEANOUT STRUCTURE 90" RCP	1	EA	\$18,000.00	\$18,000
CLEANOUT STRUCTURE 96" RCP	3	EA	\$18,000.00	\$54,000
CLEANOUT STRUCTURE 102" RCP	3	EA	\$24,000.00	\$72,000
CLEANOUT STRUCTURE 108" RCP	3	EA	\$24,000.00	\$72,000
INTERIM STRUCTURES	2	EA	\$100,000.00	\$200,000
SUBTOTAL				\$22,441,050
DESIGN / INDIRECT 40%				\$8,976,420
10% CONTINGENCY				\$2,244,105
<b>TOTAL</b>				<b>\$33,661,575</b>

**ASSUMPTIONS:**

- 1) SITE IS CLEARED AND GRUBBED, READY TO EXCAVATE STORM DRAIN TRENCH, NO SELECTIVE CLEARING REQUIRED.
- 2) WATER TABLE DEPTH IS UNKNOWN, DEWATERING IS EXCLUDED FROM THIS ESTIMATED OPINION.
- 3) COST FOR SHORING/SHEET PILES ASSUMES PILES ARE DRIVEN, EXTRACTED AND SALVAGED.
- 4) NUMBER OF CLEANOUT AND INLET STRUCTURES IS APPROXIMATE, NO BASIS FOR DESIGN.
- 5) NO COST INCLUDED FOR MODIFICATION OF EXISTING UTILITIES.
- 6) TRENCHING / EXCAVATION DEPTHS ARE ASSUMED.

# Alternative 3 - Laterals

OPINION OF PROBABLE CONSTRUCTION COSTS				
FOR: CITY OF ENCINITAS / HIGHWAY 101		JOB NO.:		14413
CUT AND COVER FOR PROPOSED STORM DRAIN - LATERALS		DATE:		06/03/04
ESTIMATED BY: CA		CHECKED BY: CSH		REVISED:
ITEM DESCRIPTION	QUANTITY	UNIT	UNIT PRICES	TOTAL COSTS
MOBILIZATION	1	LS	\$250,000.00	\$250,000
CONSTRUCTION STAKING	1	LS	\$25,000.00	\$25,000
EROSION CONTROL	1	LS	\$50,000.00	\$50,000
TRAFFIC CONTROL	1	LS	\$300,000.00	\$300,000
TRENCHING / EXCAVATION (10' DEEP)	9,000	CY	\$4.00	\$36,000
TRENCHING / EXCAVATION (15' DEEP)	4,000	CY	\$6.00	\$24,000
TRENCHING / EXCAVATION (20' DEEP)	4,000	CY	\$8.00	\$32,000
SHORING, STEEL SHEET PILES (10' DRIVE)	72,000	SF	\$18.00	\$1,296,000
SHORING, STEEL SHEET PILES (15' DRIVE)	36,000	SF	\$19.00	\$684,000
SHORING, STEEL SHEET PILES (20' DRIVE)	32,000	SF	\$20.00	\$640,000
SLURRY BACKFILLING	3,000	CY	\$50.00	\$150,000
DOZER BACKFILLING, AIR TAMPED (TOP 10	14,000	CY	\$8.00	\$112,000
EXPORT EXCAVATED MATERIAL	3,000	CY	\$10.00	\$30,000
24"RCP	400	LF	\$44.00	\$17,600
30"RCP	400	LF	\$64.00	\$25,600
36"RCP	1,800	LF	\$84.00	\$151,200
42"RCP	200	LF	\$107.00	\$21,400
48"RCP	400	LF	\$127.00	\$50,800
60"RCP	2,000	LF	\$188.00	\$376,000
GASKETS AND FITTINGS	1	LS	\$150,000.00	\$150,000
CLEANOUT STRUCTURE 24" RCP	1	EA	\$5,000.00	\$5,000
CLEANOUT STRUCTURE 30" RCP	1	EA	\$5,500.00	\$5,500
CLEANOUT STRUCTURE 36" RCP	3	EA	\$6,000.00	\$18,000
CLEANOUT STRUCTURE 42" RCP	1	EA	\$6,500.00	\$6,500
CLEANOUT STRUCTURE 48" RCP	1	EA	\$7,000.00	\$7,000
CLEANOUT STRUCTURE 60" RCP	3	EA	\$8,000.00	\$24,000
RAILROAD CROSSINGS	9	EA	\$100,000.00	\$900,000
<b>SUBTOTAL</b>				<b>\$5,387,600</b>
DESIGN / INDIRECT 35%				\$1,885,660
10% CONTINGENCY				\$538,760
<b>TOTAL</b>				<b>\$7,812,020</b>

**ASSUMPTIONS:**

- 1) SITE IS CLEARED AND GRUBBED, READY TO EXCAVATE STORM DRAIN TRENCH, NO SELECTIVE CLEARING REQUIRED.
- 2) WATER TABLE DEPTH IS UNKNOWN, DEWATERING IS EXCLUDED FROM THIS ESTIMATED OPINION.
- 3) COST FOR SHORING/SHEET PILES ASSUMES PILES ARE DRIVEN, EXTRACTED AND SALVAGED.
- 4) NUMBER OF CLEANOUT AND INLET STRUCTURES IS APPROXIMATE, NO BASIS FOR DESIGN.
- 5) NO COST INCLUDED FOR MODIFICATION OF EXISTING UTILITIES.
- 6) TRENCHING / EXCAVATION DEPTHS ARE ASSUMED.

# Alternative 4 - Main line

**Table 11. Cost Estimate for 10-Year Capacity Storm Drain System**

OPINION OF PROBABLE CONSTRUCTION COSTS				
FOR: CITY OF ENCINITAS / HIGHWAY 101			JOB NO.:	14413
CUT AND COVER FOR PROPOSED STORM DRAIN - MAIN LINE			DATE:	06/03/04
ESTIMATED BY: CA                      CHECKED BY: CSH			REVISED:	
ITEM DESCRIPTION	QUANTITY	UNIT	UNIT PRICES	TOTAL COSTS
MOBILIZATION	1	LS	\$400,000.00	\$400,000
CONSTRUCTION STAKING	1	LS	\$25,000.00	\$25,000
EROSION CONTROL	1	LS	\$50,000.00	\$50,000
TRAFFIC CONTROL	1	LS	\$600,000.00	\$600,000
TRENCHING / EXCAVATION (20' DEEP)	18,149	CY	\$8.00	\$145,188
TRENCHING / EXCAVATION (30' DEEP)	32,827	CY	\$10.00	\$328,272
TRENCHING / EXCAVATION (40' DEEP)	35,000	CY	\$16.00	\$560,000
SHORING, STEEL SHEET PILES (20' DRIVE)	148,120	SF	\$18.00	\$2,666,160
SHORING, STEEL SHEET PILES (30' DRIVE)	223,080	SF	\$19.00	\$4,238,520
SHORING, STEEL SHEET PILES (40' DRIVE)	207,120	SF	\$20.00	\$4,142,400
SLURRY BACKFILLING	56,849	CY	\$50.00	\$2,842,454
DOZER BACKFILLING, AIR TAMPED (TOP 10	28,647	CY	\$8.00	\$229,173
EXPORT EXCAVATED MATERIAL	56,849	CY	\$10.00	\$568,491
30" RCP	947	LF	\$64.00	\$60,608
48" RCP	2,756	LF	\$127.00	\$350,012
54" RCP	978	LF	\$158.00	\$154,524
60" RCP	2,740	LF	\$188.00	\$515,120
72" RCP	2,589	LF	\$250.00	\$647,250
GASKETS AND FITTINGS	1	LS	\$200,000.00	\$200,000
CLEANOUT STRUCTURE 30" RCP	2	EA	\$10,000.00	\$20,000
CLEANOUT STRUCTURE 48" RCP	5	EA	\$12,000.00	\$60,000
CLEANOUT STRUCTURE 54" RCP	2	EA	\$14,000.00	\$28,000
CLEANOUT STRUCTURE 60" RCP	4	EA	\$14,000.00	\$56,000
CLEANOUT STRUCTURE 66" RCP	1	EA	\$18,000.00	\$18,000
CLEANOUT STRUCTURE 72" RCP	5	EA	\$18,000.00	\$90,000
<b>SUBTOTAL</b>				<b>\$18,995,172</b>
DESIGN / INDIRECT 35%				\$6,648,310
10% CONTINGENCY				\$1,899,517
<b>TOTAL</b>				<b>\$27,543,000</b>

**ASSUMPTIONS:**

- 1) SITE IS CLEARED AND GRUBBED, READY TO EXCAVATE STORM DRAIN TRENCH, NO SELECTIVE CLEARING REQUIRED.
- 2) STORM DRAIN SYS. DESIGNED FOR 10YR STORM.
- 3) WATER TABLE DEPTH IS UNKNOWN, DEWATERING IS EXCLUDED FROM THIS ESTIMATED OPINION.
- 4) COST FOR SHORING/SHEET PILES ASSUMES PILES ARE DRIVEN, EXTRACTED AND SALVAGED.
- 5) NUMBER OF CLEANOUT AND INLET STRUCTURES IS APPROXIMATE, NO BASIS FOR DESIGN.
- 6) NO COST INCLUDED FOR MODIFICATION OF EXISTING UTILITIES.
- 7) TRENCHING / EXCAVATION DEPTHS ARE ASSUMED.

# Alternative 4 - Laterals

OPINION OF PROBABLE CONSTRUCTION COSTS				
FOR: CITY OF ENCINITAS / HIGHWAY 101			JOB NO.:	14413
CUT AND COVER FOR PROPOSED STORM DRAIN - LATERALS			DATE:	06/03/04
ESTIMATED BY: CA		CHECKED BY: CSH		REVISED:
ITEM DESCRIPTION	QUANTITY	UNIT	UNIT PRICES	TOTAL COSTS
MOBILIZATION	1	LS	\$250,000.00	\$250,000
CONSTRUCTION STAKING	1	LS	\$25,000.00	\$25,000
EROSION CONTROL	1	LS	\$50,000.00	\$50,000
TRAFFIC CONTROL	1	LS	\$300,000.00	\$300,000
TRENCHING / EXCAVATION (10' DEEP)	9,000	CY	\$4.00	\$36,000
TRENCHING / EXCAVATION (15' DEEP)	4,000	CY	\$6.00	\$24,000
TRENCHING / EXCAVATION (20' DEEP)	4,000	CY	\$8.00	\$32,000
SHORING, STEEL SHEET PILES (10' DRIVE)	72,000	SF	\$18.00	\$1,296,000
SHORING, STEEL SHEET PILES (15' DRIVE)	36,000	SF	\$19.00	\$684,000
SHORING, STEEL SHEET PILES (20' DRIVE)	32,000	SF	\$20.00	\$640,000
SLURRY BACKFILLING	3,000	CY	\$50.00	\$150,000
DOZER BACKFILLING, AIR TAMPED (TOP 10	14,000	CY	\$8.00	\$112,000
EXPORT EXCAVATED MATERIAL	3,000	CY	\$10.00	\$30,000
24"RCP	400	LF	\$44.00	\$17,600
30"RCP	400	LF	\$64.00	\$25,600
36"RCP	1,800	LF	\$84.00	\$151,200
42"RCP	200	LF	\$107.00	\$21,400
48"RCP	400	LF	\$127.00	\$50,800
60"RCP	2,000	LF	\$188.00	\$376,000
GASKETS AND FITTINGS	1	LS	\$150,000.00	\$150,000
CLEANOUT STRUCTURE 24" RCP	1	EA	\$5,000.00	\$5,000
CLEANOUT STRUCTURE 30" RCP	1	EA	\$5,500.00	\$5,500
CLEANOUT STRUCTURE 36" RCP	3	EA	\$6,000.00	\$18,000
CLEANOUT STRUCTURE 42" RCP	1	EA	\$6,500.00	\$6,500
CLEANOUT STRUCTURE 48" RCP	1	EA	\$7,000.00	\$7,000
CLEANOUT STRUCTURE 60" RCP	3	EA	\$8,000.00	\$24,000
RAILROAD CROSSINGS	9	EA	\$100,000.00	\$900,000
SUBTOTAL				\$5,387,600
DESIGN / INDIRECT 35%				\$1,885,660
10% CONTINGENCY				\$538,760
<b>TOTAL</b>				<b>\$7,812,020</b>

**ASSUMPTIONS:**

- 1) SITE IS CLEARED AND GRUBBED, READY TO EXCAVATE STORM DRAIN TRENCH, NO SELECTIVE CLEARING REQUIRED.
- 2) WATER TABLE DEPTH IS UNKNOWN, DEWATERING IS EXCLUDED FROM THIS ESTIMATED OPINION.
- 3) COST FOR SHORING/SHEET PILES ASSUMES PILES ARE DRIVEN, EXTRACTED AND SALVAGED.
- 4) NUMBER OF CLEANOUT AND INLET STRUCTURES IS APPROXIMATE, NO BASIS FOR DESIGN.
- 5) NO COST INCLUDED FOR MODIFICATION OF EXISTING UTILITIES.
- 6) TRENCHING / EXCAVATION DEPTHS ARE ASSUMED.

**ATTACHMENT 6**

**HALEY & ALDRICH COST ESTIMATES:**

**JUNE 8, 2004**

**AUGUST 13, 2004**

**HALEY & ALDRICH COST ESTIMATE – JUNE 8, 2004**  
**“GEOTECHNICAL FEASIBILITY STUDY”**

Haley & Aldrich, Inc.  
9040 Friars Rd.  
Suite 220  
San Diego, CA 92108-5860  
Tel: 619.280.9210  
Fax: 619.280.9415  
HaleyAldrich.com

**HALEY &  
ALDRICH**

8 June 2004  
File No. 30769-000

Mr. Dennis Bowling  
Rick Engineering Company  
5620 Friars Road  
San Diego, California 92110-2596

Subject: Geotechnical Feasibility Study  
Trenchless Construction Methods  
Encinitas Storm Drain Project  
Encinitas, California

Dear Dennis:

Haley & Aldrich, Inc. (Haley & Aldrich) is pleased to provide this letter report presenting the results of our geotechnical feasibility study to evaluate trenchless techniques for storm drain pipeline installation. Our study was performed in accordance with our 10 February 2004 proposal and the Consultant and Subconsultant Agreement dated 5 April 2004. For our study we have received plan and profile drawings from Rick Engineering Company (Rick) for "Leucadia Drainage & Sewer Force Main, CMD95A & CEE97A," dated 23 July 2001. We have also received the following two geotechnical reports for the soil conditions in the general area:

- "Comments on GeoPacifica Report of August 24, 2001, Highway 101 Sewer Force Main Replacement, 14" PVC Sewer Force Main System, Encinitas, California," dated 30 July 2003, prepared by Kleinfelder, Inc.
- "Geotechnical Investigation, Beacon's Beach Access, Encinitas, California," date 17 April 2003, prepared by URS Corporation.

#### **PROJECT DESCRIPTION**

From our discussions with you, we understand that flooding occurs in the area of Highway 101 after storm events. The City of Encinitas (City) would like to alleviate this flooding by upgrading the existing storm drain system in the area. The approximate location of the reported flooding and the proposed new storm drains (project site) are presented on the Vicinity Map, Figure 1. We further understand that three different storm drain reaches are being considered to upgrade the current storm drain system. These reaches include the Leucadia Boulevard to Beacon's Beach storm drain, the Highway 101 storm drain, and the various railroad crossings. Each of these storm drain reaches has unique properties requiring different trenchless alternative methods.

#### **OFFICES**

Boston  
*Massachusetts*

Cleveland  
*Ohio*

Dayton  
*Ohio*

Detroit  
*Michigan*

Hartford  
*Connecticut*

Kansas City  
*Kansas*

Los Angeles  
*California*

Manchester  
*New Hampshire*

Parsippany  
*New Jersey*

Portland  
*Maine*

Rochester  
*New York*

Santa Barbara  
*California*

Tucson  
*Arizona*

Washington  
*District of Columbia*

The Leucadia Boulevard to Beacon's Beach reach would start at Leucadia Roadside Park adjacent to Highway 101 and drain along Leucadia Boulevard to empty onto Beacon's Beach. We understand that a 48-inch diameter pipe is planned for this reach. This storm drain would be approximately 840 feet long. We understand that a diversionary structure would be installed at the storm drain inlet to divert normal flows into the existing storm drain and that the new storm drain would only be flowing during major storms. This line would alleviate some of the flooding in the area and may be used in conjunction with the Highway 101 storm drain. The proposed alignment for the Leucadia Boulevard reach is shown on Figure 2.

Based on preliminary information received from Rick, we understand that the Highway 101 reach will extend from just south of the intersection of Marcheta and Highway 101 and drain north to empty into Batiquitos Lagoon with the pipeline alignment traversing under the Highway 101 right-of-way. This proposed storm drain will drain the storm waters of most of the catchment area along Highway 101. The alignment is approximately 9,000 feet long with the approximate location shown on Figure 3. Tentatively, the storm drain diameter has been estimated at about 36 inches at the south end, stepping up incrementally in size to about 9 feet at the north end of the proposed alignment. This storm drain will be in addition to the existing 24-inch storm drain, which will remain in service. Storm drain manhole locations for the Highway 101 reach have been assumed to be needed at storm drain laterals. These laterals are anticipated approximately every 1000 feet.

The final reach involves transporting storm flows from the east side of the existing railroad tracks to the west side to tie into the Highway 101 storm drain. We understand that storm flows currently pass from the east to west by surface flow through the railroad track ballast. We further understand that the proposed storm drain crossings are anticipated to consist of a 48-inch diameter pipe. The number of railroad crossings required is not known at this time. We estimate that the trenchless portions of these crossings will be approximately 50 feet in length about every 1,000 feet along the railroad tracks. The approximate location of the storm drain laterals are shown on Figure 4.

## **SCOPE OF WORK**

For this study we performed a site reconnaissance on 20 April 2004, reviewed the drawings provided by Rick, and reviewed the geotechnical reports for the project area. We have also reviewed published geologic data for the project site. This feasibility study was performed to evaluate several trenchless techniques for installation of new pipelines for the three reaches listed above, including constructability and anticipated order of magnitude design and construction costs for various methods. The results of our feasibility study are presented hereinafter.

## **SITE AND SUBSURFACE CONDITIONS**

### **Site Conditions**

The various reaches are located along existing city streets or under the railroad tracks adjacent to Highway 101. The Leucadia Boulevard alignment starts at Leucadia Park at the intersection of Highway 101 and Leucadia Boulevard at an elevation of approximately +55 feet, Mean Sea Level (MSL). This alignment follows Leucadia Boulevard, which rises to an

elevation of approximately +95 feet, MSL to the parking lot for Beacon's Beach. The parking lot is positioned at the crest of coastal bluffs leading down to the beach below at an elevation of approximately +10 feet, MSL. Leucadia Boulevard is bordered on both sides by residential housing. The proposed storm drain would have an inlet structure at Leucadia Park and drain by gravity to Beacon's Beach.

The Highway 101 reach starts just south of the intersection of Marcheta and Highway 101 and extends along the Highway 101 right-of-way, north to La Costa Avenue. This alignment then moves east of Highway 101 to Batiquitos Lagoon below. Highway 101 is a four-lane asphalt paved highway with two lanes of traffic in each direction. There is parking along the west side of the highway and a tree lined median between the north and south bound lanes. Commercial buildings border the west side of Highway 101 and railroad tracks and the accompanying right-of-way border the highway on the east. Highway 101 gently slopes from an elevation of approximately +75 feet, MSL at El Portal to approximately +55 feet, MSL at Andrew Avenue. The highway rises to +60 feet, MSL at La Costa Avenue before descending towards Batiquitos Lagoon. We understand that the proposed storm drain would be located approximately 15 to 30 feet below the ground surface along the highway and empty into Batiquitos Lagoon.

We understand that the railroad crossings would be installed to transport water under the existing railroad tracks from the east to the west. The railroad tracks are relatively level and dirt access roads border the railroad on either side.

### **Geologic Conditions**

Based on our review of the available information and our site reconnaissance; we anticipate that the different reaches described above are underlain by several marine deposits including Pleistocene sand terrace deposits, the Ardath Formation and the underlying Torrey Sandstone. Fill soils derived from these parent formational soils may be encountered along the proposed pipeline reaches near the ground surface. Landslide Debris will most likely be encountered along the coastal bluffs at the end of the Leucadia Boulevard reach at Beacon's Beach.

As noted above the fill material is anticipated to be derived from the native formational material in the area. Fill materials are anticipated to be shallow (less than 10 feet thick) deposits along the graded roadways and railroad right-of-way.

Terrace deposits are exposed at the surface or underlying the fill material. The terrace deposits consist of medium dense to dense, light brown to reddish brown silty sand and sandy silt, with occasional layers of cohesionless sand. The terrace deposits are relatively flat lying sedimentary beds encountered to depths in excess of 30 feet as described in the Kleinfelder, 2003 report. The terrace deposits extend down to an elevation of approximately +20 to +25 feet, MSL at the contact with the underlying Ardath Shale.

The Ardath Shale in the area generally consists of light gray to gray green hard claystone with some slickensided bedding planes. The Ardath Shale may be encountered at lower elevations of the proposed trenchless pipeline reaches. The Torrey Sandstone underlies the site at depth, but is not anticipated within the limits of the pipeline excavations.

Several ancient landslides, thought to have occurred during the late Pleistocene have been mapped along the coastal bluffs in the Encinitas area. At the western end of the Leucadia Boulevard pipeline reach, at Beacon's Beach, a large amphitheatre-shaped landslide has been mapped. The proposed pipeline alignment would pass through this landslide. We understand that the City currently plans to stabilize this landslide within the next eight months to a year. However, if landslide stabilization is not performed prior to the installation of the storm drain pipeline, landslide debris and a failure surface will be encountered. The landslide debris consists of rotated section of the terrace deposits and Ardath Shale. The landslide failure surface consists of remolded clay with low shear strength.

Groundwater conditions within the pipeline alignment are uncertain based on the available geologic reports. Seepage was observed in the borings performed in 2001 for the existing storm drain at depths below Highway 101 of about 12 feet but is likely due to perched water.

### **TRENCHLESS ALTERNATIVES**

The subsurface conditions at the site and the final storm drain alignments selected will have an influence on the trenchless technology applicable for this project. More than one method may be technically feasible for each reach, depending upon the final alignment selected. Based on our experience it is our opinion that several trenchless methods may be technically feasible for each reach. For the Leucadia Boulevard to Beacon's Beach Reach these methods include Horizontal Directional Drilling (HDD), Jack and Bore, microtunneling, and conventional tunneling methods. For the Highway 101 Reach these methods may include one single method or a combination of methods, including mechanical methods, such as a wheel Tunnel Boring Machine (TBM) or a digger shield; and conventional tunneling methods, such as a modified horseshoe tunnel. A combination of two of these methods may be used as the required pipeline diameter changes along the alignment. Jack & Bore is probably the most feasible method for the railroad crossings. A discussion of each of these methods for the respective reach follows.

#### **Leucadia Boulevard to Beacon's Beach**

##### **A. Horizontal Directional Drilling**

Horizontal directional drilling is a process of drilling a guided borehole, referred to as the pilot hole through the ground along a predetermined path from a bore pit to a receiving pit. For larger pipes, once the pilot hole is completed it is reamed by one or more passes of a reamer to a diameter typically 1.5 times the pipe diameter. Throughout the pilot hole drilling and reaming process, soil and rock cuttings are removed and borehole stability is maintained by a drilling fluid, typically bentonite slurry. On completion of reaming, the pipe is typically pulled into the borehole. Prior to pulling, the pipe is typically preassembled to its final length so that it can be pulled into the hole in one shot. The pipe can be preassembled in segments and welded/fused in the field during pull back but at an elevated risk and increased pull time.

##### **B. Jack and Bore**

Jack and Bore is a trenchless method in which pipe casing is directly advanced through the ground with thrust provided by hydraulic jacks from a jacking pit and excavation being

performed from within a steerable jacking shield at the leading edge of the pipe being jacked. Soil and rock may be excavated using augers within the casing, which transport the muck through the pipe back to the jacking pit for removal, or alternatively, excavation can be conducted manually by hand-held tools or mechanically with wheel-type or hydraulic excavators at the face. Open face shields are those without a system for pressure regulation at the face in order to prevent uncontrolled ground and groundwater inflow into the face, and wherein the excavation face is readily accessible by the workers. Open face shields are typically used in soil types with good stand-up time, or in soils that have been dewatered or otherwise prestabilized by ground improvement methods such as grouting. For open face shields used on jack and bore projects, removal of excavated soil is typically done using small carts winched between the jacking shaft and the face. The process requires personnel entry into the pipe being jacked to operate excavation equipment.

Typically, the pipe being jacked using jack and bore techniques is the product (final) pipe to be installed. However, with auger boring, where the soil is transported from the face using augers inside the pipe, and with small diameter pipes, an oversize pipe or sleeve would be jacked in-place and the storm drain pipe would be placed in the sleeve and grouted in place. Typically, jacking and boring is done with pipes 42 to 48 in. in diameter and larger.

#### **C. Microtunneling**

Microtunneling is a method of trenchless construction using a remotely controlled, laser-guided tunnel-boring machine that uses pipe jacking and permits continuous support of the excavation face. The remotely operated microtunneling tunnel-boring machine (MTBM) cuts a circular excavation slightly larger than the required pipeline diameter. The MTBM is typically classified as a so called closed face tunneling shield in that there is a face support/stabilization system which uses either earth or slurry pressure to ensure that the soil ahead of the MTBM remains stable and there is no uncontrolled flow of groundwater into the MTBM. The excavated material is mixed into slurry at the face of the MTBM and transported back to a "mud plant" by transmission lines, typically at the jacking shaft site where the solids are removed. The "clean" slurry is then recycled and the solids are disposed of.

#### **D. Conventional Tunneling**

A conventional modified horseshoe tunnel is a method by which the tunnel is excavated a few feet at a time horizontally along the alignment and is supported by the ground's own strength until support structures can be added. The tunnel progresses incrementally with a series of tunnel excavation followed by tunnel support erection. The tunnel support generally consists of beam and column bracing or wire mesh and shotcrete. After the initial support is complete and the tunnel excavation finished, the carrier pipe is installed and the annular space between the carrier pipe and the tunnel support is grouted.

#### **Highway 101**

Several methods are presented below for this reach. However, because of the varying required pipeline diameter, more than one method may be employed for the reach with two different tunnel sizes as will be described in the Recommendations section of this report.

Non-pressurized face machines are applicable for this reach above groundwater levels in formations such as soil, cemented sandstone, conglomerate, and shale. Non-pressurized face machines can also be used below the groundwater level in soil and rock where groundwater seepage can be controlled and adequate ground stability can be maintained. Two types of non-pressurized face machines (TBM and shield tunneling) are considered feasible for this reach of the project. Pressurized face machines can also be used but are not considered necessary for this project.

**A. Tunnel Boring Machine**

A tunnel boring machine consists of a rotating cutterhead and a tunnel shield. The cutterhead excavates the ground at the tunnel heading and is attached to a full circular shield to support the ground during excavation and installation of the initial or final support system. The excavated ground is taken into the machine through openings located within the cutterhead and is conveyed through the machine. The tunnel spoils are subsequently removed from the tunnel using additional conveyor systems and/or a locomotive with muck cars. A TBM would generally be applicable to the longer tunnel segments in ground with good to limited stand-up time.

The initial support system for this method would most likely consist of steel ribs and lagging or lattice support and shotcrete. These liner systems would be installed in the tail of the shield and expanded to support the tunnel. After completion of the tunnel and the initial liner system the carrier pipe would be installed and the annular space would be grouted.

**B. Shield Tunneling**

A digger shield consists of a full circular shield. The shield also supports the ground in the rear of the machine during installation of the initial or final tunnel support system. Shield tunneling requires the use of a tunneling shield, which provides immediate support of the ground prior to installation of the initial support system. The shield is required to have steering jacks to maintain line and grade. The shield may have breasting capabilities to support the face when unstable ground conditions are encountered. Full breasting is usually required during shutdown periods such as weekends, off shifts, and mechanical breakdowns. Dewatering is required when tunneling below natural groundwater. An open faced digger shield is well suited to all the anticipated ground conditions. The open face configuration allows access for removal of cobbles and boulders, if encountered. To allow for man-entry, tunnel shields are usually a minimum of 42-in. diameter.

The initial tunnel support system (typically steel ribs and lagging or liner plate) is erected from within the tail of the tunneling shield and jacking of the tunnel shield from the installed tunnel support is used to advance the shield. The excavation proceeds using hand mining or mechanical excavation methods, such as electric digger arms, breakers, or roadheaders, from within the shield. Muck is transported from the face of the tunnel to the access pit using train type muck cars or conveyor systems. The carrier pipe is placed within the excavated tunnel and the annular space between the carrier pipe and the initial tunnel support system is filled with cement grout.

### **C. Conventional Tunneling**

Two types of conventional tunneling were considered for this reach. A conventional modified horseshoe tunnel as described for the Leucadia Boulevard to Beacon's Beach Reach above and the Sequential Excavation Method, also known as the New Austrian Tunneling Method (NATM). The sequential excavation method is a method of creating underground space, which utilizes the self-supporting capacity of the rock or soil. The tunnel is generally excavated sequentially, beginning with a starter tunnel, and progressively widened with side drifts and/or bottom headings until the required underground space is achieved. Rock bolts, lattice girders, wire mesh and shotcrete are typically used for ground support and reinforcement. When the initial support of the NATM tunnel is finished, drainage, waterproofing, and a final structural liner are added to complete the tunnel. Further evaluation of the ground condition is warranted before selecting this trenchless method, as the Kleinfelder report for the area indicates pockets of cohesionless sand, which will not support itself.

### **D. Jack & Bore**

The Jack & Bore method described above for the Leucadia Boulevard to Beacon's Beach Reach will be the same for this reach as well. This method would be practical for pipeline diameters less than about 7 feet to account for the space limitations for jacking and receiving pits along Highway 101.

### **Railroad Crossings**

The actual number of crossings and the location of the crossings are not known at this time. We assumed one crossing every 1,000 feet (about 11 crossings) and each crossing about 50 feet long. The Jack & Bore method as described above is the most practical method for the railroad crossings. Because of the short distance and the space available for jacking and receiving pits, this method would be both feasible and cost effective. However, for railroad crossings, steel casing around the final carrier pipe will be required in the railroad right-of-way.

### **Shaft Construction**

Each of the trenchless methods described above, except HDD will require a work shaft from the surface to install the tunnel. However, we understand that a drop shaft will be required for the Leucadia Boulevard to Beacon's Beach Reach for the inlet manhole. Work shafts, as defined herein, are the shafts required by the contractor during construction to provide access to the tunnel or trenchless method for personnel and equipment, as well as for removal of excavated material (muck). The work shaft will also be used to jack pipe as necessary and for pipe installation within the tunnel excavation. From a constructability standpoint, it would be desirable, although not necessary, to locate the work shaft at the down stream end of the pipeline segment being constructed. This reduces problems associated with removal of groundwater infiltration and improves efficiency of muck removal. We understand that environmental limitations with staging on the beach will most likely require a work shaft at the upstream end of the alignment for the Leucadia Boulevard to Beacon's Beach Reach. Approximate land area requirements at the work shaft sites would include the access shaft

itself and room for cranes and additional equipment and pipe materials. The area required for the work shafts are anticipated to be on the order of 1 acre for larger tunnels constructed using TBMs or shields. Work shaft area requirements for smaller jack and bore operations can be much smaller, perhaps on the order of ½ acre.

Along with a work shaft, it should be assumed for planning purposes that additional shafts, referred to herein as access shaft will be required at the opposite end of each tunnel or trenchless segment from the work shaft. The purpose of these shafts would be to remove tunnel excavation equipment (shields or TBM's) after completion of excavation and provide access to the tunnel during final lining construction. The various methods will require a different number of intermediate shafts and spacing between shafts as well as the size of the shaft required to account for limited drive lengths. The Jack & Bore methods described can have drive lengths of approximately 400 to 800 feet for the diameters and soil types anticipated. This would require an access shaft at these intervals. Similarly, microtunneling can typically have drive lengths of approximately 1,000 feet. These methods would allow for an entrance shaft at Leucadia Park and a receiving area or pit at Beacon's Beach for the Leucadia Boulevard to Beacon's Beach alignment.

The TBM, shield tunneling, and conventional tunneling methods all have theoretically infinite drive lengths. An access shaft would only need to be installed at the ends of the alignment. However, intermediate shafts may be installed for manhole construction or storm drain laterals as needed. The land area requirement for the access shafts would be on the order of ¼ to ½ acre.

Access shafts could be installed in Leucadia Park and within the median of Highway 101. The entrance shaft for a pipeline of about 9 feet in diameter along Highway 101 could most likely be installed in the vacant parcel between Highway 101 and the railroad tracks, immediately north of La Costa Boulevard to minimize traffic impacts. Intermediate access shafts for jacking pits or manhole construction would generally need to be about 12 to 15 feet wide for pipeline diameters of less than 7 feet and about 20 to 25 feet long for pipeline diameters between 7 and 9 feet. These intermediate shafts may require that parking along Highway 101 be temporarily removed and that the traffic lanes be rerouted around the access shafts to ease traffic impacts. These access shafts could be located to minimize impacts to businesses. Additional work laydown areas for pipe material and equipment storage could be located off the pipeline alignments. Pipe storage laydown areas are currently being utilized along Highway 101 for the installation of storm drain and sewer pipe in Encinitas as shown in the Appendix to this report.

### **Spoil Handling and Disposal**

Spoil will be generated from tunnel boring, shafts and underground excavation activities. The volume will be proportional to the mined volume of the tunnels, shafts and underground excavations, combined with bulking and/or shrinking associated with the soil and rock materials. The bulking factor is the ratio of the excavated volume of material to the in-situ volume of material. Similarly, the shrinkage factor is the ratio of the volume after placement and compaction to the in-situ volume.

The characteristics of the spoil will depend upon the type of material being excavated and the excavation/tunneling methods employed. Every effort should be made during design and construction planning to determine commercial reuse for the spoil. These may include reuse as concrete aggregate, structural fill, daily cover or lining material at landfills, or other uses.

Tunnels which are constructed using slurry methods will create spoil which contains a mixture of slurry and excavated soil or rock. Slurry for tunneling is typically composed of bentonite, a naturally occurring clay mineral, and water. The soil and rock are typically removed from the slurry and the slurry reused via an automated process consisting of a series of sieves, hydro-cyclones and filter presses. Although rigorous separation techniques can remove virtually all slurry from the soil and rock, the potential presence of residual slurry or other materials in the spoil should be considered when selecting a suitable commercial reuse or disposal of the material.

### CONCEPTUAL COST ESTIMATES

Conceptual cost estimates have been prepared for trenchless construction methods and are presented in the table below. These costs include equipment mobilization, excavation and spoils disposal, casing or initial tunnel support, shaft construction, and grouting as applicable.

Proposed Trenchless Method	Estimated Cost <sup>2</sup>	Estimated Construction Duration <sup>3</sup>
<b>Highway 101</b>		
TBM only	\$22 to 25 million	14 months
TBM and shield tunnel	\$23 to 26 million	20 months
TBM and Jack & Bore	\$20 to 24 million	20 months
Conventional (horseshoe or NATM)	\$28 to 33 million	30 months
Digger Shield	\$24 to 28 million	30 months
<b>Leucadia Boulevard</b>		
HDD	\$1.5 to 1.8 million	2 months
Microtunnelling	\$0.90 to 1.05 million	2 months
Jack & Bore	\$0.90 to 1.05 million	3 months
Conventional	\$1 to 1.25 million	6 months
<b>Railroad Crossings<sup>1</sup></b>		
Jack & Bore	\$75,000 to 100,000	1 month each

Notes:

1. Costs for railroad crossings indicated are per crossing. *EACH OR EQUIV 1000'?* The number of crossings and exact lengths are unknown at this time.
2. Estimated costs include shaft construction, tunnel excavation, soil disposal, and pipe installation.
3. Estimated construction schedule includes tunnel and shaft excavation and pipeline installation. Duration is based on 5 day work week.

The estimated costs presented do not include the cost for permitting or other utility realignment. We have assumed a 20 percent contingency in our cost estimate as indicated by the cost estimate range provided. For preliminary planning purposes, we recommend that a design cost of approximately 35 percent be added to the above costs for comparison purposes with the conventional open trench cost estimate prepared by Rick Engineering for this project. We have included an estimated cost of 4.2 million for the cost of the final product pipe,

gaskets and fittings, and the 11 cleanout structures assumed in the Rick Engineering open trench cost estimate. The cost estimate presented above is subject to change based on the number of access shaft required for final pipeline access and the final pipeline alignment, and the number of connections to laterals. Additional cost estimates will be required in subsequent stages of project planning and design.

Contaminated soils are not anticipated to be encountered along the proposed pipeline alignments. Costs associated with testing, handling, or disposal of potentially hazardous material encountered in the subsurface is not included in this project. Likewise the cost for dewatering is not included in this study.

We understand that the landslide on the coastal bluffs at Beacon's Beach will be stabilized within the next year. If this landslide stabilization does not occur before the start of this storm drain project, stabilization of the earth slope in the vicinity of the proposed storm drain will be required, which was not included in this cost estimate.

For cost estimating purposes, we evaluated several different scenarios for the Highway 101 Reach using different trenchless methods and two different tunnel diameters. We assumed that the tunnel may be completed with one 12-foot diameter using TBM technology or with the tunnel diameter stepping down to 7-foot diameter to complete the tunnel with various other methods. The smaller 7-foot diameter was chosen based on the hydraulic requirements for the storm drain. Additional evaluations of the practical tunnel sizes and refinement of the cost estimates can be performed during a follow-on geotechnical investigation. The estimates provided above are for preliminary planning purposed only.

## CONCLUSIONS AND RECOMMENDATIONS

For the proposed project alignments and the geologic and topographic conditions present at the site, it is our opinion that the methods discussed above for each reach are all technically feasible options to install a new pipeline by trenchless technology. The various methods along each pipeline reach are presented on Figures 2 through 4. However, each method has its own limitations. Based on our review of the project constraints, the geologic conditions at the site, our site reconnaissance, our discussion with local contractors, and our experience, the three reaches will each be discussed below. Photographs of the various pipeline alignments, potential access pit locations, and staging areas are presented in an Appendix to this report.

The methods selected are based on the preliminary information obtained for this study. Additional geotechnical investigations and the cost of construction materials may alter the feasibility factors for the recommended methods presented below.

### **Leucadia Boulevard to Beacon's Beach**

It is our opinion that conventional tunneling would be the most feasible trenchless method for the Leucadia Boulevard to Beacon's Beach Reach to keep the alignment within the Leucadia Boulevard right-of-way. Microtunneling or jack & Bore methods may also be reasonable, if a straight alignment from Leucadia Park to Beacon's Beach is permissible (outside of the Leucadia Boulevard right-of-way). Our evaluation takes into account the two horizontal curves in the alignment necessary to stay within the city street right-of-way, the grade change

or slope of the storm drain, and the necessity to pass through the existing landslide. We have assumed that the entrance shaft will be located within Leucadia Park and that the storm drain will empty onto the sand at Beacon's Beach. HDD methods are pushing the size limitations for this reach (an approximately 5-foot diameter tunnel for a 4-foot diameter carrier pipe). Likewise, the approximately 850 foot length may be approaching the upper bound for a feasible drive length for jack & bore techniques.

As the Beacon's Beach end of the pipeline alignment would require passage through the existing landslide, additional hazards are present. Movement of the landslide after pipeline installation could damage the pipe and cause leakage of storm water into the ground, which may propagate the movement of the landslide. We recommend that the landslide repair that is planned occur before the installation of the pipeline. A knockout panel can be placed in the retaining wall planned for the landslide repair to accommodate the trenchless alignment.

### **Highway 101**

For the Highway 101 alignment, we have evaluated excavating one tunnel for the entire approximately 9,000 foot of length with an diameter of 12 feet, and we have evaluated transitioning the tunnel excavation after about 5,800 feet from a 12-ft diameter tunnel to a 7-ft diameter tunnel for the last approximately 3,200 feet at the south end of the alignment, using two different tunnel methods. The diameters and number of transitions selected are preliminary and included for planning purposed only. Additional analyses would be required to evaluate the number of transitions and diameters to be used in design. In our opinion, the most feasible and cost effective methods for the installation of the proposed storm drain would be a combination of a TBM machine for the larger diameter portion of the tunnel followed by a transition to a tunnel excavated using digger shield methods, or one diameter using the TBM method only. Conventional tunneling would be costly and time prohibitive. In addition, conventional methods may not be practical if cohesionless areas of the terrace deposit sandstone are encountered as discussed in the Kleinfelder report. The jack & bore method would be cost effective, but would cause much more disruption to the traffic and business as additional access shafts would be required at approximately 500 foot intervals.

For these methods existing laydown areas that have recently been used for the installation of the 24-inch storm drain and associated sewer lines in the area can probably be used for staging areas for this project. We have assumed that the main tunnel entrance will be located on the vacant parcel of land between Highway 101 and the railroad tracks immediately north of La Costa Avenue. Additional access shafts may be located in the center median of Highway 101 as described above to minimize traffic, parking, and business impacts.

Ground surface settlements resulting from tunneling and their impacts on adjacent utilities and structures will have to be evaluated for this trenchless alignment as additional information becomes available. Surface manifestations of ground settlement would most likely be the greatest directly above the tunnel excavation and diminish to a negligible amount at a distance equal to approximately two times the depth of the tunnel either side of the centerline. If settlement related impacts are determined to be unacceptable then mitigation measures such as compaction grouting will be necessary to reduce tunneling related settlement to acceptable levels.

### **Railroad Crossings**

Because of the short length for each railroad crossing and the requirement for steel casing beneath the railroad tracks, we recommend that jack & bore methods be used for the railroad crossings. However, we understand from Rick Engineering that there are tentative plans to lower the railroad tracks along this stretch of Highway 101 in Encinitas. If this plan comes to fruition, conventional open trench pipe installation may be feasible during the grade realignment of the railroad tracks. If the storm drains are installed prior to lowering of the grade, the steel casing will allow for a minimal amount of soil cover between the pipeline invert and the bottom of the railroad ballast.

### **Further Studies**

This feasibility study was performed based on the geotechnical reports provided to us, published information on the local and regional geology, and our experience in the area. Although the geotechnical information provided was adequate for this conceptual level study, it is not sufficient for future planning and design. Before pipeline design and specifications for trenchless excavation are developed, we recommend that an additional geotechnical investigation be performed for this project including field explorations, laboratory testing, measurement of groundwater, if present, and engineering analyses. In addition, we recommend that the records for the City of Encinitas be examined for additional geotechnical investigations in the area that could assist with the geotechnical investigation for this project. Haley & Aldrich would be pleased to provide this additional geotechnical investigation and recommendations for trenchless pipeline design for the project, if this next step is taken towards the completion of this exciting project.

### **LIMITATIONS**

This report was prepared for the purposes of a feasibility planning study only. The preliminary geotechnical considerations discussed herein are not intended for detailed design purposes. This work was performed by Haley & Aldrich, Inc., in accordance with generally accepted geotechnical engineering practices. No other warranty, expressed or implied, is made.

The preliminary geotechnical considerations presented herein are based, in part, on information from previous subsurface investigations by others. The accuracy of this information and nature and extent of variations along the pipeline alignments may not become evident until additional subsurface explorations are conducted. If changes do appear, it will be necessary to re-evaluate the information presented in this report.

The scope of work for this report did not include an assessment of the presence of or impact that hazardous materials might have on the feasibility or cost of the proposed construction.

Rick Engineering Company

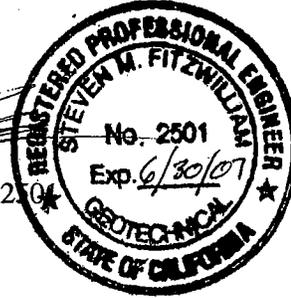
8 June 2004

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Sincerely,

HALEY & ALDRICH, INC.

  
Steven M. Fitzwilliam, G.E. 2501  
Senior Engineer

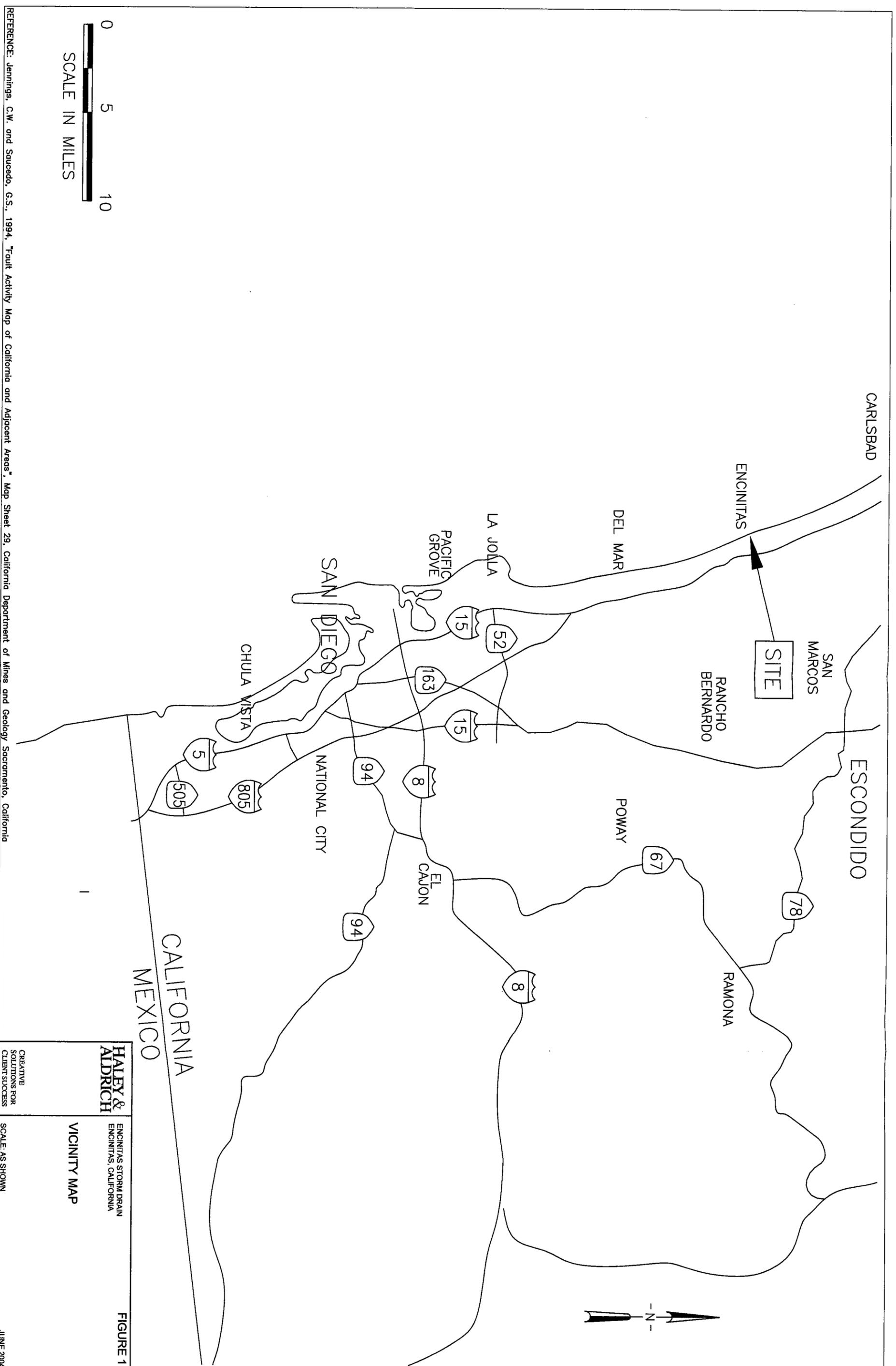


  
Daniel J. Dobbels  
Vice President

Enclosures:

- Figure 1 - Vicinity Map
- Figure 2 - Site Plan Leucadia Boulevard
- Figure 3 - Site Plan Highway 101
- Figure 4 - Site Plan Railroad Crossings
- Appendix A - Project Photographs

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REFERENCE: Jennings, C.W. and Saucedo, G.S., 1994, "Fault Activity Map of California and Adjacent Areas", Map Sheet 29, California Department of Mines and Geology Sacramento, California

0 5 10  
SCALE IN MILES

CALIFORNIA  
MEXICO

HALEY &  
ADDRICH

ENCINITAS STORM DRAIN  
ENCINITAS, CALIFORNIA

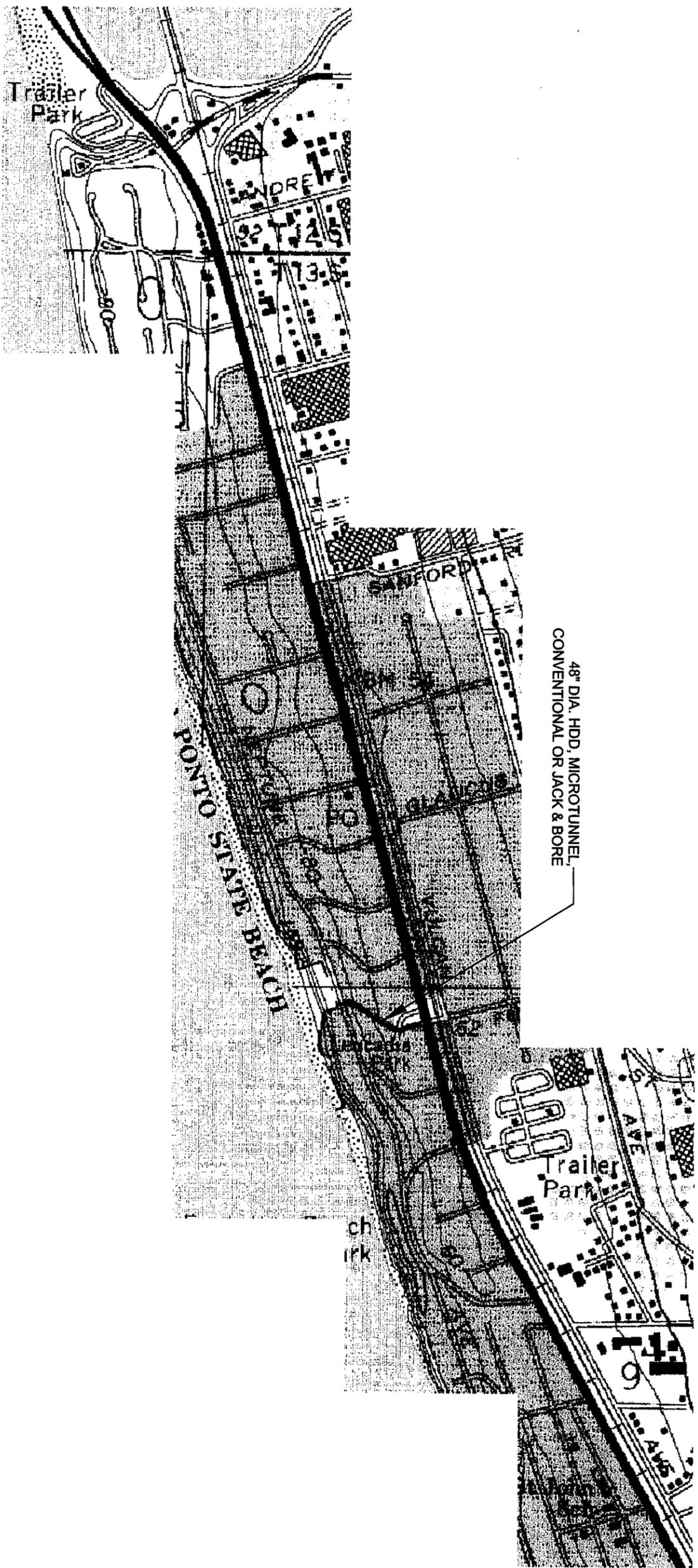
VICINITY MAP

FIGURE 1

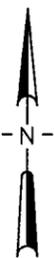
CREATIVE  
SOLUTIONS FOR  
CLIENT SUCCESS

SCALE: AS SHOWN

JUNE 2004



**LEGEND**  
 — PIPELINE ALIGNMENT



0 1/6 1/3  
 APPROXIMATE SCALE IN MILES

SOURCE: USGS ENCINITAS 7.5 QUADRANGLE, 1979

**HALEY &  
 ALDRICH**

ENCINITAS STORM DRAIN  
 ENCINITAS, CALIFORNIA

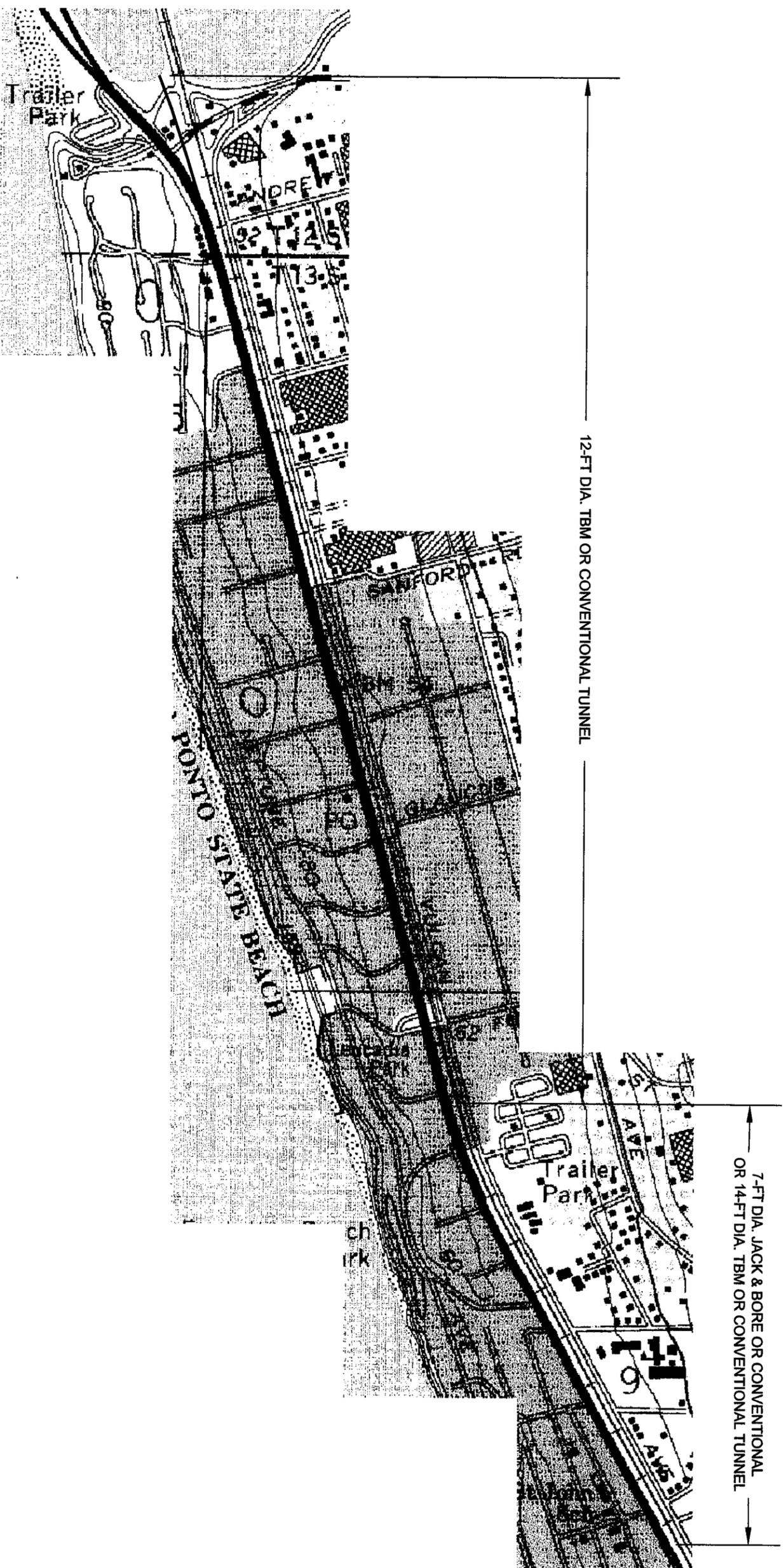
**FIGURE 2**

**SITE PLAN  
 LEUCADIA BOULEVARD STORM DRAIN**

CREATIVE  
 SOLUTIONS FOR  
 CLIENT SUCCESS

SCALE: AS SHOWN

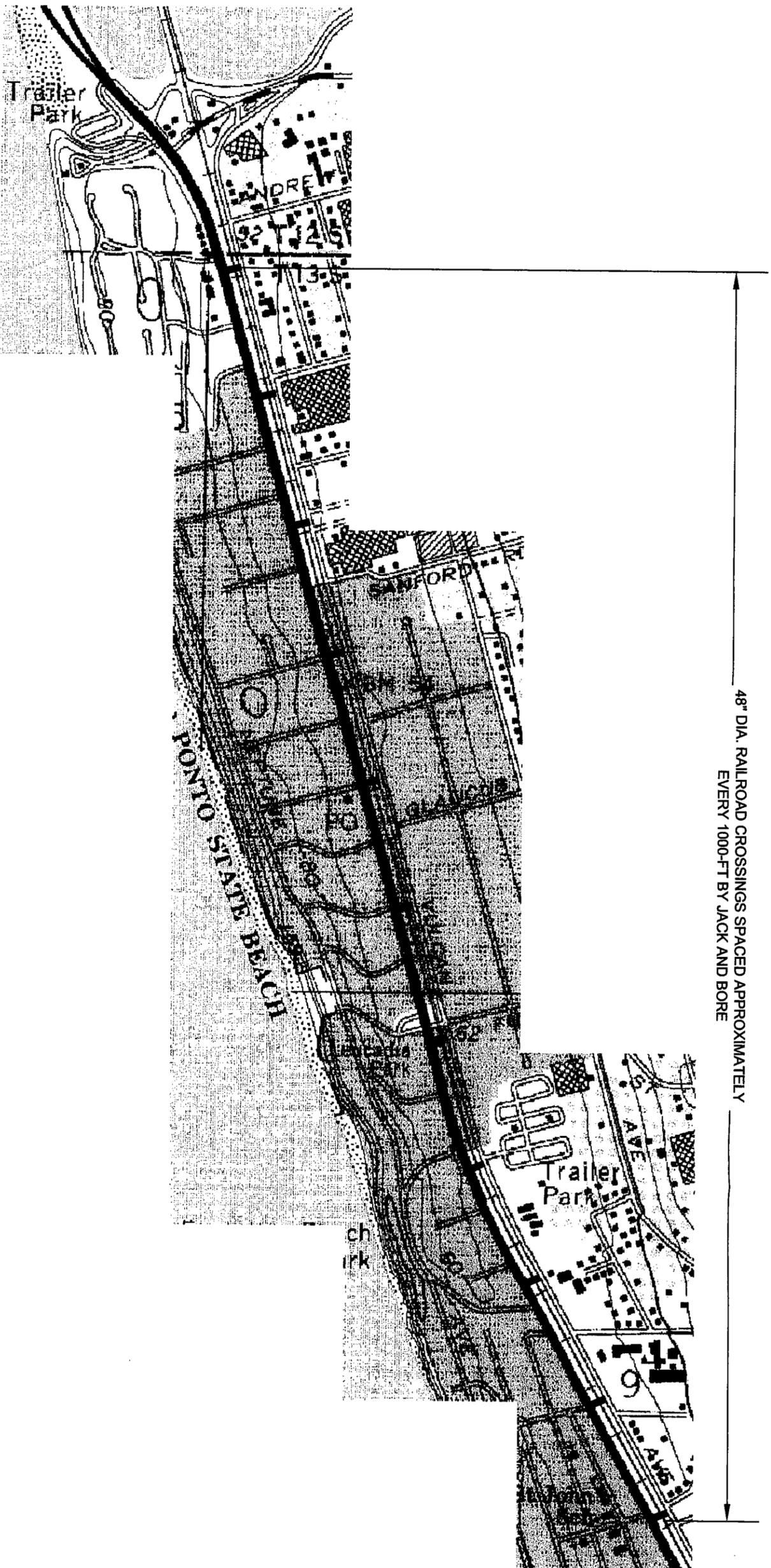
JUNE 2004



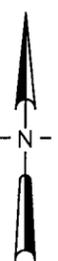
SOURCE: USGS ENCINITAS 7.5' QUADRANGLE, 1979

<p><b>HALEY &amp; ADDRICH</b></p>	<p>ENGINEER ENCINITAS, CALIFORNIA</p>	<p><b>FIGURE 3</b></p>
<p>CREATIVE SOLUTIONS FOR CLIENT SUCCESS</p>	<p><b>SITE PLAN</b> <b>HIGHWAY 101 STORM DRAIN</b></p> <p>SCALE: AS SHOWN</p>	<p>JUNE 2004</p>

48" DIA. RAILROAD CROSSINGS SPACED APPROXIMATELY EVERY 1000-FT BY JACK AND BORE



**LEGEND**  
 — RAILROAD CROSSINGS BY JACK AND BORE



0 1/6 1/3  
 APPROXIMATE SCALE IN MILES

SOURCE: USGS ENCINITAS 7.5' QUADRANGLE, 1979

**HALEY & ADRICH**

ENCINITAS STORM DRAIN  
 ENCINITAS, CALIFORNIA

**FIGURE 4**

**SITE PLAN  
 RAILROAD CROSSINGS**

SCALE: AS SHOWN

JUNE 2004

CREATIVE SOLUTIONS FOR CLIENT SUCCESS



*Potential working shaft location at Leucadia Park*



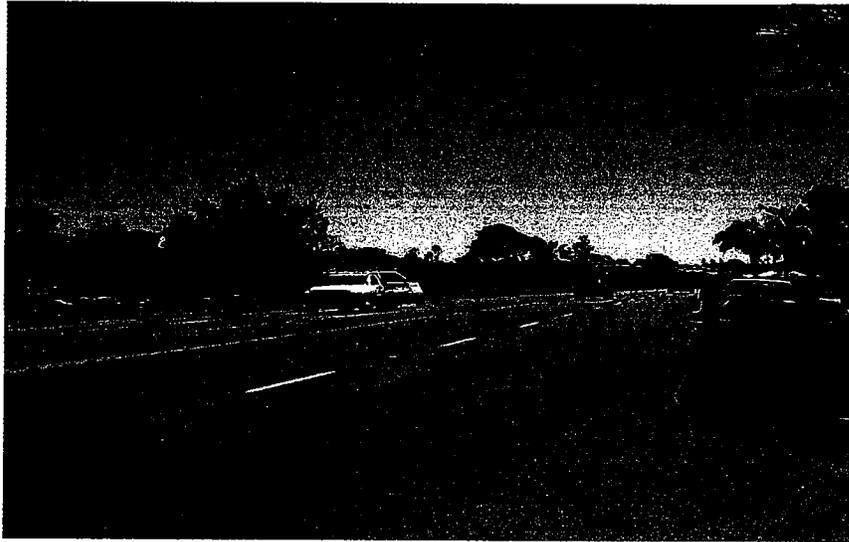
*View looking west of Leucadia Boulevard from Leucadia Park*



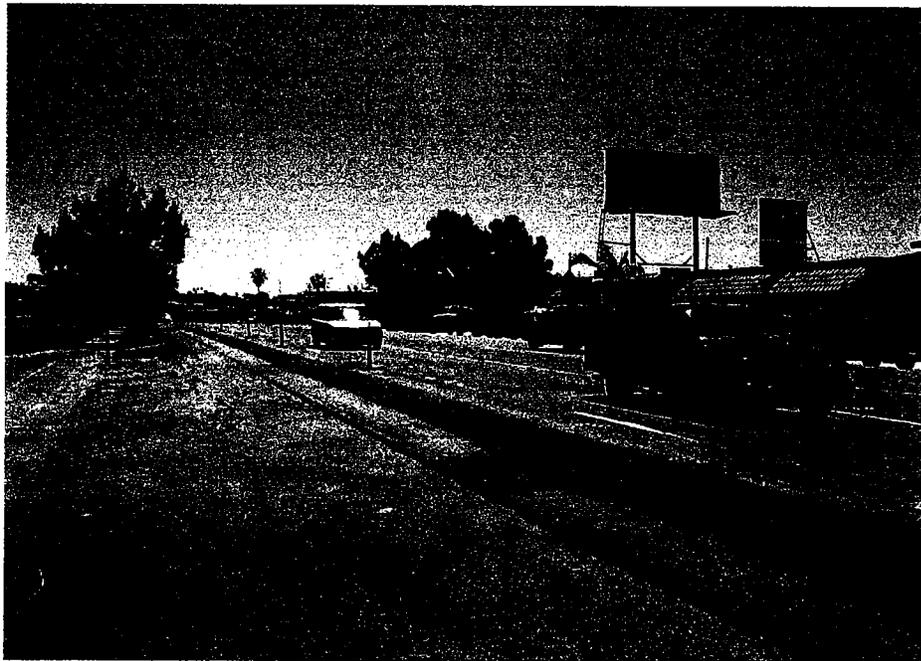
*Parking area above Beacon's Beach along Leucadia Boulevard*



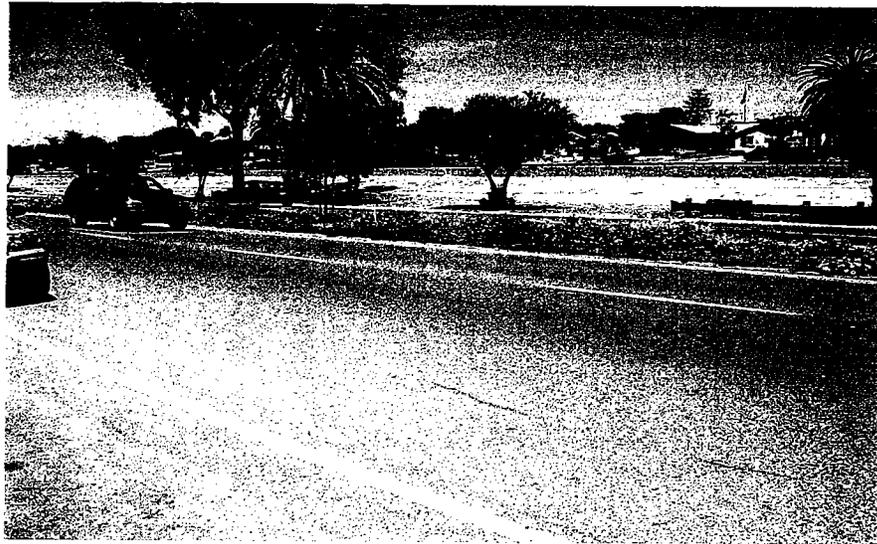
*View of Beacon's Beach Landslide at end of Leucadia Boulevard*



*Highway 101 looking south from Marcheta*



*Highway 101 showing two lanes of traffic each direction, median, and parking on west side of street*



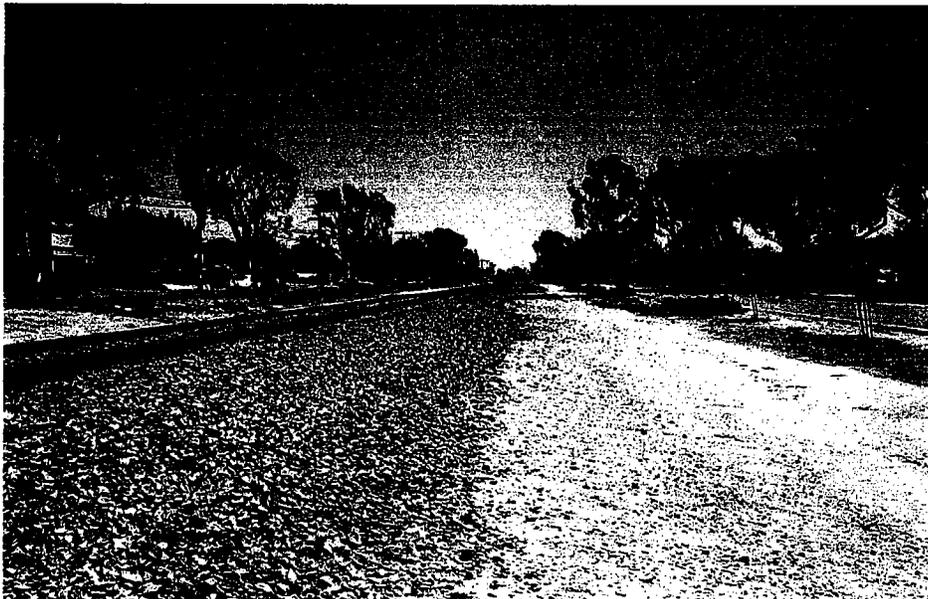
*Highway 101 showing two lanes of traffic each direction, center median, and railroad ballast to the east north or Leucadia Boulevard*



*Vacant lot adjacent to La Costa Avenue between Highway 101 and railroad tracks*



*View from vacant lot adjacent to La Costa Avenue looking down to Batiquitos Lagoon*



*View of railroad tracks adjacent to Highway 101*



*View of laydown area for along Highway 101 for current storm drain and sewer installation project*

**HALEY & ALDRICH COST ESTIMATE – AUGUST 13, 2004**  
**“SUPPLEMENTAL GEOTECHNICAL FEASIBILITY STUDY”**

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**HALEY &  
ALDRICH**

13 August 2004  
File No. 30769-001

Mr. Dennis Bowling  
Rick Engineering Company  
5620 Friars Road  
San Diego, California 92110-2596

Subject: Supplemental Geotechnical Feasibility Study  
Trenchless Construction Methods  
Encinitas Storm Drain Project  
Encinitas, California

Dear Dennis:

Haley & Aldrich, Inc. (Haley & Aldrich) is pleased to provide this letter report presenting the results of our supplemental geotechnical feasibility study relative trenchless pipeline construction techniques for the subject project. We have previously prepared a report for the project entitled "Geotechnical Feasibility Study, Trenchless Construction Methods, Encinitas Storm Drain Project, Encinitas, California," dated 8 June 2004. This letter report is an addendum to that report and presents additional recommendations and cost estimates for alternative pipeline sizes and construction scenarios. Our supplemental geotechnical engineering services were performed in accordance with our proposal dated 20 July 2004 and our Consultant and Subconsultant Agreement dated 5 April 2004.

#### PROJECT DESCRIPTION

As indicated in our 8 June 2004 report, we understand that flooding occurs in the area of Highway 101 after storm events. The City of Encinitas (City) would like to alleviate this flooding by upgrading the existing storm drain system in the area. We further understand that three different storm drain reaches are being considered to upgrade the current storm drain system. These reaches include the Leucadia Boulevard to Beacon's Beach storm drain, the Highway 101 storm drain, and the various railroad crossings.

We understand that the Highway 101 reach will extend from just south of the intersection of Marcheta and Highway 101 and drain north to empty into Batiquitos Lagoon with the pipeline alignment traversing under the Highway 101 right-of-way. This proposed storm drain will drain the storm waters of most of the catchment area along Highway 101. The alignment is approximately 9,000 feet long. This storm drain will be in addition to the existing 24-inch storm drain, which will remain in service. Storm drain manhole locations for the Highway 101 reach have been assumed to be needed at storm drain laterals. These laterals are anticipated approximately every 1000 feet.

#### OFFICES

Boston  
*Massachusetts*

Cleveland  
*Ohio*

Dayton  
*Ohio*

Detroit  
*Michigan*

Hartford  
*Connecticut*

Kansas City  
*Kansas*

Los Angeles  
*California*

Manchester  
*New Hampshire*

Parsippany  
*New Jersey*

Portland  
*Maine*

Rochester  
*New York*

Santa Barbara  
*California*

Tucson  
*Arizona*

Washington  
*District of Columbia*

## **SCOPE OF WORK**

For the proposed storm drain along Highway 101, we have been requested by the City of Encinitas and Rick Engineering to evaluate the estimated costs to construct (by trenchless methods) a storm drain pipeline sized to pass 10-year storm flows as opposed to the 100-year storm flow pipeline sizes considered in our 8 June 2004 report. We understand that the pipeline diameter required for the 10-year storm flows are about half the diameter of those required for the 100-year storm flows. Feasible trenchless construction methods for these smaller pipeline diameters have been evaluated as part of this additional study.

We have also been requested to evaluate the feasibility and estimated construction costs for constructing the full size (100-year storm flow) pipeline along Encinitas Boulevard in three separate construction periods. We understand that the City of Encinitas is interested in the cost to break up the total construction into three parts to spread the costs out over several years. The results of our supplemental feasibility study and cost estimates are presented hereinafter.

## **SITE AND SUBSURFACE CONDITIONS**

### **Site Conditions**

The Highway 101 reach starts just south of the intersection of Marcheta and Highway 101 and extends along the Highway 101 right-of-way, north to La Costa Avenue. This alignment then moves east of Highway 101 to Batiquitos Lagoon below. Highway 101 is a four-lane asphalt paved highway with two lanes of traffic in each direction. There is parking along the west side of the highway and a tree lined median between the north and south bound lanes. Commercial buildings border the west side of Highway 101 and railroad tracks and the accompanying right-of-way border the highway on the east. Highway 101 gently slopes from an elevation of approximately +75 feet, Mean Sea Level (MSL) at El Portal to approximately +55 feet, MSL at Andrew Avenue. The highway rises to +60 feet, MSL at La Costa Avenue before descending towards Batiquitos Lagoon. We understand that the proposed storm drain would be located approximately 15 to 30 feet below the ground surface along the highway and empty into Batiquitos Lagoon.

### **Geologic Conditions**

As described in our 8 June 2004 report; we anticipate that the Highway 101 alignment underlain by several marine deposits including Pleistocene sand terrace deposits, the Ardath Formation and the underlying Torrey Sandstone. Fill soils derived from these parent formational soils may be encountered along the proposed pipeline alignment near the ground surface.

Groundwater conditions within the pipeline alignment are uncertain based on the available geologic reports. Seepage was observed in the borings performed in 2001 for the existing storm drain at depths below Highway 101 of about 12 feet but is likely due to perched water.

## **10-YEAR STORM EVENT**

Our 8 June 2004 report provides a feasibility study for trenchless methods and estimated construction costs for a pipeline with diameters suitable for passing the 100-year storm event. The pipeline diameters for a 10-year storm event are smaller and would present different constraints on trenchless construction. Based on the information provided by Rick Engineering, the design diameter to pass the 100-year storm event has been estimated at about 36 inches at the south end, stepping up incrementally in size to about 9 feet at the north end of the proposed alignment. Alternatively, the design diameter to pass the 10-year storm event has been estimated at about 30 inches at the south end, stepping up incrementally in size to about 6 feet at the north end.

For background, evaluations for the 100-year storm event design, included two different tunnel diameters for different pipeline reaches (e.g. part of the alignment was assumed to be a 12-foot diameter tunnel to accommodate the larger diameter pipe and part of the alignment was assumed to be an approximately 7-foot diameter tunnel). This scenario of using two different tunnel diameters and potential trenchless methods is impractical for the smaller required diameter of the 10-year storm pipeline design and was not considered. The trenchless methods considered feasible for the 10-year storm event are non-pressurized face tunnel boring machines, shield tunneling, conventional tunneling, and jack & bore. These methods are described below as in our 8 June 2004 report for convenience.

### **Trenchless Alternatives**

#### **A. Tunnel Boring Machine**

For this study we define a tunnel boring machine as consisting of a rotating cutterhead and a tunnel shield. The cutterhead excavates the ground at the tunnel heading and is attached to a full circular shield to support the ground during excavation and installation of the initial or final support system. The excavated ground is taken into the machine through openings located within the cutterhead and is conveyed through the machine. The tunnel spoils are subsequently removed from the tunnel using additional conveyor systems and/or a locomotive with muck cars. A TBM would generally be applicable to the longer tunnel segments in ground with good to limited stand-up time.

The initial support system for this method would most likely consist of steel ribs and lagging or lattice support and shotcrete. These liner systems would be installed in the tail of the shield and expanded to support the tunnel. After completion of the tunnel and the initial liner system the carrier pipe would be installed and the annular space would be grouted.

#### **B. Shield Tunneling**

A digger shield consists of a full circular shield. The shield also supports the ground in the rear of the machine during installation of the initial or final tunnel support system. Shield tunneling requires the use of a tunneling shield, which provides immediate support of the ground prior to installation of the initial support system. The shield is required to have steering jacks to maintain line and grade. The shield may have breasting capabilities to support the face when unstable ground conditions are encountered. Full breasting is usually

required during shutdown periods such as weekends, off shifts, and mechanical breakdowns. Dewatering is required when tunneling below natural groundwater. An open faced digger shield is well suited to all the anticipated ground conditions. The open face configuration allows access for removal of cobbles and boulders, if encountered. To allow for man-entry, tunnel shields are usually a minimum of 42-in. diameter.

The initial tunnel support system (typically steel ribs and lagging or liner plate) is erected from within the tail of the tunneling shield and jacking of the tunnel shield from the installed tunnel support is used to advance the shield. The excavation proceeds using hand mining or mechanical excavation methods, such as electric digger arms, breakers, or roadheaders, from within the shield. Muck is transported from the face of the tunnel to the access pit using train type muck cars or conveyor systems. The carrier pipe is placed within the excavated tunnel and the annular space between the carrier pipe and the initial tunnel support system is filled with cement grout.

### **C. Conventional Tunneling**

Two types of conventional tunneling were considered. A conventional modified horseshoe tunnel is a method by which the tunnel is excavated a few feet at a time horizontally along the alignment and is supported by the ground's own strength until support structures can be added. The tunnel progresses incrementally with a series of tunnel excavation followed by tunnel support erection. The tunnel support generally consists of beam and column bracing or wire mesh and shotcrete. After the initial support is complete and the tunnel excavation finished, the carrier pipe is installed and the annular space between the carrier pipe and the tunnel support is grouted.

Alternatively, for larger diameter tunnel excavations, the Sequential Excavation Method, also known as the New Austrian Tunneling Method (NATM) may be used. The sequential excavation method is a method of creating underground space, which utilizes the self-supporting capacity of the rock or soil. The tunnel is generally excavated sequentially, beginning with a starter tunnel, and progressively widened with side drifts and/or bottom headings until the required underground space is achieved. Rock bolts, lattice girders, wire mesh and shotcrete are typically used for ground support and reinforcement. When the initial support of the NATM tunnel is finished, drainage, waterproofing, and a final structural liner are added to complete the tunnel.

Although technically feasible, an NATM tunnel would likely not be practicable for the smaller size of the 10-year storm pipeline diameters.

### **D. Jack & Bore**

Jack and Bore is a trenchless method in which pipe casing is directly advanced through the ground with thrust provided by hydraulic jacks from a jacking pit and excavation being performed from within a steerable jacking shield at the leading edge of the pipe being jacked. Soil and rock may be excavated using augers within the casing, which transport the muck through the pipe back to the jacking pit for removal, or alternatively, excavation can be conducted manually by hand-held tools or mechanically with wheel-type or hydraulic excavators at the face. Open face shields are those without a system for pressure regulation at

the face in order to prevent uncontrolled ground and groundwater inflow into the face, and wherein the excavation face is readily accessible by the workers. Open face shields are typically used in soil types with good stand-up time, or in soils that have been dewatered or otherwise prestabilized by ground improvement methods such as grouting. For open face shields used on jack and bore projects, removal of excavated soil is typically done using small carts winched between the jacking shaft and the face. The process requires personnel entry into the pipe being jacked to operate excavation equipment.

Typically, the pipe being jacked using jack and bore techniques is the product (final) pipe to be installed. However, with auger boring, where the soil is transported from the face using augers inside the pipe, and with small diameter pipes, an oversize pipe or sleeve would be jacked in-place and the storm drain pipe would be placed in the sleeve and grouted in place. Typically, jacking and boring is done with pipes 42 to 48 in. in diameter and larger.

### Shaft Construction

Work shafts, as defined herein, are the vertical excavations that are required by the contractor during construction to provide access to the tunnel or trenchless method for personnel, ventilation, and equipment, as well as for removal of excavated material (spoil). The work shaft requirements presented in our 8 June 2004 report for the project are applicable for both of the new scenarios evaluated. However, additional considerations are discussed below for the phased construction option.

### Conceptual Cost Estimates

Conceptual cost estimates have been prepared for trenchless construction methods and are presented in the table below. These costs include equipment mobilization, excavation and spoils disposal, casing or initial tunnel support, shaft construction, and grouting as applicable.

Proposed Trenchless Method 10-year Storm Event	Estimated Cost <sup>1</sup>	Estimated Construction Duration <sup>2</sup>
TBM only	\$13 to 16 million	14 months
TBM and shield tunnel	N/A	N/A
TBM and Jack & Bore	N/A	N/A
Conventional (horseshoe or NATM)	\$15 to 18 million	30 months
Digger Shield	\$15 to 18 million	30 months
Jack & Bore	\$13 to 16 million	25 months

Notes:

1. Estimated costs include shaft construction, tunnel excavation, soil disposal, and pipe installation.
2. Estimated construction schedule includes tunnel and shaft excavation and pipeline installation. Duration is based on 5 day work week.

The estimated costs presented do not include the cost for permitting or other utility realignment. We have assumed a 20 percent contingency in our cost estimate as indicated by the cost estimate range provided. For preliminary planning purposes, we recommend that a design cost of approximately 35 percent be added to the above costs for comparison purposes with the conventional open trench cost estimate prepared by Rick Engineering for this project.

We have included an estimated cost of \$1.7 million for the cost of the final product pipe, gaskets and fittings, and the 11 cleanout structures assumed in the Rick Engineering open trench cost estimate.

The cost estimate presented above is subject to change based on the number of access shaft required for final pipeline access and the final pipeline alignment, and the number of connections to laterals. Additional cost estimates will be required in subsequent stages of project planning and design.

Contaminated soils are not anticipated to be encountered along the proposed pipeline alignments. Costs associated with testing, handling, or disposal of potentially hazardous material encountered in the subsurface is not included in this project. Likewise the cost for dewatering is not included in this study.

### PHASED CONSTRUCTION OF PIPELINE FOR 100 YEAR STORM EVENT

The feasibility and estimated costs for phased construction of the pipeline diameters for the 100-year storm event were evaluated for this project. The methods described above and in our 8 June 2004 report for Highway 101 were evaluated for construction performed in three separate phases. As the ultimate phased construction schedule is unknown, no consideration for time related cost escalation the economic factors with time was taken into consideration.

#### Conceptual Cost Estimates

For conveyance, the table below includes the estimated costs to perform the construction of the pipeline to pass a 100-year storm event as presented in our 8 June 2004 report, as well as the estimated costs to perform the construction in three separate stages. The additional costs associated with the phased construction include additional mobilization/demobilization of the equipment and personnel, overhead costs for additional mobilizations (such as additional costs for new electrical and water taps), additional access shafts required for separate mobilizations, and efficiencies of excavation with three shorter alignments rather than one long alignment. The base costs as presented in our 8 June 2004 report include equipment mobilization, excavation and spoils disposal, casing or initial tunnel support, shaft construction, and grouting as applicable.

Proposed Trenchless Method	Estimated Cost <sup>1</sup> - From 8 June 2004 Report	Estimated Cost <sup>1</sup> - Phased Construction
TBM only	\$22 to 25 million	\$25 to 29 million
TBM and shield tunnel	\$23 to 26 million	\$26 to 30 million
TBM and Jack & Bore	\$20 to 24 million	\$23 to 27 million
Conventional (horseshoe or NATM)	\$28 to 33 million	\$32 to 37 million
Digger Shield	\$24 to 28 million	\$27 to 32 million

Notes:

1. Estimated costs include shaft construction, tunnel excavation, soil disposal, and pipe installation.

Similar to above, the estimated costs presented do not include the cost for permitting or other utility realignment. We have assumed a 20 percent contingency in our cost estimate as

indicated by the cost estimate range provided. For preliminary planning purposes, we recommend that a design cost of approximately 35 percent be added to the above costs for comparison purposes with the conventional open trench cost estimate prepared by Rick Engineering for this project. We have included an estimated cost of \$4.2 million for the cost of the final product pipe, gaskets and fittings, and the 11 cleanout structures assumed in the Rick Engineering open trench cost estimate. Contaminated soils are not anticipated to be encountered along the proposed pipeline alignments.

## **CONCLUSIONS AND RECOMMENDATIONS**

For the proposed project alignments and the geologic and topographic conditions present at the site, it is our opinion that the methods discussed above are all technically feasible options to install a new pipeline by trenchless technology. However, each method has its own limitations. Additional geotechnical investigations and the cost of construction materials may alter the feasibility factors for the recommended methods presented below.

### **10-Year Storm Event**

The methods evaluated and presented above for the 10-year storm event pipeline diameters are all considered feasible. Using two different methods and two different diameters along the alignment, as evaluated for the 100-year storm event were not considered practical. The cost estimates suggest that both the jack & bore and the TBM methods would be the most cost efficient. However, the jack & bore method would cause much more disruption to the traffic and business as additional access shafts would be required at approximately 500 foot intervals.

The diameters and number of transitions selected are preliminary and included for planning purposes only. Additional analyses would be required to evaluate the number of transitions and diameters to be used in design.

### **Phased Construction of Pipeline for 100 Year Storm Event**

As indicated in the table above presenting our estimated costs for the phased construction, as compared with construction performed during one mobilization to the site, the phased construction is significantly more expensive. However, inflation, depreciation of equipment and financing costs were outside of the scope of work for this project and were not considered. These factors may make the phased construction more cost effective or feasible over time.

## **SUMMARY OF COST ESTIMATE**

We have summarized the estimated costs for the various scenarios in the table below for convenience. We have also included in the estimated costs below the 35 percent design costs as assumed above. A 20 percent contingency is still evident in the range of estimated costs presented. Included in the table are the 100-year storm costs from our 8 June 2004 report, the 100-year storm pipeline costs for construction in three phases, and the 10-year storm pipeline costs.

Proposed Trenchless Method	Estimated Cost 100-year Storm	Estimated Cost 100-year Storm - Phased Construction	Estimated Cost 10-year Storm
TBM only	\$30 to 34 million	\$34 to 39 million	\$18 to 22 million
TBM and shield tunnel	\$31 to 35 million	\$35 to 40 million	N/A
TBM and Jack & Bore	\$27 to 32 million	\$31 to 36 million	N/A
Conventional (horseshoe or NATM)	\$38 to 45 million	\$43 to 50 million	\$20 to 24 million
Digger Shield	\$32 to 38 million	\$36 to 43 million	\$20 to 24 million
Jack & Bore	N/A	N/A	\$18 to 22 million

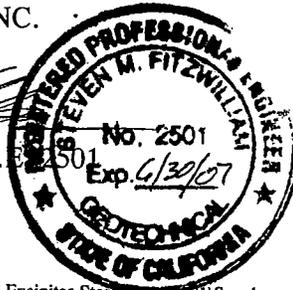
**LIMITATIONS**

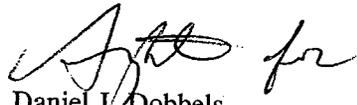
This report is subject to the same limitations presented in our 8 June 2004 report for the project.

Sincerely,

HALEY & ALDRICH, INC.

  
 Steven M. Fitzwilliam, G.E.  
 Senior Engineer



  
 Daniel J. Dobbels  
 Vice President

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